



**REPORT**

# Preliminary Geotechnical Data Report REV01

*Interstate 95 Bridges 1427 and 5800 over Stillwater Avenue, Bangor, Maine  
(WIN 027176.00)*

Submitted to:

**Maine Department of Transportation**

Submitted by:

**WSP USA, Inc.**

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WIN 027176.00 / WSP US0025840.3905

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## 1.0 INTRODUCTION

This Preliminary Geotechnical Data Report (PGDR) summarizes the results of the geotechnical subsurface investigation and laboratory testing program of site soils and rock that WSP USA Inc. (WSP) performed to support the replacement of Bridge No. 1427 & No. 5800 that carries Interstate 95 (I-95) over Stillwater Avenue in Bangor, Maine. Figure 1 shows the site location.

## 2.0 PROJECT UNDERSTANDING

WSP reviewed the historical drawings<sup>1</sup> for the two existing I-95 bridges over Stillwater Avenue including historical boring logs provided by MaineDOT. The existing structures were constructed in 1960 and consist of two (2) three-span bridges with two (2) piers and two (2) abutments each.

## 3.0 GEOLOGIC SETTING

Available site geology information, consisting of surficial<sup>2</sup> geologic maps of the area indicate subsurface conditions consist of road embankment fills overlying Pleistocene Presumpscot Formation glaciomarine deposits generally consisting predominantly of silt and fine sand.

Available site geology information, consisting of bedrock<sup>3</sup> geologic maps of the area indicate bedrock in the region is mapped as the Medium bedded facies of the Penobscot River Member of the Silurian-aged Bangor Formation of the Vassalboro Group, consisting of medium to dark gray, fine-grained to very fine-grained, metawacke; a metamorphosed impure, poorly sorted sandstone with appreciable clay minerals. The 1958 historical Kenduskeag Avenue boring logs<sup>1</sup> characterize bedrock as phyllite (a general term for metamorphosed clay-rich rocks).

## 4.0 SUBSURFACE INVESTIGATIONS

### 4.1 Geotechnical Borings

WSP completed six (6) borings (BB-BSA-102, BB-BSA-103, BB-BSA-108, BB-BSA-109, BB-BSA-109A, and BB-BSA-110) within the paved roadway of Stillwater Avenue beyond the extents of the existing bridges in May 2024 and seven (7) borings (BB-BSA-101, BB-BSA-104, BB-BSA-104A, BB-BSA-105, BB-BSA-106, BB-BSA-107, and BB-BSA-111) within the paved roadway of I-95 beyond the existing bridge abutments in July 2024. The as-drilled boring locations and elevations are summarized in Table 1 and boring locations with respect to existing site features are illustrated in the Boring Location Plan in Figure 2.

The field program included Standard Penetration Testing (SPT) of predominantly coarse-grained soils and recovery of rock core from the bedrock. A WSP geotechnical engineer monitored drilling activities, selected sampling intervals, logged subsurface conditions encountered, and obtained soil samples for use in visual descriptions and subsequent laboratory testing and classification.

WSP subcontracted Seaboard Drilling, LLC (Seaboard) of Bangor, Maine, who completed the borings using a Diedrich D-50 drill rig for all borings. Borings were advanced using solid stem augers (SSA) followed by 4-inch or

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<sup>1</sup> Maine State Highway Commission, 1960 Final As Built Plans, Project No. I-95-8(6)180, Interstate #95 over Stillwater Ave. in the City of Bangor, Penobscot County, Plans and Profiles, 41 sheets, Received from HNTB, Filename: 1427 & 5800 Bangor 1958 As-Built.pdf.

<sup>2</sup> Syverson, K.M., Thompson, A.M., and Johnston, R.A., (2011). Surficial Geology, Bangor Quadrangle, Maine. Open-File No. 11-6, Maine Geological Survey, 1 sheet, scale 1:24,000.

<sup>3</sup> Pollock, S.G., Johnston, R.A., (2011). Bedrock Geology of the Bangor Quadrangle, Maine, Open-File No. 11-57, Maine Geological Survey, 1 sheet, scale 1:240,000.

3-inch casing and drive and wash methods to refusal; rock coring was performed in either 4-inch or 3-inch casing seated in rock, depending on the drilling conditions.

SPT was performed using a calibrated automatic hammer system and standard 2-inch split spoon sampler in general accordance with American Society for Testing and Materials (ASTM) D1586. Sampling was conducted at approximately 5-foot intervals, where split spoons were advanced 24 inches with a 140-pound hammer dropped 30 inches. WSP recorded the number of hammer blows required to advance the sampler through each 6-inch increment. Measured, uncorrected N-values, calculated as the sum of the hammer blows to advance the sampler during the 6-inch to 18-inch intervals. Seaboard provided WSP with a copy of the automatic hammer calibration report from November 2023<sup>4</sup> for both drill rigs used. WSP used a calibrated hammer energy transfer ratio of 106.6% for the May borings and 108.7% for the July borings provided by in the report convert the measured N-values to  $N_{60}$  values. Uncorrected N-values and  $N_{60}$  are shown on the boring logs (Appendix A). WSP collected and stored soil samples in sealed glass jars for later evaluation and laboratory testing.

Up to 10 feet of rock core was collected in each boring using NX size (1-7/8-inch diameter) diamond tipped core barrels following either refusal of casing or failure to advance the split spoon sampler or roller bit. Rock core samples were placed in wooden boxes and transported to the WSP office. WSP recorded the lithology, Total Core Recovery (TCR), Rock Quality Designation (RQD), and coring rates for each core run which are provided in the boring logs in Appendix A. Photographs of all collected rock core are presented in Appendix B.

The boring logs provided in Appendix A present details of the sampling methods used, field data obtained, and soil and rock conditions encountered during the investigation. A description of the boring log symbols and terms used for the soil and rock descriptions precedes the boring logs. A WSP geotechnical engineer monitored drilling activities, selected sampling intervals, logged subsurface conditions encountered, and obtained soil samples for use in visual descriptions and subsequent laboratory testing and classification WSP field characterized the soils in accordance with ASTM D2488. WSP field characterized the bedrock lithology.

## 4.2 Geologic Evaluation of Exposed Rock Cuts

On April 23, 2024, WSP visited the Stillwater Avenue site to collect geological data from the exposed rock cuts along Stillwater Avenue beneath the I-95 existing bridge foundations. The general locations of the exposed rock cuts are shown in plan view in Appendix D. During the site visit, WSP measured 37 geologic discontinuities and photographed existing rock cut conditions. Photographs of the existing rock cut conditions and discontinuities evaluated are presented in Appendix E. Our discontinuity measurements and observations are summarized in Table 2 (attached) and include discontinuity type, orientation, persistence, aperture, infilling materials, estimated strength, surface roughness, shape, spacing, and groundwater conditions. Our measured discontinuity orientations are plotted in Appendix D.1.

## 5.0 LABORATORY TESTING PROGRAM

After reviewing the collected samples in the office, WSP transferred select samples to GeoTesting Express (GTX) of Acton, Massachusetts for geotechnical laboratory testing in accordance with applicable AASHTO and ASTM testing procedures. The types and numbers of each of the laboratory tests conducted on soil samples and rock

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<sup>4</sup> GRL Engineers, Inc., SPT Energy Calibration on November 2, 2023, Submitted to Eric Baron of S.W. Cole Explorations, LLC (now known as Seaboard Drilling LLC) on November 10, 2023.

core are presented in Table 5-1. Soil testing results are included on the boring logs in Appendix A. Complete soil and rock laboratory testing results are provided in Appendix C.

**Table 5-1: Number and Type of Laboratory Tests Performed**

Laboratory Test	Test Standard	No. Tests Completed
Moisture content	AASHTO T267, ASTM D2216	18
Grain size analysis (coarse)	AASHTO T88, ASTM D6913	37
Grain size (fine)	AASHTO T88, ASTM D7928	12
Atterberg limits	AASHTO T89 / T90, ASTM D4318	11
Chlorides	AASHTO T291, ASTM D512	2
pH	AASHTO T289, ASTM D4972	2
Sulfates	AASHTO T290	2
Electric Resistivity	ASTM G57	1
Elastic Moduli of Rock in Uniaxial Compression - Rock	ASTM D7012 Method D	6

## 6.0 SUBSURFACE CONDITIONS

The boring logs in Appendix A provide detailed descriptions of the soil, bedrock, and measured groundwater conditions encountered in the borings.

**Soils:** The soils encountered in the borings generally consist of fill materials placed during construction of the bridge and roadway and naturally occurring sand deposits, clay deposits, sand and gravel interpreted as glacial till. Table 6-1 summarizes the major stratigraphic units, the range of thicknesses, and generalized material descriptions for soils encountered.

**Table 6-1: Summary of Subsurface Fill and Soil Encountered**

Stratigraphic Unit	Approximate Range in Encountered Thickness (feet)	Generalized Description
Asphalt	0.5 to 0.8	Asphalt pavement approximately 5-inch to 10-inch thick ( <i>Encountered in all borings</i> )
Fill	2.6 to 20	The fill consists of olive brown to brown or grey to brown, dry to moist, medium dense to very dense, hard, fine to coarse Sand or SILT, with trace to little fine to coarse gravel, and non-plastic to slightly plastic. USCS: SM, ML, GM. AASHTO: A-1-b (0), A-4 (0), A-2-4 (0) ( <i>Encountered in all borings</i> )
Sand, Silt, Gravel	1.3 to 22	Olive to brown to grey, moist to wet, medium dense to very dense, very stiff to hard, fine to coarse SAND or SILT with varying amounts of fine to coarse GRAVEL, and non-plastic to slightly

Stratigraphic Unit	Approximate Range in Encountered Thickness (feet)	Generalized Description
		plastic. USCS: SM, ML, GM, SC. AASHTO: A-2-4 (0), A-4 (0) <i>(Encountered in BB-BSA-101, -102, -105, -106, -107, -108, and -109)</i>
Clay	3 to 14.5	Grey with brown and olive, wet, very soft to hard, CLAY, trace to little fine sand, trace gravel, medium plasticity with interbedded silt or sand lenses. USCS: CL. AASHTO: A-6 (9, 10, 11, 15, 18, 19, 37) <i>(Encountered in BB-BSA-104, -106, -107, and -111)</i>
Glacial Till	3 to 10.3	Grey with brown to olive, wet, very dense to hard, fine to coarse SAND and fine to coarse GRAVEL, with varying amounts of silt and gravel, non-plastic, and weathered rock fragments. USCS: SM, GM, ML. AASHTO: A-1-b (0), A-4 (0) <i>(Encountered in BB-BSA-104, -106, -107, and -111)</i>

Notes: USCS classification from laboratory testing in accordance with ASTM D2487. AASHTO classification from laboratory testing and includes Group Classification and Group Index in parentheses in accordance with AASHTO M145.

**Bedrock:** Bedrock was cored for each boring location. Bedrock cores for BB-BSA-104 and BB-BSA-109 were taken at the offset borings BB-BSA-104A and BB-BSA-109A respectively. For the borings performed from Stillwater Avenue, top of bedrock surface ranged from 3.5 feet bgs (EL. 123.5 feet NAVD88) to 12.2 feet bgs (EL. 121.3 feet NAVD88). For the borings performed from I-95, top of bedrock ranged from 17.8 feet bgs (130.5 feet NAVD88) to 63.8 feet bgs (EL. 79.8 feet NAVD88). The bedrock was described as grey, very fine to fine grained, very thinly to thinly bedded, Metawacke [metasandstone] with calcite veins, medium strong to very strong, slightly to moderately weathered.

Rock quality designation (RQD) is a common parameter that is used to help assess the competency of sampled bedrock. RQD is defined as the sum of pieces of recovered bedrock greater than 4 inches in length divided by the total length of the core run. RQD values for bedrock encountered at the site ranges between 0 and 88 percent, which generally correlates to Rock Mass Quality ratings of very poor to good.

**Groundwater:** Groundwater levels were measured in all borings except BB-BSA-104, BB-BSA-104A, and BB-BSA-109. Groundwater was measured before the casing was withdrawn and at the end of the drilling day. Groundwater elevations vary from approximately EL. 123.1 feet to EL. 135.1 feet (NAVD88), ground water levels encountered at the time of drilling may have been influenced by the drilling methods used. Groundwater levels will fluctuate due to soil conditions and topography and seasonal variations in precipitation. Groundwater levels encountered during construction may differ from those recorded from the borings.

## 7.0 CONDITIONS OF EXPOSED ROCK CUTS

Rock Mass Rating (RMR) and Geological Strength Index (GSI) values were calculated for the existing rock cut exposures along Stillwater Avenue and for the rock core collected in each boring for comparison. The RMR system<sup>5</sup> assigns numerical ratings to six parameters, including strength of the intact rock, RQD, discontinuity spacing, discontinuity surface conditions, groundwater conditions, and orientation of discontinuities. These ratings are summed to provide the RMR value. The GSI system<sup>6</sup> assigns a numerical rating to qualitative estimates of the lithology, discontinuity structure, and discontinuity surface conditions in a rock mass.

To determine the RMR, WSP used the discontinuities described in each rock cut exposure or core run and the RQD measured in each core run to assign ratings. We used the discontinuity orientations measured in the rock cuts to assign rating adjustments for the discontinuity sets that we identified as having unfavorable orientations relative to the existing foundation orientation (i.e., kinematically susceptible to sliding or toppling failure). The proposed foundation orientation may allow for a different rating adjustment for discontinuity orientation, and thus a modification to the RMR value. Our calculated RMR values are summarized in Table 2 (attached) for the measured rock cut exposures and Table 3 (attached) for the boring rock core runs. Full RMR calculations including the individual parameter ratings are provided in Appendix D.2. Photographs of the rock cuts evaluated are presented in Appendix E. Based on our field observations and measurements at the Stillwater Avenue bridge site, we estimate that:

- RMR values range from 40 to 79 and average 63 for the exposed rock cuts from 37 discontinuities evaluated.
- RMR values range from 26 to 72 and average 44 for the rock core runs from 30 runs.

To determine the GSI, WSP used the discontinuity structure observed in the existing rock cuts and the discontinuity surface conditions described in the rock cuts and core runs to assign a rating. We selected the GSI value from the range established by Marinos and Hoek<sup>6</sup> for typical sandstone lithologies. The GSI chart is presented in Appendix D.3. Based on our field observations and measurements, we estimate a GSI value of 55 for the exposed rock cuts at the Stillwater Avenue bridge site.

## 8.0 REPORT AND EXPLORATION LIMITATIONS

This Preliminary Geotechnical Data Report (PGDR) was prepared for the replacement of I-95 Bridge No. 1427 & Bridge No. 5800 over Stillwater Ave in Bangor, Maine. The professional services provided by WSP for this project include only the geotechnical aspects of the subsurface conditions at this site. The presence or implications of possible surface and/or subsurface contamination resulting from previous activities or uses of the site and/or resulting from the introduction onto the site of materials from off-site sources are outside the terms of reference for this report and have not been investigated or addressed.

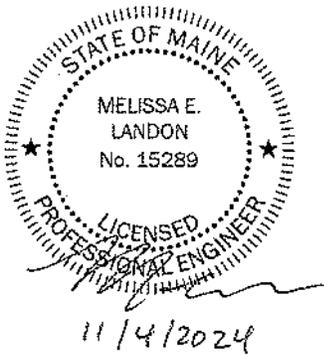
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<sup>5</sup> Bieniawski, Z.T. 1989. Engineering Rock Mass Classifications: A Complete Manual for Engineers and Geologists in Mining, Civil, and Petroleum Engineering. John Wiley & Sons.

<sup>6</sup> Marinos, Paul and Hoek, Evert. November 2000. GSI: a geologically friendly tool for rock mass strength estimation. ISRM International Symposium, Melbourne, Australia, paper number ISRM-IS-2000-035.

# Signature Page

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## TABLES

**Table 1: Summary of Subsurface Explorations  
Geotechnical Data Report  
MaineDOT I-95 Bridge Over Stillwater Avenue, Bangor, Maine  
MaineDOT WIN 027176.00**

	As-Drilled Locations <sup>4</sup>				Approximate Strata Thickness (feet)						Approximate Top of Bedrock Depth (feet bgs <sup>5</sup> )	Approximate Elevation of Top of Bedrock (feet NAVD88)	Approximate Bottom of Exploration Depth (ft) (feet bgs <sup>5</sup> )	Approximate Elevation of Bottom of Exploration (feet NAVD88)
	Test Boring No. <sup>1,2,3</sup>	Northing	Eastings	Ground Surface Elevation <sup>4</sup> (feet NAVD88)	Asphalt	Fill	Sand, Silt, Gravel <sup>6</sup>	Clay	Glacial Till	Weathered Bedrock				
South bound Bridge #1427	BB-BSA-101	482856.27	1735264.27	150.5	0.6	12.9	15.0	NE <sup>5</sup>	3.0	NE <sup>5</sup>	31.5	119.0	41.5	109.0
	BB-BSA-102	482969.08	1735451.57	133.5	0.6	4.4	7.2	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	12.2	121.3	22.2	111.3
	BB-BSA-103	482888.01	1735425.94	132.1	0.6	2.5	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	4.1	7.2	124.9	17.2	114.9
	BB-BSA-104	483018.96	1735602.84	151.9	0.8	14.7	NE <sup>5</sup>	3.0	4.5	NE <sup>5</sup>	23.0	128.9	23.5	128.4
	BB-BSA-104A	483017.59	1735600.99	152.0	0.7	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	20.4	131.6	31.0	121.0
	BB-BSA-105	482984.90	1735593.56	152.1	0.8	12.3	11.9	NE <sup>5</sup>	NE <sup>5</sup>	1.4	26.4	125.7	36.2	115.9
North bound Bridge #5800	BB-BSA-106	482611.20	1735095.82	143.6	0.8	18.2	22.0	12.5	10.3	NE <sup>5</sup>	63.8	79.8	74.1	69.5
	BB-BSA-107	482578.95	1735092.78	143.1	0.5	20.0	18.5	14.5	9.9	NE <sup>5</sup>	63.4	79.7	77.2	65.9
	BB-BSA-108	482749.52	1735322.13	129.5	0.6	2.6	3.5	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	6.7	122.8	16.7	112.8
	BB-BSA-109	482636.37	1735255.48	127.0	0.7	8	1.3	NE <sup>5</sup>	NE <sup>5</sup>	0.1	NE <sup>5</sup>	NE <sup>5</sup>	10.1	116.9
	BB-BSA-109A	482637.93	1735257.73	127.0	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	3.5	123.5	14.0	113.0
	BB-BSA-110	482660.73	1735292.34	127.5	0.6	4.7	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	NE <sup>5</sup>	5.3	122.2	15.3	112.2
	BB-BSA-111	482728.68	1735418.07	148.3	0.6	8.9	NE <sup>5</sup>	4.0	4.3	NE <sup>6</sup>	17.8	130.5	29.0	119.3

Notes:

- Boring locations are shown in Figure 2 - Boring Location Plan of the Preliminary Geotechnical Data Report.
- Borings BB-BSA-102, BB-BSA-103, BB-BSA-108, BB-BSA-109, BB-BSA-109A, and BB-BSA-110 were performed by Seaboard Drilling, LLC in May, 2024. Borings BB-BSA-101, BB-BSA-104, BB-BSA-104A, BB-BSA-105, BB-BSA-106, BB-BSA-107, and BB-BSA-111 were performed by Seaboard Drilling, LLC in July, 2024.
- Boring logs are presented in Appendix A of the Preliminary Geotechnical Data Report.
- As drilled Boring Locations Derived from the Electronic file "Ground.dgn" Provided to WSP by HNTB on August 12, 2024.
- bgs = below ground surface, NE = not encountered
- This layer mainly consists of silty Sand or sandy Silt, but includes Gravel with some sand in borings BB-BSA-102 and BB-BSA-108 strata layers.

Prepared By: RJN  
Checked By: LMP  
Reviewed By: MEL

**Table 2: Summary of Rock Cut Discontinuities**  
**Preliminary Geotechnical Design Report**  
**Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine**  
**MaineDOT WIN 027176.00**

Outcrop Area	Discontinuity		Dip [degrees]	Uncorrected Dip Direction State Plane Grid North [degrees]	Corrected Dip Direction State Plane Grid North <sup>(1)</sup> [degrees]	Set <sup>(2)</sup>	Persistence [ft]	Aperture [in]	Infilling	Infilling Shear Strength <sup>(3)</sup>	Surface Roughness	Discontinuity Shape	Water	Discontinuity Spacing [ft]	Notes/Comments <sup>(4)</sup>	RMR
	ID	Type														
Stillwater Ave Northbound	1	bedding	32	348	333	5	10	0.13	none	-	rough	undulating to stepped	dry	0.2		40
	2	joint	84	229	214	3	15	0.25	lichen	low	slightly rough	planar	dry	1.5		64
	3	joint	88	245	230	3	3	0.50	none	-	slightly rough	planar	dry	2.8		78
	4	joint	85	265	250	2	8	0.25	lichen	low	smooth	planar	dry	0.9		46
	5	joint	11	243	228	1	5	0.13	none	-	smooth	undulating	dry	5.9		78
	6	joint	83	186	171	4	10	0.06	none	-	slightly rough	planar	dry	1.6		72
	7	bedding	25	335	320	5	10	tight	none	-	rough	stepped	dry	0.3		49
	8	joint	8	100	85	1	3	0.50	sandy soil	medium	smooth	planar	dry	5.9		73
	9	joint	75	50	35	3	15	0.06	none	-	slightly rough	planar	dry	1.1	Quartz veins 0.25" thick in vicinity	58
	10	joint	10	58	43	1	20	0.75	quartz	high	slightly rough	planar	dry	1.0		52
	11	joint	64	4	349	-	4	0.75	quartz	high	rough	irregular	dry	3.7		64
	12	joint	83	41	26	3	12	0.06	none	-	slightly rough	planar	dry	4.5		66
	13	joint	65	278	263	2	6	0.13	none	-	slightly rough	stepped	dry	5.4		54
	14	joint	4	48	33	1	10	0.50	quartz	high	slightly rough	undulating	dry	0.9		63
	15	joint	83	133	118	2	5	tight	none	-	smooth	planar	dry	5.1		68
	16	joint	8	124	109	1	10	0.38	broken rock	high	rough	undulating	dry	1.3		67
	17	joint	89	357	342	4	15	0.06	roots	low	slightly rough	undulating	dry	2.5		71
	18	joint	67	213	198	-	15	tight	none	-	smooth	undulating	dry	2.5		78
	19	joint	87	20	5	4	15	0.06	none	-	rough	stepped	dry	1.8		71
	20	joint	88	124	109	2	15	0.25	topsoil	low	slightly rough	planar	dry	1.7		47
	21	bedding	21	26	11	5	6	0.06	none	-	smooth	stepped	dry	0.4		42
	22	joint	80	278	263	2	10	0.13	none	-	slightly rough	planar	dry	1.8	Shotcrete and dowel repair 2 ft north	54
	23	joint	10	111	96	1	22.5	0.25	quartz	high	smooth	planar	dry	2.0		64
	24	joint	18	65	50	1	20	tight	none	-	slightly rough	undulating	dry	1.4		72
	25	joint	85	190	175	4	15	tight	none	-	slightly rough	planar	dry	2.3		79
	26	joint	59	212	197	-	15	1.50	quartz	high	smooth	planar	dry	2.2	Blast fragmentation to south	67
	27	joint	31	106	91	1	10	0.50	roots, topsoil	low	smooth	planar	dry	4.0		68
	28	joint	25	5	350	5	10	0.50	quartz, broken rock	high	rough	undulating	dry	1.8		69
	29	joint	81	10	355	4	10	0.13	broken rock	high	rough	planar	dry	2.2		74
	30	joint	10	220	205	1	24.8	0.50	broken rock	high	slightly rough	planar	dry	1.6		67
	31	joint	84	55	40	3	4.5	0.50	roots, sandy soil	low	slightly rough	planar	dry	2.3		69

**Table 2: Summary of Rock Cut Discontinuities**  
**Preliminary Geotechnical Design Report**  
**Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine**  
**MaineDOT WIN 027176.00**

Outcrop Area	Discontinuity		Dip [degrees]	Uncorrected Dip Direction State Plane Grid North [degrees]	Corrected Dip Direction State Plane Grid North <sup>(1)</sup> [degrees]	Set <sup>(2)</sup>	Persistence [ft]	Aperture [in]	Infilling	Infilling Shear Strength <sup>(3)</sup>	Surface Roughness	Discontinuity Shape	Water	Discontinuity Spacing [ft]	Notes/Comments <sup>(4)</sup>	RMR
	ID	Type														
Stillwater Ave Southbound	32	joint	76	329	314	-	3.9	0.25	sandy soil	medium	very rough	undulating	dry	0.9		66
	33	joint	72	183	168	4	3.5	0.13	sandy soil	medium	rough	planar to stepped	dry	0.2		53
	34	joint	66	278	263	2	-	0.13	sandy soil	medium	very rough	planar	dry	0.3		40
	35	joint	17	62	47	1	9.7	0.50	none	-	rough	undulating	dry	2.0		74
	36	joint	88	219	204	3	2.9	0.13	sandy soil	medium	smooth	planar	dry	0.6		60
	37	joint	89	262	247	2	3.4	0.25	none	-	smooth	stepped	dry	0.4		41

(1) Dip direction data corrected for magnetic declination (15 degrees west).

(2) See Appendix E for stereonet.

(3) Shear strength of infilling materials as follows:

Low = friction angle < 20 degrees

Medium = 20 degrees < friction angle < 30 degrees

High = 30 degrees < friction angle

(4) Discontinuity measurements were collected on April 23, 2024.

Prepared by: KAR

Checked by: BK

Reviewed by: JDL

**Table 3: Summary of Rock Core Quality**  
**Preliminary Geotechnical Design Report**  
**Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine**  
**MaineDOT WIN 027176.00**

Test Boring Designation	Core Size (in)	No.	Midpoint Depth Below Bedrock Surface (ft)	Run			TCR <sup>1</sup>			RQD <sup>2</sup>			Physical Rock Parameters			Lithologic, Rock Mass and Discontinuity Description <sup>5,6</sup>
				Depth Below Ground Surface (ft)			Length (ft)	Length (ft)	%	Length (ft)	%	Designation	Weathering <sup>3</sup>	Estimated Field Strength <sup>3</sup>	Rock Mass Rating [RMR] <sup>4</sup>	
				Start	End	Midpoint	(ft)	(ft)	%	(ft)	%					
BB-BSA-101	NX (1.88)	R1	0.4	31.5	32.4	32.0	0.9	0.8	89%	0.00	0%	Very Poor	Slightly Weathered (W2)	Very Strong (R5)	31	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, very strong, slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, smooth to very rough, tight to open, highly fractured, clay infilling at bottom of run [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	1.2	32.4	32.9	32.7	0.5	0.5	100%	0.00	0%	Very Poor	Slightly Weathered (W2)	Strong (R4) to Very Strong (R5)	30	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], clay and sand infilling at the top of run, strong to very strong, slightly weathered; discontinuities low angle to steep dipping, very close spacing, rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R3	3.2	32.9	36.5	34.7	3.6	3.6	100%	0.50	14%	Very Poor	Slightly Weathered (W2) to Fresh (W1)	Strong (R4) to Very Strong (R5)	39	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, slightly weathered to fresh; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R4	7.5	36.5	41.5	39.0	5.0	5.0	100%	3.00	60%	Fair	Fresh (W1)	Strong (R4)	56	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong, fresh; discontinuities low angle to steep dipping, very close spacing, rough to very rough, tight, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-102	NX (1.88)	R1	2.5	12.2	17.2	14.7	5.0	4.5	90%	2.58	52%	Fair	Slightly Weathered (W2)	Strong (R4) to Extremely Strong (R6)	40	Grey, very fine to fine grained, thinly to thickly laminated, METAWACKE [metasandstone], frequent thin to thick calcite veins, strong to extremely strong, slightly weathered; discontinuities moderately to steeply dipping, close to moderately close spacing, irregular to planar, smooth to very rough, open; average 3.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.5	17.2	22.2	19.7	5.0	4.9	98%	4.38	88%	Good	Fresh (W1)	Extremely Strong (R6)	72	Grey, very fine to fine grained, thinly laminated, METAWACKE [metasandstone], frequent calcite veins, extremely strong, fresh; discontinuities horizontal dipping, close to wide spacing, irregular to planar, smooth to very rough, open; average 0.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].

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				Depth Below Ground Surface (ft)			Length	Length		Length		Designation	Weathering <sup>3</sup>	Estimated Field Strength <sup>3</sup>	Rock Mass Rating [RMR] <sup>4</sup>	
				Start	End	Midpoint	(ft)	(ft)	%	(ft)	%					
BB-BSA-103	NX (1.88)	R1	2.5	7.2	12.2	9.7	5.0	5.0	100%	1.54	31%	Poor	Slightly Weathered (W2)	Extremely Strong (R6)	44	Grey, very fine to fine grained, METAWACKE [metasandstone] with thin calcite veins and thick quartz veins, extremely strong, thinly laminated, slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, stepped to irregular, very rough to smooth, open; average 4.0 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.5	12.2	17.2	14.7	5.0	5.0	100%	3.50	70%	Fair	Fresh (W1)	Extremely Strong (R6)	62	Grey, very fine to fine grained, METAWACKE [metasandstone] with thin calcite and quartz veins, extremely strong, thinly laminated, fresh; discontinuities moderately dipping, close to moderately close spacing, stepped to irregular, rough, open; average 0.8 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-104A	NX (1.88)	R1	3.1	21.0	26.0	23.5	5.0	4.8	95%	2.80	56%	Fair	Slightly Weathered (W2) to Fresh (W1)	Strong (R4) to Very Strong (R5)	41	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, slightly weathered to fresh, clay and sand infilling 22.5 ft to 23 ft; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.0	26.0	28.8	27.4	2.8	2.1	75%	1.70	61%	Fair	Fresh (W1)	Strong (R4) to Very Strong (R5)	58	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, fresh; discontinuities low angle to moderate dipping, very close spacing, rough to very rough, tight, average 0.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R3	9.5	28.8	31.0	29.9	2.2	2.0	91%	0.50	23%	Very Poor	Fresh (W1)	Strong (R4) to Very Strong (R5)	41	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], strong to very strong, fresh; discontinuities low angle to steep dipping, very close spacing, rough, tight to open, average 3.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-105	NX (1.88)	R1	2.5	26.4	31.4	28.9	5.0	5.0	100%	1.50	30%	Poor	Slightly Weathered (W2) to Fresh (W1)	Strong (R4)	41	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong, slightly weathered to fresh; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.4	31.4	36.2	33.8	4.8	4.8	100%	3.60	75%	Fair	Fresh (W1)	Very Strong (R5)	58	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, very strong, fresh; discontinuities low angle to steep dipping, very close spacing, smooth to rough, tight, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].

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				Depth Below Ground Surface (ft)			Length (ft)	Length (ft)	%	Length (ft)	%	Designation	Weathering <sup>3</sup>	Estimated Field Strength <sup>3</sup>	Rock Mass Rating [RMR] <sup>4</sup>	
				Start	End	Midpoint										
BB-BSA-106	NX (1.88)	R1	0.5	63.8	64.8	64.3	1.0	0.3	30%	0.00	0%	Very Poor	Slightly Weathered (W2) to Fresh (W1)	Strong (R4) to Very Strong (R5)	36	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, slightly weathered to fresh; discontinuities low angle dipping, very close to close spacing, rough to very rough, tight to open [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	3.1	64.8	69.1	67.0	4.3	4.3	100%	2.00	47%	Poor	Fresh (W1)	Strong (R4) to Very Strong (R5)	35	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, fresh with chemical weathering 67.4 ft to 68.3 ft, sand infilling 67.9 ft to 68.3 ft; discontinuities low angle to vertical dipping, very close to close spacing, smooth to rough, tight to open, average 3.3 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R3	7.8	69.1	74.1	71.6	5.0	5.0	100%	3.10	62%	Fair	Fresh (W1)	Weak (R2)	45	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, weak, fresh; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 1.4 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-107	NX (1.88)	R1	2.3	63.4	67.2	65.3	3.8	0.6	16%	0.00	0%	Very Poor	Highly Weathered (W4)	Strong (R4)	26	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], strong, highly weathered with clay and sand infilling from 64.2 ft to 67.2; discontinuities low angle to steep dipping, close spacing, rough to very rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	4.7	67.2	68.2	67.7	1.0	0.2	17%	0.00	0%	Very Poor	Highly Weathered (W4)	Strong (R4)	27	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], strong, highly weathered with clay and sand infilling; discontinuities low angle dipping, close spacing, very rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R3	7.2	68.2	72.2	70.2	4.0	3.8	95%	1.41	35%	Poor	Slightly Weathered (W2)	Strong (R4) to Very Strong (R5)	36	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, slightly weathered, occasional moderate to severe chemical weathering with sand infilling; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R4	11.7	72.2	77.2	74.7	5.0	5.0	100%	1.96	39%	Poor	Slightly Weathered (W2)	Strong (R4) to Very Strong (R5)	36	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, slightly weathered, occasional moderate to severe chemical weathering with sand and clay infilling; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].

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				Depth Below Ground Surface (ft)				Length (ft)	%	Length (ft)	%	Designation	Weathering <sup>3</sup>	Estimated Field Strength <sup>3</sup>	Rock Mass Rating [RMR] <sup>4</sup>	
				Start	End	Midpoint										
BB-BSA-108	NX (1.88)	R1	2.5	6.7	11.7	9.2	5.0	4.9	98%	2.92	58%	Fair	Slightly Weathered (W2)	Very Strong (R5) to Extremely Strong (R6)	51	Grey, very fine to fine grained, METAWACKE [metasandstone] with frequent calcite veins, very to extremely strong, thinly laminated, slightly weathered; discontinuities moderate to steep dipping, close to moderately close spacing, rough to polished, open; average 2.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	5.5	11.7	12.7	12.2	1.0	0.9	92%	0.42	42%	Poor	Slightly Weathered (W2) to Fresh (W1)	Extremely Strong (R6)	51	Grey, very fine to fine grained, METAWACKE [metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open; average 1.0 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R3	7.0	12.7	14.7	13.7	2.0	1.8	88%	0.33	17%	Very Poor	Slightly Weathered (W2) to Fresh (W1)	Extremely Strong (R6)	45	Grey, very fine to fine grained, METAWACKE [metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open; average 2.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R4	9.0	14.7	16.7	15.7	2.0	1.9	96%	0.71	35%	Poor	Slightly Weathered (W2) to Fresh (W1)	Extremely Strong (R6)	48	Grey, very fine to fine grained, METAWACKE [metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open; average 2.0 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-109A	NX (1.88)	R1	2.9	4.0	8.8	6.4	4.8	4.6	95%	1.42	30%	Poor	Slightly Weathered (W2) to Fresh (W1)	Very Strong (R5) to Extremely Strong (R6)	43	Grey, very fine grained, METAWACKE [metasandstone] with frequent calcite veins, very to extremely strong, thinly laminated, fresh to slightly weathered; discontinuities steep dipping, close spacing, planar to stepped, rough to smooth, open; average 2.1 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.9	8.8	14.0	11.4	5.2	5.1	99%	2.54	49%	Poor	Fresh (W1)	Very Strong (R5) to Extremely Strong (R6)	49	Grey, very fine grained, METAWACKE [metasandstone] with frequent calcite veins (0.1 to 0.7 in thick), very to extremely strong, thinly laminated, fresh; discontinuities low angle to steep dipping, very close to moderately close spacing, planar to stepped, rough to smooth, open; average 1.8 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-110	NX (1.88)	R1	2.5	5.3	10.3	7.8	5.0	4.8	95%	2.46	49%	Poor	Fresh (W1)	Medium Strong (R3)	43	Grey, very fine grained, METAWACKE [metasandstone] with frequent thick and thin calcite veins, medium strong, thinly laminated, fresh; discontinuities horizontal to steep dipping, close to moderately close spacing, stepped, smooth to polished, open; average 1.0 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.5	10.3	15.3	12.8	5.0	5.0	100%	3.54	71%	Fair	Fresh (W1)	Very Strong (R5) to Extremely Strong (R6)	54	Grey, very fine grained, METAWACKE [metasandstone] with frequent thick and thin calcite veins, very to extremely strong, thinly laminated, fresh; discontinuities steep dipping, close to wide spacing, stepped, smooth, open; average 0.8 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].

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				Depth Below Ground Surface (ft)			Length (ft)	Length (ft)	%	Length (ft)	%	Designation	Weathering <sup>3</sup>	Estimated Field Strength <sup>3</sup>		Rock Mass Rating [RMR] <sup>4</sup>
				Start	End	Midpoint										
BB-BSA-111	NX (1.88)	R1	3.7	19.0	24.0	21.5	5.0	3.4	68%	0.75	15%	Very Poor	Slightly Weathered (W2)	Strong (R4) to Very Strong (R5)	37	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, slightly weathered with signs of chemical weathering; discontinuities low angle to steep dipping, close to very close spacing, rough to very rough, open to tight, highly fractured average from 19 ft to 21.3 ft [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	8.7	24.0	29.0	26.5	5.0	5.0	100%	3.00	60%	Fair	Fresh (W1)	Strong (R4) to Very Strong (R5)	54	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, fresh; discontinuities low angle dipping, very close spacing, rough, tight, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].

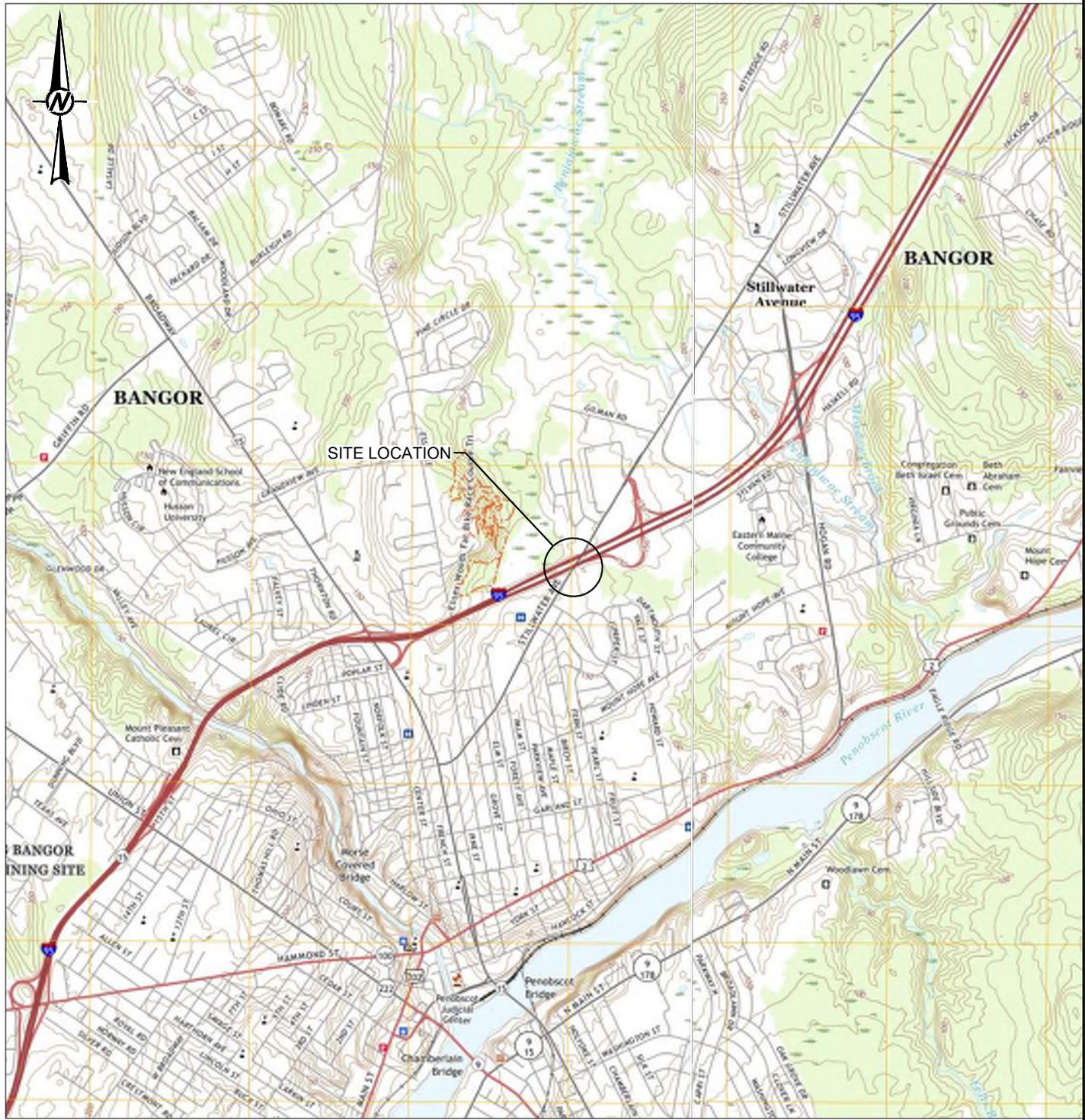
**Notes:**

1. TCR = total core recovery. Total core recovery is the length of core recovered divided by the length of the run.
2. RQD = rock quality designation. RQD is the total length of intact, full diameter core pieces recovered with a length greater than or equal to 4 inches measured along the core axis. The percent RQD is the total length of RQD measured divided by the run length. Note that vertical discontinuities are not included in determination of RQD.
3. Weathering and Estimated Field Strength based on Tables II.4 and II.3 (respectively) in Wyllie and Mah, 2004, Rock Slope Engineering: Civil and Mining, 4th Edition (based on ISRM, 1981).
4. Rock Mass Rating (RMR) System (Bieniawski, 1989) assigns numerical ratings to six parameters, including the strength of the intact rock, the RQD, the discontinuity spacing, groundwater conditions, and orientation of discontinuities. These ratings are summed to provide the RMR value. The rating adjustment for joint orientation was assigned a value of -4, which is the average of the orientation adjustments obtained from geologic field mapping of the exposed rock outcrops and which is based on the existing rock cut orientation. The proposed foundation orientation may allow for a different rating adjustment for joint orientation, and thus a modification to the RMR value shown on this table.
5. Bedrock formation name from: Pollock, Stephen G. 2011. Bedrock geology of the Bangor Quadrangle, Maine. Maine Geological Survey Open-File No. 11-57. Map scale 1:24,000.
6. ft = feet, in = inches

Prepared by: KAR  
 Checked by: BK  
 Reviewed by: JDL

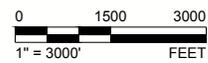
## FIGURES

Last Edited By: usam701004 Date: 2024-08-14 Time: 9:49:43 AM | Printed By: USAM701004 Date: 2024-08-14 Time: 9:54:44 AM  
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**REFERENCE(S)**

1. BASE MAP TAKEN FROM U.S.G.S. 7.5 MINUTE QUADRANGLES OF BANGOR AND VEAZIE, MAINE DATED 2021



CLIENT  
**MAINE DEPARTMENT OF TRANSPORTATION**

PROJECT  
**DESIGN BUILD PHASE I  
 I-95 BRIDGE NO. 1427 & 5800 OVER STILLWATER AVENUE  
 BANGOR, ME (WIN 027176.00)**

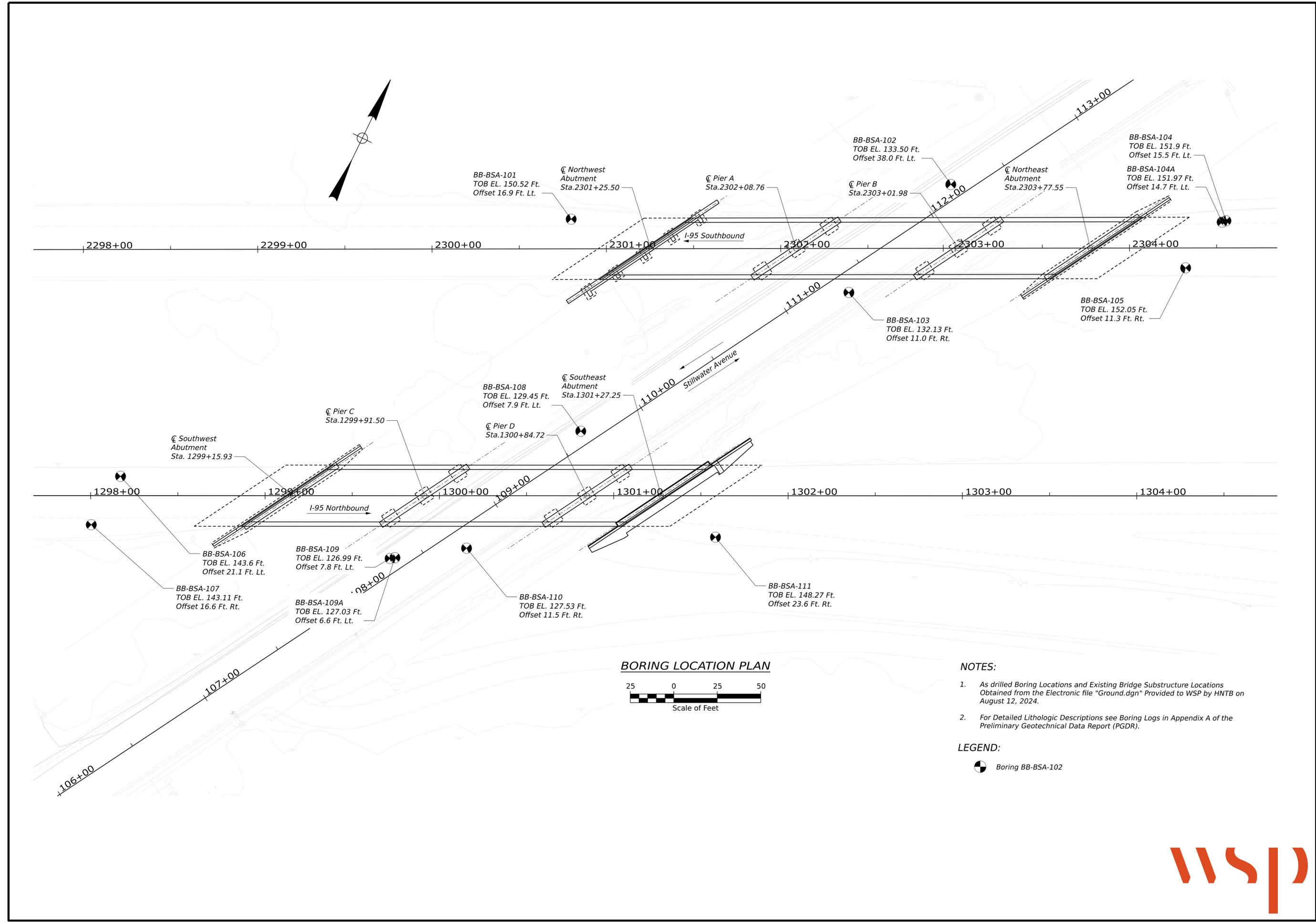
CONSULTANT	YYYY-MM-DD	2024-08-14
	DESIGNED	DEB
	PREPARED	AM
	REVIEWED	
	APPROVED	

TITLE	PROJECT NO.	CONTROL	REV.	FIGURE
<b>SITE LOCATION MAP</b>	US025840.3905	0001-001	0	1

IF THIS MEASUREMENT DOES NOT MATCH WHAT IS SHOWN, THE SHEET SIZE HAS BEEN MODIFIED FROM ANSI A

Date: 9/13/2024

Username: gomeznl



STATE OF MAINE  
DEPARTMENT OF TRANSPORTATION

027176.00

WIN  
027176.00  
BRIDGE PLANS

PROJ. MANAGER	BY	DATE

SIGNATURE	P.E. NUMBER	DATE

BANGOR PENOBSKOT COUNTY  
I-95 NB & SB OVER STILLWATER AVE

BORING LOCATION PLAN

SHEET NUMBER

02

OF 02



**APPENDIX A**

**Boring Logs**



**Table A-2****Classification of Rock Material Strengths<sup>1</sup>**

Grade	Description	Field Identification	Approx. Range of Uniaxial Compressive Strength	
			MPa	psi
S1	Very soft clay	Easily penetrated several inches by fist	<0.025	<4
S2	Soft clay	Easily penetrated several inches by thumb	0.025-0.05	4-7
S3	Firm clay	Can be penetrated several inches by thumb with moderate effort	0.05-0.10	7-15
S4	Stiff clay	Readily indented by thumb but penetrated only with great effort	0.10-0.25	15-35
S5	Very stiff clay	Readily indented by thumbnail	0.25-0.50	35-70
S6	Hard clay	Indented with difficulty by thumbnail	>0.50	>70
R0	Extremely weak rock	Indented by thumbnail	0.25-1.0	35-150
R1	Very weak rock	Crumbles under firm blows with point of geological hammer; can be peeled by a pocket knife	1-5	150-725
R2	Weak rock	Can be peeled by a pocket knife with difficulty; shallow indentations made by firm blow with point of geological hammer	5-25	725-3,500
R3	Medium strong rock	Cannot be scraped or peeled with a pocket knife; specimen can be fractured with single firm blow of geological hammer	25-50	3,500-7,000
R4	Strong rock	Specimen requires more than one blow of geological hammer to fracture it	50-100	7,000-15,000
R5	Very strong rock	Specimen requires many blows of geological hammer to fracture it	100-250	15,000-36,000
R6	Extremely strong rock	Specimen can only be chipped with geological hammer	>250	>36,000

*Note:* Grades S1 to S6 apply to cohesive soils, for example clays, silty clays, and combinations of silts and clays with sand, generally slow draining. Discontinuity wall strength will generally be characterized by grades R0-R6 (rock) while S1-S6 (clay) will generally apply to filled discontinuities.

<sup>1</sup> International Society for Rock Mechanics (ISRM), Commission on standardization of laboratory and field tests (1978): Suggested methods for the quantitative description of discontinuities in rock masses. Int. J. Rock Mech. Min. Sci. & Geomech. Abstr., Vol. 15, No. 6, pp. 319-368.

<b>Driller:</b> Seaboard  <b>Operator:</b> Ryan H.	<b>Elevation (ft.):</b> 150.52  <b>Datum:</b> Maine East Zone	<b>Auger ID/OD:</b>  <b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> D. Burgess	<b>Rig Type:</b> Diedrich D-50	<b>Hammer Wt./Fall:</b> 140lb/30in
<b>Date Start/Finish:</b> 7/29/24 (21:00); 7/30/24 (3:15)	<b>Drilling Method:</b> SSA, Drive & Wash	<b>Core Barrel:</b> NQ/NX
<b>Boring Location:</b> N: 482856.27, E: 1735264.27	<b>Casing ID/OD:</b> 4" (ID)	<b>Water Level*:</b> 24.8' at 1:47 7/30/24

**Hammer Efficiency Factor:** 1.087      **Hammer Type:** Automatic     Hydraulic     Rope & Cathead

Definitions:      R = Rock Core Sample       $S_u$  = Peak/Remolded Field Vane Undrained Shear Strength (psf)       $T_v$  = Pocket Torvane Shear Strength (psf)  
 D = Split Spoon Sample      SSA = Solid Stem Auger       $S_{u(lab)}$  = Lab Vane Undrained Shear Strength (psf)      WC = Water Content, percent  
 MD = Unsuccessful Split Spoon Sample Attempt      HSA = Hollow Stem Auger       $q_p$  = Unconfined Compressive Strength (ksf)      LL = Liquid Limit  
 U = Thin Wall Tube Sample      RC = Roller Cone      N-uncorrected = Raw Field SPT N-value      PL = Plastic Limit  
 MU = Unsuccessful Thin Wall Tube Sample Attempt      WOH = Weight of 140lb. Hammer      Hammer Efficiency Factor = Rig Specific Annual Calibration Value      PI = Plasticity Index  
 V = Field Vane Shear Test, PP = Pocket Penetrometer      WOR/C = Weight of Rods or Casing       $N_{60}$  = SPT N-uncorrected Corrected for Hammer Efficiency      G = Grain Size Analysis  
 MV = Unsuccessful Field Vane Shear Test Attempt      WO1P = Weight of One Person       $N_{60}$  = (Hammer Efficiency Factor/60%)\*N-uncorrected      C = Consolidation Test

Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.	
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	$N_{60}$	Casing Blows					
0	1D	24/15	0.70 - 2.70	12-12-12-11	24	43	SSA	149.9		Fines = 16.8% A-1-b (0), SM		
	2D	24/22	2.70 - 4.70	10-21-21-21	42	76					Olive with brown, dry, hard, SILT, some fine to coarse gravel, little fine to coarse sand, non-plastic (FILL).	
5	3D	24/22	5.00 - 7.00	15-28-43-42	71	129					Olive with brown, dry, hard, SILT, some fine to coarse gravel, little fine to coarse sand, non-plastic (FILL).	WC = 11.1% Fines = 52.2% A-4 (0), ML
	4D	24/22	7.00 - 9.00	24-16-26-39	42	76					Olive with brown, dry to moist (becomes moist at 8.9' bgs), hard, SILT, some fine to coarse sand, little fine to coarse gravel, non-plastic (FILL).	
10	5D	24/22	10.00 - 12.00	11-13-16-17	29	53	182				Olive with brown, moist, hard, SILT, some fine to coarse sand, little fine to coarse gravel, non-plastic (FILL).	WC = 10.7% Fines = 28.8% A-2-4 (0), SM-GM
							171					
							142					WC = 9.6% Fines = 17.5% A-1-b (0), GM-SM
							85					
15	6D	22/6	15.00 - 16.83	16-16-10-22	26	47	OPEN				Olive brown, moist, dense, fine to coarse SAND, some fine to coarse gravel, some silt (SILTY SAND and GRAVEL)	
							53				Olive brown, moist, dense, fine to coarse SAND, some fine to coarse gravel, some silt (SILTY SAND and GRAVEL)	
20	7D	24/9	20.00 - 22.00	13-22-30-30	52	94			Brown, wet, very dense, fine to medium SAND, some fine gravel, some silt (SILTY SAND WITH GRAVEL)			
									Increased roller bit resistance			
25	8D	24/6	25.00 - 27.00	29-33-34-23	67	121			Dark grayish brown, wet, very dense, fine to coarse SANDY GRAVEL, little silt (SANDY GRAVEL)			
30												

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level reading taken on 7/30/24 at 1:47 am was made after the rock coring.

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-101				
Driller: Seaboard				Elevation (ft.): 150.52		Auger ID/OD:				
Operator: Ryan H.				Datum: Maine East Zone		Sampler: Standard Split Spoon				
Logged By: D. Burgess				Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in				
Date Start/Finish: 7/29/24 (21:00); 7/30/24 (3:15)				Drilling Method: SSA, Drive & Wash		Core Barrel: NQ/NX				
Boring Location: N: 482856.27, E: 1735264.27				Casing ID/OD: 4" (ID)		Water Level*: 24.8' at 1:47 7/30/24				
Hammer Efficiency Factor: 1.087				Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>						
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt				R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person		S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u</sub> (lab) = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected				
T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test										
Depth (ft.)	Sample Information							Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows			
30	9D	8/3	30.00 - 30.67	50/3"	R			119.0	Grey, wet, hard, SILT, some fine to coarse sand, some fine to coarse gravel, trace clay, fractured rock fragments (GLACIAL TILL)	
	R-1	10.8/9.6	31.50 - 32.40	RQD = 0%			NQ/NX			
	R-2	6/6	32.40 - 32.90	RQD = 0%						
	R-3	43.2/43.2	32.90 - 36.50	RQD = 14%						
35										
	R-4	60/60	36.50 - 41.50	RQD = 60%						
40								109.0	Bedrock encountered at 31.5 feet bgs Top of Bedrock Elev. 119.0 ft R1 (31.5' - 32.4'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, very strong, slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, smooth to very rough, tight to open, highly fractured, clay infilling at bottom of run [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 89% recovery 0% RQD Rock Core Rate (min:sec) 31.5 - 32.4 ft (3:01)	
45										
50										
55										
60										
<b>Remarks:</b> 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023. 2. As-drilled boring locations and ground surface elevations were provided by HNTB. 3. Water level reading taken on 7/30/24 at 1:47 am was made after the rock coring.										
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.								Page 2 of 3		
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.								Boring No.: BB-BSA-101		

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-101 <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard <b>Operator:</b> Ryan H. <b>Logged By:</b> D. Burgess <b>Date Start/Finish:</b> 7/29/24 (21:00); 7/30/24 (3:15) <b>Boring Location:</b> N: 482856.27, E: 1735264.27	<b>Elevation (ft.):</b> 150.52 <b>Datum:</b> Maine East Zone <b>Rig Type:</b> Diedrich D-50 <b>Drilling Method:</b> SSA, Drive & Wash <b>Casing ID/OD:</b> 4" (ID)	<b>Auger ID/OD:</b> <b>Sampler:</b> Standard Split Spoon <b>Hammer Wt./Fall:</b> 140lb/30in <b>Core Barrel:</b> NQ/NX <b>Water Level*:</b> 24.8' at 1:47 7/30/24
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<b>Hammer Efficiency Factor:</b> 1.087	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected

Depth (ft.)	Sample Information									Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows	Elevation (ft.)				
60											36.5 - 37.5 ft (3:04) 37.5 - 38.5 ft (3:24) 38.5 - 39.5 ft (3:32) 39.5 - 40.5 ft (4:40) 40.5 - 41.5 ft (4:44)	
65											41.5-	
70											<b>Bottom of Exploration at 41.5 feet below ground surface.</b> Boring backfilled with bentonite chips in the rock core socket, drill cuttings and gravel to bottom of pavement and patched with cold patch asphalt.	
75												
80												
85												
90												

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level reading taken on 7/30/24 at 1:47 am was made after the rock coring.

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-102  <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard	<b>Elevation (ft.):</b> 133.5	<b>Auger ID/OD:</b>
<b>Operator:</b> Kevin Hanscom	<b>Datum:</b> Maine East Zone	<b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> Lina-Maria Pua	<b>Rig Type:</b> Diedrich D-50	<b>Hammer Wt./Fall:</b> 140 lbs/30 in
<b>Date Start/Finish:</b> 05/07/24 (23:53); 05/08/24 (02:12)	<b>Drilling Method:</b> SSA, Cased Wash	<b>Core Barrel:</b> NX
<b>Boring Location:</b> N: 482969.08, E: 1735451.57	<b>Casing ID/OD:</b> 3 in/3.25 in	<b>Water Level*:</b> 9.3 ft on 05/08/24 at 01:59

<b>Hammer Efficiency Factor:</b> 1.066	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person
	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
	T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test

Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows				
0								132.9	7.5" Asphalt Pavement		
	1D	24/11.5	1.00 - 3.00	14-13-20-38	33	59			Brown, moist, very dense, fine to medium SAND, some fine gravel, little silt (FILL).	WC = 3.7% Fines = 14.0% A-1-b(0), SM	
	2D	24/12	3.00 - 5.00	15-24-12-43	36	64			Brown, dry to moist, very dense, medium to fine SILTY SAND, some fine gravel, non-plastic (FILL). q <sub>p</sub> > 0.9ksf	WC = 8.6% Fines = 38.0% A-4 (0), SM	
5	3D	24/11	5.00 - 7.00	47-22-10-12	32	57	40	128.5	Brown to yellow, moist to wet, hard, SILT, some sand, trace gravel, nonplastic to low plasticity (SANDY SILT).		
	4D	24/12	7.00 - 9.00	15-14-9-39	23	41	45		Brown to yellow, wet, hard, SANDY SILT, trace fine gravel, non-plastic to low plasticity (SANDY SILT). q <sub>p</sub> = 0.8ksf, 0.9ksf	Fines = 50.2% A-4 (0), ML	
10	5D	24/5	9.00 - 11.00	69-34-27-13	61	108	36	124.5	Brown to yellow, wet, very dense, fine to coarse GRAVEL, some fine to coarse sand, some silt, low to medium plasticity (GRAVEL)	WC = 15.5% Fines = 25.6% A-2-4 (0), GM	
	R1	60/54	12.20 - 17.20	RQD = 73%			135	121.3	Bedrock encountered at 12.2 feet bgs Top of Bedrock at Elev. 121.3 ft. R1 (12.2'-17.2'): Grey, very fine to fine grained, thinly to thickly laminated, METAWACKE [metasandstone], frequent thin to thick calcite veins, strong to extremely strong, slightly weathered; discontinuities moderately to steeply dipping, close to moderately close spacing, irregular to planar, smooth to very rough, open; average 3.2 fractures per foot, chemical weathering in joints [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = Fair 90% Recovery Rock Core Rate (min:sec) 12.2-13.2 ft (2:24) 13.2-14.2 ft (3:05) 14.2-15.2 ft (3:17) 15.2-16.2 ft (3:03) 16.2-17.2 ft (3:19)		
15											
	R2	60/59	17.20 - 22.20	RQD = 98%				111.3	R2 (17.2'-22.2'): Grey, very fine to fine grained, thinly laminated, METAWACKE [metasandstone], frequent calcite veins, extremely strong, fresh; discontinuities horizontal dipping, close to wide spacing, irregular to planar, smooth to very rough, open; average 0.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = Fair 98% Recovery Rock Core Rate (min:sec) 17.2-18.2 ft (2:54) 18.2-19.2 ft (3:07) 19.2-20.2 ft (2:48) 20.2-21.2 ft (3:15)		

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level reading taken on 5/8/24 at 01:59 was made 15 minutes after completion of drilling with bottom of casing at 12.2 ft bgs.

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-102 <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard <b>Operator:</b> Kevin Hanscom <b>Logged By:</b> Lina-Maria Pua <b>Date Start/Finish:</b> 05/07/24 (23:53); 05/08/24 (02:12) <b>Boring Location:</b> N: 482969.08, E: 1735451.57	<b>Elevation (ft.):</b> 133.5 <b>Datum:</b> Maine East Zone <b>Rig Type:</b> Diedrich D-50 <b>Drilling Method:</b> SSA, Cased Wash <b>Casing ID/OD:</b> 3 in/3.25 in	<b>Auger ID/OD:</b> <b>Sampler:</b> Standard Split Spoon <b>Hammer Wt./Fall:</b> 140 lbs/30 in <b>Core Barrel:</b> NX <b>Water Level*:</b> 9.3 ft on 05/08/24 at 01:59
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<b>Hammer Efficiency Factor:</b> 1.066	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test		

Depth (ft.)	Sample Information									Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows	Elevation (ft.)				
30											21.2-22.2 ft (3:31)	
											22.2	
											<b>Bottom of Exploration at 22.2 feet below ground surface.</b> Boring backfilled with bentonite chips in the rock core socket, gravel to bottom of pavement and patched with cold patch asphalt.	
35												
40												
45												
50												
55												
60												

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level reading taken on 5/8/24 at 01:59 was made 15 minutes after completion of drilling with bottom of casing at 12.2 ft bgs.

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-103  <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard  <b>Operator:</b> Kevin Hanscom  <b>Logged By:</b> Lina-Maria Pua  <b>Date Start/Finish:</b> 05/08/24 (21:32); 05/08/24 (23:30)	<b>Elevation (ft.):</b> 132.13  <b>Datum:</b> Maine East Zone  <b>Rig Type:</b> Diedrich D-50  <b>Drilling Method:</b> SSA, Cased Wash  <b>Casing ID/OD:</b> 3 in/3.25 in	<b>Auger ID/OD:</b>  <b>Sampler:</b> Standard Split Spoon  <b>Hammer Wt./Fall:</b> 140 lbs/30 in  <b>Core Barrel:</b> NX  <b>Water Level*:</b> 5.2 ft on 05/08/24 at 23:14
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<b>Hammer Efficiency Factor:</b> 1.066	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u</sub> (lab) = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test		

Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows				
0								131.5	Asphalt Pavement	-0.6	
	1D	24/16	1.00 - 3.00	21-24-21-21	45	80			Brown, dry, dense, SILTY GRAVEL, some sand, poorly-graded (FILL).		
	2D	24/12	3.00 - 5.00	7-10-6-48	16	28		129.0	2DA, Top 1 in: Brown, dry, medium dense, SILTY GRAVEL, some sand, poorly-graded (FILL).	-3.1	
5	3D	26.4/15.5	5.00 - 7.20	45-34-45-50/4"	79	140			2DB, Bottom 11 in: Grey, dry, medium dense, angular GRAVEL, some weathered rock fragments (WEATHERED BEDROCK). Grey, moist to wet, very dense, WEATHERED BEDROCK, some silt, little sand (WEATHERED BEDROCK).	-7.2	
	R1	60/60	7.20 - 12.20	RQD = 31%				124.9	Bedrock encountered at 7.2 feet bgs Top of Bedrock at Elev. 124.9 ft R1 (7.2'-12.2'): Grey, very fine to fine grained, METAWACKE [metasandstone] with thin calcite veins and thick quartz veins, extremely strong, thinly laminated, slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, stepped to irregular, very rough to smooth, open. average 4.0 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 100% Recovery Rock Core Rate (min:sec) 7.2-8.2 ft (4:32) 8.2-9.2 ft (4:43) 9.2-10.2 ft (5:32) 10.2-11.2 ft (5:50) 11.2-12.2 ft (6:37)	-7.2	
10									R2 (12.2'-17.2'): Grey, very fine to fine grained, METAWACKE [metasandstone] with thin calcite and quartz veins, extremely strong, thinly laminated, fresh; discontinuities moderately dipping, close to moderately close spacing, stepped to irregular, rough, open, average 0.8 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = Excellent 100% Recovery	-17.2	
15	R2	60/60	12.20 - 17.20	RQD = 71%				114.9	<b>Bottom of Exploration at 17.2 feet below ground surface.</b> Boring backfilled with bentonite chips in the rock core socket, gravel to bottom of pavement and patched with cold patch asphalt.	-17.2	
20											
25											
30											

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by MaineDOT.
- Water level reading taken on 5/8/24 at 23:14 was made after completion of drilling with bottom of casing at 7.2 ft bgs.



<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-104A  <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard	<b>Elevation (ft.):</b> 151.97	<b>Auger ID/OD:</b>
<b>Operator:</b> Ryan H.	<b>Datum:</b> Maine East Zone	<b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> D. Burgess	<b>Rig Type:</b> DieDrich D-50	<b>Hammer Wt./Fall:</b> 140lb/30in
<b>Date Start/Finish:</b> 7/30/24 (23:40); 7/31/24 (2:33)	<b>Drilling Method:</b> SSA, Drive & Wash	<b>Core Barrel:</b> NX
<b>Boring Location:</b> N: 483017.59, E: 1735600.99	<b>Casing ID/OD:</b> 4" (ID)	<b>Water Level*:</b> Not measured

<b>Hammer Efficiency Factor:</b> NA	<b>Hammer Type:</b> Automatic <input type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test		

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows /6 in. Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows					
0								SSA	151.3		8" Asphalt pavement	
5												
10												
15												
20												
	R-1	60/57	21.00 - 26.00	RQD = 56%								
25												
	R-2	33.6/25.2	26.00 - 28.80	RQD = 61%								
	R-3	26.4/24	28.80 - 31.00	RQD = 23%								
30												

**Remarks:**

1. As-drilled boring locations and ground surface elevations were provided by HNTB.

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-104A <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard	<b>Elevation (ft.):</b> 151.97	<b>Auger ID/OD:</b>
<b>Operator:</b> Ryan H.	<b>Datum:</b> Maine East Zone	<b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> D. Burgess	<b>Rig Type:</b> DieDrich D-50	<b>Hammer Wt./Fall:</b> 140lb/30in
<b>Date Start/Finish:</b> 7/30/24 (23:40); 7/31/24 (2:33)	<b>Drilling Method:</b> SSA, Drive & Wash	<b>Core Barrel:</b> NX
<b>Boring Location:</b> N: 483017.59, E: 1735600.99	<b>Casing ID/OD:</b> 4" (ID)	<b>Water Level*:</b> Not measured

<b>Hammer Efficiency Factor:</b> NA	<b>Hammer Type:</b> Automatic <input type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person
	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
	T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test

Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in. Shear Strength (psf) or RQD (%))	N-uncorrected	N <sub>60</sub>	Casing Blows				
30								121.0		23.0 - 24.0 ft (2:08) 24.0 - 25.0 ft (2:14) 25.0 - 26.0 ft (2:50) R2 (26.0' - 28.8'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, fresh; discontinuities low angle to moderate dipping, very close spacing, rough to very rough, tight, average 0.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = fair 75% recovery 61% RQD Rock Core Rate (min:sec) 26.0 - 27.0 ft (2:19) 27.0 - 28.0 ft (2:28) 28.0 - 28.8 ft (0:15)	
35										R3 (28.8' - 31.0'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] strong to very strong, fresh; discontinuities low angle to steep dipping, very close spacing, rough, tight to open, average 3.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 91% recovery 23% RQD Rock Core Rate (min:sec) 28.8 - 29.0 ft (0:08) 29.0 - 30.0 ft (2:56) 30.0 - 31.0 ft (3:18)	
40										<b>Bottom of Exploration at 31.0 feet below ground surface.</b> Boring backfilled with bentonite chips in the rock core socket, drill cuttings and gravel to bottom of pavement and patched with cold patch asphalt.	
45											
50											
55											
60											

**Remarks:**

- As-drilled boring locations and ground surface elevations were provided by HNTB.

<b>Driller:</b> Seaboard <b>Operator:</b> Ryan H. <b>Logged By:</b> D. Burgess <b>Date Start/Finish:</b> 7/31/24 (20:07); 8/1/24 (0:30) <b>Boring Location:</b> N: 482984.9, E: 1735593.56	<b>Elevation (ft.):</b> 152.05 <b>Datum:</b> Maine East Zone <b>Rig Type:</b> Diedrich D-50 <b>Drilling Method:</b> SSA, Cased Wash <b>Casing ID/OD:</b>	<b>Auger ID/OD:</b> <b>Sampler:</b> Standard Split Spoon <b>Hammer Wt./Fall:</b> 140lb/30in <b>Core Barrel:</b> NX <b>Water Level*:</b> 17.0' BGS 11:56 7/31/24
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<b>Hammer Efficiency Factor:</b> 1.087	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test		

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows					
0	1D	24/18	0.90 - 2.90	14-14-15-14	29	53	SSA	151.2		10" Asphalt pavement.	Fines = 16.2% A-1-b (0), SM	
								0.8		Olive brown, dry, very dense, fine to coarse SAND, some fine to coarse gravel, little silt (FILL).		
	2D	24/19	2.90 - 4.90	9-11-13-12	24	43					Olive with brown, dry, hard, SILT, some fine to coarse sand, some fine to coarse gravel, non- plastic (FILL).	Fines = 46.4% A-4 (0), ML/SM
5											Dark grayish brown, dry, hard, SANDY SILT, trace gravel (FILL).	
	3D	8/8	5.00 - 5.67	11-50/2"	R						Dark grayish brown, dry, hard, SANDY SILT, trace gravel (FILL).	Fines = 46.4% A-4 (0), ML/SM
	4D	24/10	7.00 - 9.00	13-23-20-16	43	78					Dark grayish brown, dry, hard, SANDY SILT, trace gravel (FILL).	Fines = 46.4% A-4 (0), ML/SM
10											Dark grayish brown, dry, hard, SANDY SILT, trace gravel (FILL).	Fines = 46.4% A-4 (0), ML/SM
	5D	13.5/7	10.00 - 11.13	11-31-50/1.5"	R			35				
								67				Fines = 46.4% A-4 (0), ML/SM
								40				
								57				Fines = 46.4% A-4 (0), ML/SM
								45				
15										Grayish brown, wet, medium dense, SILT, some fine to coarse sand, little fine to coarse subrounded gravel (SANDY SILT to SILTY SAND).	WC = 20.5% Fines = 55.7% A-4 (0), ML	
	6D	24/13	15.00 - 17.00	3-4-8-11	12	22		38				
								33			WC = 20.5% Fines = 55.7% A-4 (0), ML	
								35				
								39			WC = 20.5% Fines = 55.7% A-4 (0), ML	
								40				
20										Increased drilling resistance. Olive brown, wet, very dense SILTY SAND, little fine to coarse gravel (SANDY SILT to SILTY SAND).	WC = 11.7% Fines = 40.3% A-4 (0), ML/SM	
	7D	24/11	20.00 - 22.00	14-11-20-18	31	56		60				
								92			WC = 11.7% Fines = 40.3% A-4 (0), ML/SM	
								57				
								165			WC = 11.7% Fines = 40.3% A-4 (0), ML/SM	
								58				
25										Grey, wet, very dense, fractured rock with fine to coarse sand (WEATHERED ROCK)	WC = 11.7% Fines = 40.3% A-4 (0), ML/SM	
	8D	14/6	25.00 - 26.17	20-28-30/2"				OPEN				
										Bedrock encountered at 26.4 feet bgs Top of Bedrock Elev. 125.7 ft	WC = 11.7% Fines = 40.3% A-4 (0), ML/SM	
	R-1	60/60	26.40 - 31.40	RQD = 30%				NX		R1 (26.4' - 31.4'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong, slightly weathered to fresh; discontinuities low angle to steep dipping.		
30												

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level reading taken on 7/31/24 at 23:58 was made after the rock coring.

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-105 <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard <b>Operator:</b> Ryan H. <b>Logged By:</b> D. Burgess <b>Date Start/Finish:</b> 7/31/24 (20:07); 8/1/24 (0:30) <b>Boring Location:</b> N: 482984.9, E: 1735593.56	<b>Elevation (ft.):</b> 152.05 <b>Datum:</b> Maine East Zone <b>Rig Type:</b> Diedrich D-50 <b>Drilling Method:</b> SSA, Cased Wash <b>Casing ID/OD:</b>	<b>Auger ID/OD:</b> <b>Sampler:</b> Standard Split Spoon <b>Hammer Wt./Fall:</b> 140lb/30in <b>Core Barrel:</b> NX <b>Water Level*:</b> 17.0' BGS 11:56 7/31/24
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<b>Hammer Efficiency Factor:</b> 1.087	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test		

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows					
30	R-2	57.6/57.6	31.40 - 36.20	RQD = 75%					115.9		very close to close spacing, rough to very rough, tight to open, average 3.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = poor 100% recovery 30% RQD Rock Core Rate (min:sec) 26.4 - 27.4 ft (2:33) 27.4 - 28.4 ft (3:10) 28.4 - 29.4 ft (2:54) 29.4 - 30.4 ft (4:01) 30.4 - 31.4 ft (10:40) R2 (31.4' - 36.2'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, very strong, fresh; discontinuities low angle to steep dipping, very close spacing, smooth to rough, tight, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = fair 100% recovery 75% RQD Rock Core Rate (min:sec) 31.4 - 32.4 ft (2:36) 32.4 - 33.4 (2:53) 33.4 - 34.4 (2:51) 34.4 - 35.4 (2:41) 35.4 - 36.2 (4:20)	
35											Bottom of Exploration at 36.2 feet below ground surface. Boring backfilled with bentonite chips in the rock core socket, drill cuttings and gravel to bottom of pavement and patched with cold patch asphalt.	
40												
45												
50												
55												
60												

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level reading taken on 7/31/24 at 23:58 was made after the rock coring.

<b>Driller:</b> Seaboard	<b>Elevation (ft.):</b> 143.6	<b>Auger ID/OD:</b>
<b>Operator:</b> Ryan H.	<b>Datum:</b> Maine East Zone	<b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> D. Burgess	<b>Rig Type:</b> Diedrich D-50	<b>Hammer Wt./Fall:</b> 140lb/30in
<b>Date Start/Finish:</b> 7/25/24 (20:19); 7/29/24 (1:56)	<b>Drilling Method:</b> SSA, Cased Wash	<b>Core Barrel:</b> NX
<b>Boring Location:</b> N: 482611.2, E: 1735095.82	<b>Casing ID/OD:</b> 4" (ID)	<b>Water Level*:</b> Refer to remarks note 3

**Hammer Efficiency Factor:** 1.087      **Hammer Type:** Automatic     Hydraulic     Rope & Cathead

Definitions:      R = Rock Core Sample       $S_u$  = Peak/Remolded Field Vane Undrained Shear Strength (psf)       $T_v$  = Pocket Torvane Shear Strength (psf)  
 D = Split Spoon Sample      SSA = Solid Stem Auger       $S_{u(lab)}$  = Lab Vane Undrained Shear Strength (psf)      WC = Water Content, percent  
 MD = Unsuccessful Split Spoon Sample Attempt      HSA = Hollow Stem Auger       $q_p$  = Unconfined Compressive Strength (ksf)      LL = Liquid Limit  
 U = Thin Wall Tube Sample      RC = Roller Cone      N-uncorrected = Raw Field SPT N-value      PI = Plasticity Index  
 MU = Unsuccessful Thin Wall Tube Sample Attempt      WOH = Weight of 140lb. Hammer      Hammer Efficiency Factor = Rig Specific Annual Calibration Value      PL = Plasticity Limit  
 V = Field Vane Shear Test, PP = Pocket Penetrometer      WOR/C = Weight of Rods or Casing       $N_{60}$  = SPT N-uncorrected Corrected for Hammer Efficiency      G = Grain Size Analysis  
 MV = Unsuccessful Field Vane Shear Test Attempt      WO1P = Weight of One Person       $N_{60}$  = (Hammer Efficiency Factor/60%)\*N-uncorrected      C = Consolidation Test

Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	$N_{60}$	Casing Blows				
0							SSA	142.8	10" Asphalt Pavement		
	1D	24/13	1.00 - 3.00	14-9-7-5	16	29			Brown, dry, medium dense, fine to coarse SAND, some fine gravel, trace silt (FILL).	0.8	
	2D	24/19	3.00 - 5.00	11-13-18-20	31	56			Olive with brown, moist, hard, SILT, some fine to medium sand, some fine to coarse gravel, non-plastic (FILL)		
5	3D	24/15	5.00 - 7.00	13-16-37-30	53	96			Olive with brown, moist, hard, SILT, some fine to medium sand, some fine to coarse gravel, non-plastic (FILL)		
	4D	24/0	7.00 - 9.00	25-27-22-23	49	89			No recovery.		
10	5D	24/13	10.00 - 12.00	8-9-11-27	20	36	64		Olive with brown, moist, hard, SILT, some fine to medium sand, some fine to coarse gravel, non-plastic (FILL)		
							148				
							133				
							166				
15	6D	24/9	15.00 - 17.00	12-31-20-15	51	92	87		Grey, wet, very dense, fine to coarse SAND, flakey fractured rock fragments (FILL).		
							124		Possible boulder or cobbles 12 to 15" thick.		
							OPEN				
20	7D	24/22	20.00 - 22.00	5-6-3-4	9	16	24	124.6	Olive with grey and orange mottling, wet, very stiff, CLAY, trace sand, medium plasticity (CLAY). Pp = 4.0 to 6.0 ksf.	19.0	
							26			WC = 26% Fines = 98.9% LL = 37 PL = 19 PI = 18 LI = 0.4 A-6 (19), CL	
							22				
							34				
							31				
25	8D	24/24	25.00 - 27.00	4-7-8-9	15	27	42		Olive with grey and orange mottling, wet, very stiff, CLAY, trace sand, medium plasticity (CLAY). Pp = 6.0 to 8.0 ksf.		
							55			WC = 28% Fines = 99.7% LL = 36 PL = 19 PI = 17 LI = 0.5 A-6 (18), CL	
							61				
							54				
30							35				

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level measured during drilling at 20.55' bgs on 7/26/24 at 3:23, 20.55' bgs on 7/28/24 at 20:19. Water level measured at 24.9' bgs on 7/29/24 at 1:08 was made after the rock coring.

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-106					
Driller: Seaboard		Elevation (ft.): 143.6		Auger ID/OD:							
Operator: Ryan H.		Datum: Maine East Zone		Sampler: Standard Split Spoon							
Logged By: D. Burgess		Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in							
Date Start/Finish: 7/25/24 (20:19); 7/29/24 (1:56)		Drilling Method: SSA, Cased Wash		Core Barrel: NX							
Boring Location: N: 482611.2, E: 1735095.82		Casing ID/OD: 4" (ID)		Water Level*: Refer to remarks note 3							
Hammer Efficiency Factor: 1.087		Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>									
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt		R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person		S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected		T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test					
Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows				
30	9D	24/24	30.00 - 32.00	WOH/18"-8			49	112.1		WC = 29% Fines = 98.7% LL = 26 PL = 15 PI = 11 LI = 1.3 A-6 (9), CL	
							42				
							56				
							100				
							57				
35	10D	24/12	35.00 - 37.00	4-2-6-7	8	14	43				
							40				
							42				
							51				
							42				
40	11D	24/10	40.00 - 42.00	5-3-7-7	10	18	59				
							48				
							50				
							52				
							40				
45	12D	24/18	45.00 - 47.00	3-4-4-6	8	14	53				
							49				
							53				
							61				
							43				
50	13D	24/12	50.00 - 52.00	10-8-6-11	14	25	54				
							42				
							96				
							173				
							248				
55	14D	24/15	55.00 - 57.00	14-13-16-19	29	53	61	90.1			
							45				
							62				
							108				
60							112				

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level measured during drilling at 20.55' bgs on 7/26/24 at 3:23, 20.55' bgs on 7/28/24 at 20:19. Water level measured at 24.9' bgs on 7/29/24 at 1:08 was made after the rock coring.



<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-106 <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard <b>Operator:</b> Ryan H. <b>Logged By:</b> D. Burgess <b>Date Start/Finish:</b> 7/25/24 (20:19); 7/29/24 (1:56) <b>Boring Location:</b> N: 482611.2, E: 1735095.82	<b>Elevation (ft.):</b> 143.6 <b>Datum:</b> Maine East Zone <b>Rig Type:</b> Diedrich D-50 <b>Drilling Method:</b> SSA, Cased Wash <b>Casing ID/OD:</b> 4" (ID)	<b>Auger ID/OD:</b> <b>Sampler:</b> Standard Split Spoon <b>Hammer Wt./Fall:</b> 140lb/30in <b>Core Barrel:</b> NX <b>Water Level*:</b> Refer to remarks note 3
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<b>Hammer Efficiency Factor:</b> 1.087	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test		

Depth (ft.)	Sample Information									Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows	Elevation (ft.)				
90											Boring backfilled with bentonite chips in the rock core socket, drill cuttings and gravel to bottom of pavement and patched with cold patch asphalt.	
91												
92												
93												
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120												

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level measured during drilling at 20.55' bgs on 7/26/24 at 3:23, 20.55' bgs on 7/28/24 at 20:19. Water level measured at 24.9' bgs on 7/29/24 at 1:08 was made after the rock coring.

<b>Driller:</b> Seaboard	<b>Elevation (ft.):</b> 143.11	<b>Auger ID/OD:</b>
<b>Operator:</b> Ryan H.	<b>Datum:</b> Maine East Zone	<b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> D. Burgess	<b>Rig Type:</b> Diedrich D-50	<b>Hammer Wt./Fall:</b> 140lb/30in
<b>Date Start/Finish:</b> 7/22/24 (21:09); 7/24/24 (0:25)	<b>Drilling Method:</b> SSA, Drive & Wash	<b>Core Barrel:</b> NX
<b>Boring Location:</b> N: 482578.95, E: 1735092.78	<b>Casing ID/OD:</b> 4" (ID)	<b>Water Level*:</b> Refer to remarks note 3

**Hammer Efficiency Factor:** 1.087      **Hammer Type:** Automatic     Hydraulic     Rope & Cathead

Definitions:      R = Rock Core Sample       $S_u$  = Peak/Remolded Field Vane Undrained Shear Strength (psf)       $T_v$  = Pocket Torvane Shear Strength (psf)  
 D = Split Spoon Sample      SSA = Solid Stem Auger       $S_u(lab)$  = Lab Vane Undrained Shear Strength (psf)      WC = Water Content, percent  
 MD = Unsuccessful Split Spoon Sample Attempt      HSA = Hollow Stem Auger       $q_p$  = Unconfined Compressive Strength (ksf)      LL = Liquid Limit  
 U = Thin Wall Tube Sample      RC = Roller Cone      N-uncorrected = Raw Field SPT N-value      PL = Plastic Limit  
 MU = Unsuccessful Thin Wall Tube Sample Attempt      WOH = Weight of 140lb. Hammer      Hammer Efficiency Factor = Rig Specific Annual Calibration Value      PI = Plasticity Index  
 V = Field Vane Shear Test, PP = Pocket Penetrometer      WOR/C = Weight of Rods or Casing       $N_{60}$  = SPT N-uncorrected Corrected for Hammer Efficiency      G = Grain Size Analysis  
 MV = Unsuccessful Field Vane Shear Test Attempt      WO1P = Weight of One Person       $N_{60}$  = (Hammer Efficiency Factor/60%)\*N-uncorrected      C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	$N_{60}$	Casing Blows					
0	1D	24/14	0.70 - 2.70	8-10-8-6	18	33	SSA	142.6		6" Asphalt Pavement		
										Brown, dry, medium dense, fine to coarse SAND, some fine to coarse gravel, trace silt (FILL).		
	2D	24/16	2.70 - 4.70	6-8-8-17	16	29				Grayish brown, dry, medium dense, SANDY SILT, trace fine gravel, non-plastic (FILL).		
5	3D	24/19	4.70 - 6.70	12-19-18-18	37	67				Grayish brown, dry, hard, SANDY SILT, trace fine gravel, non-plastic (FILL).	Fines = 55.2% A-4 (0), ML	
	4D	24/10	6.70 - 8.70	14-7-18-10	25	45				Grayish brown, dry, hard, SANDY SILT, trace fine gravel, non-plastic (FILL).		
	5D	24/6	8.70 - 10.70	4-3-4-4	7	13				Grayish brown, dry, stiff, SANDY SILT, trace fine gravel, slightly plastic (FILL).		
10	6D	24/9	10.70 - 12.70	6-8-41-50/2"	49	89	23			Olive brown, wet, hard, SILT, some fine to coarse sand, trace fine gravel, slightly plastic, fractured rock fragments (FILL). Pp = 7.0 ksf	WC = 14.7% Fines = 62.3% A-4 (0), ML	
							64					
							77					
							94					
							77					
15	7D	24/5	15.00 - 17.00	12-19-20-8	39	71	59			Olive brown, wet, very dense, fine to coarse SAND, fractured scaly rock fragments (FILL).		
							135					
							180					
							91					
							86					
20	8D	24/14	20.00 - 22.00	17-4-7-6	11	20	65	122.6		Grey with orange, mottled, wet, very stiff, CLAY, trace sand, medium plasticity (CLAY). Pp = 6.0 ksf	WC = 24% Fines = 98.3% LL = 33 PL = 17 PI = 16 LI = -0.4 A-6 (15), CL	
							53					
							65					
							82					
							87					
25	9D	24/24	25.00 - 27.00	4-3-6-6	9	16	65		Grey to brown, mottled, wet, very stiff, CLAY, trace sand (CLAY) Pp = 4.5 to 5.0 ksf	Fines = 99.3% A-6 (37), CL		
							93					
							88					
							97					
30							79					

**Remarks:**

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- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level measured during drilling at 6.45' bgs on 7/23/24 at 3:28, 18.7' bgs on 7/24/24 at 3:22, 19.3' bgs on 7/24/24 at 20:09. Water level measured at 23.9' bgs on 7/24/24 at 23:51 was made after the rock coring.

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-107									
Driller: Seaboard		Elevation (ft.): 143.11		Auger ID/OD:		WIN: 027176.00									
Operator: Ryan H.		Datum: Maine East Zone		Sampler: Standard Split Spoon											
Logged By: D. Burgess		Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in											
Date Start/Finish: 7/22/24 (21:09); 7/24/24 (0:25)		Drilling Method: SSA, Drive & Wash		Core Barrel: NX											
Boring Location: N: 482578.95, E: 1735092.78		Casing ID/OD: 4"(ID)		Water Level*: Refer to remarks note 3											
Hammer Efficiency Factor: 1.087				Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>											
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt				R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person				S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected				T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test			
Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.				
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows								
30	10D	24/17	30.00 - 32.00	3-3-3-3	6	11	70	108.1		Greyish brown, moist, medium stiff, CLAY, trace sand, medium plasticity, interbedded silt seams (CLAY). Pp < 2.0 ksf  FV-1: 442psf / 118psf (55mmx110mm Vane) FV-2: 813psf / 415psf (55mmx110mm Vane)	WC = 28% Fines = 99.1% LL = 28 PL = 16 PI = 12 LI = 1 A-6 (11), CL				
							63								
							56								
							390								
							63								
35	11D	24/0	35.00 - 37.00	12-11-15-10	26	47	104	108.1		No recovery - washed water had fine to coarse gravel and clay fragments.					
							96								
							87								
							78								
							63								
40	12D	24/6	40.00 - 42.00	5-7-12-12	19	34	73		Brownish grey, wet, dense, SILTY SAND, little coarse gravel, slightly plastic (SILTY SAND)	WC = 10% Fines = 42.1% LL = 17 PL = 13 PI = 4 LI = -0.8 A-4 (0), SC/ SM					
							76								
							103								
							111								
							81								
45	13D	24/4	45.00 - 47.00	9-9-6-9	15	27	105		Brownish grey, wet, medium dense, SILTY SAND, little coarse gravel, slightly plastic (SILTY SAND).						
							103								
							111								
							118								
							90								
50	14D	24/8	50.00 - 52.00	6-8-15-8	23	42	81		Greyish brown, wet, dense, CLAYEY SAND, some gravel, low plasticity (CLAYEY SAND).	WC = 10% Fines = 39.6% LL = 20 PL = 12 PI = 8 LI = -0.3 A-4 (0), SC					
							89								
							105								
							113								
							89								
55	15D	24/14	55.00 - 57.00	26-41-51-50/4"	92	167	60	89.6	Olive with brown mottled, wet, very dense, SILTY SAND, little gravel, non-plastic (GLACIAL TILL).	WC = 10.6% Fines = 38.3% A-4 (0), SM					
							198								
							171								
							212								
60							196								
<b>Remarks:</b> 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA000074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023. 2. As-drilled boring locations and ground surface elevations were provided by HNTB. 3. Water level measured during drilling at 6.45' bgs on 7/23/24 at 3:28, 18.7' bgs on 7/24/24 at 3:22, 19.3' bgs on 7/24/24 at 20:09. Water level measured at 23.9' bgs on 7/24/24 at 23:51 was made after the rock coring.															
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 2 of 4					
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-BSA-107					

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-107					
Driller: Seaboard				Elevation (ft.): 143.11		Auger ID/OD:					
Operator: Ryan H.				Datum: Maine East Zone		Sampler: Standard Split Spoon					
Logged By: D. Burgess				Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in					
Date Start/Finish: 7/22/24 (21:09); 7/24/24 (0:25)				Drilling Method: SSA, Drive & Wash		Core Barrel: NX					
Boring Location: N: 482578.95, E: 1735092.78				Casing ID/OD: 4"(ID)		Water Level*: Refer to remarks note 3					
Hammer Efficiency Factor: 1.087				Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>							
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt				R = Rock Core Sample SSA = Solid Stern Auger HSA = Hollow Stern Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person		S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u</sub> (lab) = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected					
Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows				
60	16D	8/8	60.00 - 60.67	53-50/2"	R		OPEN			Olive with brown mottled, wet, very dense, SILT, some fine round to subround gravel, trace fine to medium sand, weathered coarse gravel (GLACIAL TILL).	
	R-1	45.6/7.2	63.40 - 67.20	RQD = 0%			R	79.7		Bedrock encountered at 63.4 feet bgs Top of Bedrock Elev. 80.1 ft R1 (63.4' - 67.2'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], strong, highly weathered with clay and sand infilling from 64.2 ft to 67.2; discontinuities low angle to steep dipping, close spacing, rough to very rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 16% recovery 0% RQD Rock Core Rate (min:sec) 63.4 - 64.2 ft (1:09) 64.2 - 65.0 ft (1:29) 65.0 - 65.3 ft (0:41) 65.3 - 66.3 ft (1:51) 66.3 - 67.2 ft (1:13)	
65							NX				
	R-2	12/2.04	67.20 - 68.20	RQD = 0%							
	R-3	48/45.6	68.20 - 72.20	RQD = 35%							
70											
	R-4	60/60	72.20 - 77.20	RQD = 39%							
75											
								65.9			
80											
85											
90											
<b>Remarks:</b> 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023. 2. As-drilled boring locations and ground surface elevations were provided by HNTB. 3. Water level measured during drilling at 6.45'bgs on 7/23/24 at 3:28, 18.7'bgs on 7/24/24 at 3:22, 19.3'bgs on 7/24/24 at 20:09. Water level measured at 23.9'bgs on 7/24/24 at 23:51 was made after the rock coring.											
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 3 of 4	
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-BSA-107	

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-107 <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard <b>Operator:</b> Ryan H. <b>Logged By:</b> D. Burgess <b>Date Start/Finish:</b> 7/22/24 (21:09); 7/24/24 (0:25) <b>Boring Location:</b> N: 482578.95, E: 1735092.78	<b>Elevation (ft.):</b> 143.11 <b>Datum:</b> Maine East Zone <b>Rig Type:</b> Diedrich D-50 <b>Drilling Method:</b> SSA, Drive & Wash <b>Casing ID/OD:</b> 4"(ID)	<b>Auger ID/OD:</b> <b>Sampler:</b> Standard Split Spoon <b>Hammer Wt./Fall:</b> 140lb/30in <b>Core Barrel:</b> NX <b>Water Level*:</b> Refer to remarks note 3
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<b>Hammer Efficiency Factor:</b> 1.087	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
T <sub>v</sub> = Pocket Torvane Shear Strength (psf) W <sub>c</sub> = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test		

Depth (ft.)	Sample Information										Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows	Elevation (ft.)					
90											steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = poor 100% recovery 39% RQD Rock Core Rate (min:sec) 72.2 - 73.2 ft (2:07) 73.2 - 74.2 ft (1:35) 74.2 - 75.2 ft (1:53) 75.2 - 76.2 ft (1:32) 76.2 - 77.2 ft (1:30)		
91													
92													
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**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level measured during drilling at 6.45' bgs on 7/23/24 at 3:28, 18.7' bgs on 7/24/24 at 3:22, 19.3' bgs on 7/24/24 at 20:09. Water level measured at 23.9' bgs on 7/24/24 at 23:51 was made after the rock coring.

<b>Driller:</b> Seaboard	<b>Elevation (ft.):</b> 129.45	<b>Auger ID/OD:</b>
<b>Operator:</b> Kevin Hanscom	<b>Datum:</b> Maine East Zone	<b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> Lina-Maria Pua	<b>Rig Type:</b> Diedrich D-50	<b>Hammer Wt./Fall:</b> 140 lbs/30 in
<b>Date Start/Finish:</b> 05/07/24 (21:55); 05/07/24 (23:30)	<b>Drilling Method:</b> SSA, Cased Wash	<b>Core Barrel:</b> NX
<b>Boring Location:</b> N: 482749.52, E: 1735322.13	<b>Casing ID/OD:</b> 3 in/3.25 in	<b>Water Level*:</b> 4.8 ft on 05/07/24 at 22:20

**Hammer Efficiency Factor:** 1.066      **Hammer Type:** Automatic  Hydraulic  Rope & Cathead

Definitions: R = Rock Core Sample      S<sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf)      T<sub>v</sub> = Pocket Torvane Shear Strength (psf)  
 D = Split Spoon Sample      SSA = Solid Stem Auger      S<sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf)      WC = Water Content, percent  
 MD = Unsuccessful Split Spoon Sample Attempt      HSA = Hollow Stem Auger      q<sub>p</sub> = Unconfined Compressive Strength (ksf)      LL = Liquid Limit  
 U = Thin Wall Tube Sample      RC = Roller Cone      N-uncorrected = Raw Field SPT N-value      PL = Plastic Limit  
 MU = Unsuccessful Thin Wall Tube Sample Attempt      WOH = Weight of 140lb. Hammer      Hammer Efficiency Factor = Rig Specific Annual Calibration Value      PI = Plasticity Index  
 V = Field Vane Shear Test, PP = Pocket Penetrometer      WOR/C = Weight of Rods or Casing      N<sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency      G = Grain Size Analysis  
 MV = Unsuccessful Field Vane Shear Test Attempt      WO1P = Weight of One Person      N<sub>60</sub> = (Hammer Efficiency Factor/60%)\*N-uncorrected      C = Consolidation Test

Sample Information										Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows	Elevation (ft.)	Graphic Log				
0							SSA	128.9		7.5" Asphalt Pavement			
	1D	24/16	1.00 - 3.00	22-18-16-20	34	60				Brown to yellow, dry, very dense, fine to coarse SAND, some silt, little fine gravel (FILL).	0.6	MC = 8.0% Fines = 28.5% A-2-4 (0), SM	
	2D	24/9	3.00 - 5.00	15-14-24-16	38	68		126.3		2DA To 2 in: Brown to yellow, dry, very dense, fine to coarse SAND, some silt, little fine gravel (FILL).	3.2		
5	3D	24/12	5.00 - 7.00	12-12-12-50/2"	24	43				2DB Bottom 7 in: Grey, dry, very dense, GRAVEL, some sand, little silt (GRAVEL)			
	R1	60/59	6.70 - 11.70	RQD = 59%			NX	122.8		Brown, wet, dense, GRAVEL, some sand, little silt (GRAVEL). Grey angular GRAVEL with some sand and little silt in the tip of the split spoon.	6.7		
										Bedrock encountered at 6.7 feet bgs Top of Bedrock at Elev. 122.8 ft			
10										R1 (6.7'-11.1'): Grey, very fine to fine grained, METAWACKE [metasandstone] with frequent calcite veins, very to extremely strong, thinly laminated, slightly weathered; discontinuities moderate to steep dipping, close to moderately close spacing, rough to polished, open. average 2.6 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].			
	R2	12/11	11.70 - 12.70	RQD = 40%						Rock Mass Quality = fair 98% Recovery Rock Core Rate (min:sec) 6.7-7.7 ft (2:33) 7.7-8.7 ft (2:46) 8.7-9.7 ft (3:19) 9.7-10.7 ft (2:51) 10.7-11.7 ft (3:17)			
	R3	24/21	12.70 - 14.70	RQD = 19%						R2 (11.1'-12.7'): Grey, very fine to fine grained, METAWACKE [metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open. average 1.0 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].			
15										Rock Mass Quality = poor 92% Recovery Rock Core Rate (min:sec) 11.7-12.7 ft (3:07)			
	R4	24/23	14.70 - 16.70	RQD = 37%						R3 (12.7'-14.7'): Grey, very fine to fine grained, METAWACKE [metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open. average 2.5 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].			
										Rock Mass Quality = very poor 88% Recovery Rock Core Rate (min:sec) 12.7-13.7 ft (2:04) 13.7-14.7 ft (3:25)			
20										R4 (14.7'-16.7'): Grey, very fine to fine grained, METAWACKE			
25													
30													

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by MaineDOT.
- Water level reading taken on 5/7/24 at 22:20 was made before the start of rock coring with bottom of casing at 6.7 ft bgs.

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-108  <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard	<b>Elevation (ft.):</b> 129.45	<b>Auger ID/OD:</b>
<b>Operator:</b> Kevin Hanscom	<b>Datum:</b> Maine East Zone	<b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> Lina-Maria Pua	<b>Rig Type:</b> Diedrich D-50	<b>Hammer Wt./Fall:</b> 140 lbs/30 in
<b>Date Start/Finish:</b> 05/07/24 (21:55); 05/07/24 (23:30)	<b>Drilling Method:</b> SSA, Cased Wash	<b>Core Barrel:</b> NX
<b>Boring Location:</b> N: 482749.52, E: 1735322.13	<b>Casing ID/OD:</b> 3 in/3.25 in	<b>Water Level*:</b> 4.8 ft on 05/07/24 at 22:20

<b>Hammer Efficiency Factor:</b> 1.066	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person
	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
	T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test

Depth (ft.)	Sample Information									Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows	Elevation (ft.)				
30											[metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open, average 2.0 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = poor 96% Recovery Rock Core Rate (min:sec) 14.7-15.7 ft (2:30) 15.7-16.7 ft (2:48)	
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33												
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**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by MaineDOT.
- Water level reading taken on 5/7/24 at 22:20 was made before the start of rock coring with bottom of casing at 6.7 ft bgs.

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-109  <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard	<b>Elevation (ft.):</b> 126.99	<b>Auger ID/OD:</b> 4.0 in/4.5 in
<b>Operator:</b> Kevin Hanscom	<b>Datum:</b> Maine East Zone	<b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> Lina-Maria Pua	<b>Rig Type:</b> Diedrich D-50	<b>Hammer Wt./Fall:</b> 140 lbs/30 in
<b>Date Start/Finish:</b> 05/07/24 (1:20); 05/07/24 (2:30)	<b>Drilling Method:</b> Hollow Stem Augers	<b>Core Barrel:</b> NX
<b>Boring Location:</b> N: 482636.37, E: 1735255.48	<b>Casing ID/OD:</b>	<b>Water Level*:</b> Not Measured

<b>Hammer Efficiency Factor:</b> 1.066	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
<small>Definitions:          D = Split Spoon Sample          MD = Unsuccessful Split Spoon Sample Attempt          U = Thin Wall Tube Sample          MU = Unsuccessful Thin Wall Tube Sample Attempt          V = Field Vane Shear Test, PP = Pocket Penetrometer          MV = Unsuccessful Field Vane Shear Test Attempt       </small>	<small>R = Rock Core Sample          SSA = Solid Stem Auger          HSA = Hollow Stem Auger          RC = Roller Cone          WOH = Weight of 140lb. Hammer          WOR/C = Weight of Rods or Casing          WO1P = Weight of One Person       </small>	<small>S<sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf)          S<sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf)          q<sub>p</sub> = Unconfined Compressive Strength (ksf)          N-uncorrected = Raw Field SPT N-value          Hammer Efficiency Factor = Rig Specific Annual Calibration Value          N<sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency          N<sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected       </small>
		<small>T<sub>v</sub> = Pocket Torvane Shear Strength (psf)          WC = Water Content, percent          LL = Liquid Limit          PL = Plasticity Limit          PI = Plasticity Index          G = Grain Size Analysis          C = Consolidation Test       </small>

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows					
0								SSA	126.3	Asphalt Pavement		
	1D	24/12	1.00 - 3.00	19-16-17-18	33	59				Brown to yellow, dry, very dense, fine to coarse SAND, some gravel, little silt (FILL).		
	2D	24/15.5	3.00 - 5.00	27-22-63-54	85	151				Brown to yellow, dry to moist, very dense, SANDY GRAVEL, little silt (FILL).	MC = 5.7% Fines = 15.9% A-1-b (0), GM	
5	3D	24/13.5	5.00 - 7.00	19-23-16-17	39	69				Brown to yellow, wet, very dense, fine to coarse SAND, some gravel, some silt, poorly-graded (FILL).		
	4D	24/23	7.00 - 9.00	41-41-67-103	108	192				4DA Top 19 in: Brown, wet to moist, very dense, fine to coarse SAND, some gravel, little silt (FILL).	MC = 11.7% Fines = 20.3% A-1-b (0), SM	
	5D	12/10	9.00 - 10.00	28-63	R				118.3	4DB Bottom 4 in: Brown, moist, hard, SILT, some fine sand, little gravel (SANDY SILT).		
10	6D	1/1	10.00 - 10.08	50/1"	R				117.0 116.9	Brown, moist, SILT, some fine sand, little gravel (SANDY SILT). Grey, very dense, PROBABLE BEDROCK FRAGMENTS, some silt. (WEATHERED BEDROCK).		
										<b>Bottom of Exploration at 10.1 feet below ground surface.</b> Boring backfilled with drill cuttings to bottom of pavement and patched with cold patch.		
15												
20												
25												
30												

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by MaineDOT.

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-109A  <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard	<b>Elevation (ft.):</b> 127.03	<b>Auger ID/OD:</b> 4 in/4.5in
<b>Operator:</b> Kevin Hanscom	<b>Datum:</b> Maine East Zone	<b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> Lina-Maria Pua	<b>Rig Type:</b> Diedrich D-50	<b>Hammer Wt./Fall:</b> 140 lbs/30 in
<b>Date Start/Finish:</b> 05/07/24 (20:18); 05/07/24 (21:44)	<b>Drilling Method:</b> SSA, Cased Wash	<b>Core Barrel:</b> NX
<b>Boring Location:</b> N: 482637.93, E: 1735257.73	<b>Casing ID/OD:</b> 4.0 in/4.25 in	<b>Water Level*:</b> 2.8 ft on 05/07/24 at 21:35

<b>Hammer Efficiency Factor:</b> 1.066	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test		

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows					
0												
5	R-1	57.6/52	4.00 - 8.80	RQD = 33%								
10	R-2	66/61.5	8.80 - 14.30	RQD = 49%								
15												
20												
25												
30												

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by MaineDOT.
- Water level reading taken on 5/7/24 at 21:35 was made after rock coring was completed with bottom of casing at 3.5 ft bgs.

<b>Driller:</b> Seaboard	<b>Elevation (ft.):</b> 127.53	<b>Auger ID/OD:</b>
<b>Operator:</b> Kevin Hanscom	<b>Datum:</b> Maine East Zone	<b>Sampler:</b> Standard Split Spoon
<b>Logged By:</b> Lina-Maria Pua	<b>Rig Type:</b> Diedrich D-50	<b>Hammer Wt./Fall:</b> 140 lbs/30 in
<b>Date Start/Finish:</b> 05/08/24 (20:09); 05/08/24 (21:22)	<b>Drilling Method:</b> SSA, Cased Wash	<b>Core Barrel:</b> NX
<b>Boring Location:</b> N: 482660.73, E: 1735292.34	<b>Casing ID/OD:</b> 3.0 in/3.25 in	<b>Water Level*:</b> 3.1 ft on 05/08/24 at 20:34

**Hammer Efficiency Factor:** 1.066      **Hammer Type:** Automatic  Hydraulic  Rope & Cathead

Definitions:      R = Rock Core Sample      S<sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf)      T<sub>v</sub> = Pocket Torvane Shear Strength (psf)  
 D = Split Spoon Sample      SSA = Solid Stem Auger      S<sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf)      WC = Water Content, percent  
 MD = Unsuccessful Split Spoon Sample Attempt      HSA = Hollow Stem Auger      q<sub>p</sub> = Unconfined Compressive Strength (ksf)      LL = Liquid Limit  
 U = Thin Wall Tube Sample      RC = Roller Cone      N-uncorrected = Raw Field SPT N-value      PL = Plasticity Limit  
 MU = Unsuccessful Thin Wall Tube Sample Attempt      WOH = Weight of 140lb. Hammer      Hammer Efficiency Factor = Rig Specific Annual Calibration Value      PI = Plasticity Index  
 V = Field Vane Shear Test, PP = Pocket Penetrometer      WOR/C = Weight of Rods or Casing      N<sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency      G = Grain Size Analysis  
 MV = Unsuccessful Field Vane Shear Test Attempt      WO1P = Weight of One Person      N<sub>60</sub> = (Hammer Efficiency Factor/60)\*N-uncorrected      C = Consolidation Test

Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows				
0								126.9	Asphalt Pavement	0.6	
	1D	24/11	1.00 - 3.00	16-21-16-20	37	66			Brown, dry, dense, Silty GRAVEL, little sand (FILL).		
	2D	24/6	3.00 - 5.00	10-8-9-21	17	30			Grey, wet, medium dense, Silty angular GRAVEL, trace sand (FILL).		
5	3D R1	3/3 60/57	5.00 - 5.25 5.30 - 10.30	50/3" RQD = 52%	R			122.2	Grey, wet, very dense, angular GRAVEL, some silt, trace sand, poorly-graded (FILL).	5.3	
									Bedrock encountered at 5.3 feet bgs Top of Bedrock at Elev. 122.2 ft R1 (5.3'-10.3'): Grey, very fine grained, METAWACKE [metasandstone] with frequent thick and thin calcite veins, medium strong, thinly laminated, fresh; discontinuities horizontal to steep dipping, close to moderately close spacing, stepped, smooth to polished, open. average 1.0 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = fair 95% Recovery Rock Core Rate (min:sec) 5.3-6.3 ft (2:20) 6.3-7.3 ft (2:31) 7.3-8.3 ft (2:21) 8.3-9.3 ft (2:54) 9.3-10.3 ft (3:10)		
10	R2	60/60	10.30 - 15.30	RQD = 72%					R2 (10.3'-15.3'): Grey, very fine grained, METAWACKE [metasandstone] with frequent thick and thin calcite veins, very to extremely strong, thinly laminated, fresh; discontinuities steep dipping, close to wide spacing, stepped, smooth, open. average 0.8 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = fair 100% Recovery Rock Core Rate (min:sec) 10.3-11.3 ft (3:15) 11.3-12.3 ft (2:42) 12.3-13.3 ft (3:30) 13.3-14.3 ft (2:58) 14.3-15.3 ft (3:40)		
15								112.2			
20											
25											
30											

**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by MaineDOT.
- Water level reading taken on 5/8/24 at 20:34 was made before the start of rock coring with bottom of casing at 5.3 ft bgs.

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-111					
Driller: Seaboard		Elevation (ft.): 148.27		Auger ID/OD:		WIN: 027176.00					
Operator: Ryan H.		Datum: Maine East Zone		Sampler: Standard Split Spoon							
Logged By: D. Burgess		Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in							
Date Start/Finish: 7/25/24 (0:44); 7/25/24 (4:25)		Drilling Method: SSA, Cased Wash		Core Barrel: NX							
Boring Location: N: 482728.68, E: 1735418.07		Casing ID/OD: 4" (ID)		Water Level*: 14.75' 4:07 7/25/24							
Hammer Efficiency Factor: 1.087		Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>									
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt		R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person		S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u</sub> (lab) = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected		T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test					
Sample Information											
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows	Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
0	1D	24/9	0.60 - 2.60	9-11-9-11	20	36	SSA	147.7		7" Asphalt pavement	Fines = 13.5% A-1-a (0), GM-SM
5	2D	24/19	3.00 - 5.00	11-20-22-16	42	76				Olive with brown, moist, hard, SILT, some round to subround gravel, little fine to medium sand, weathered coarse gravel, non-plastic (FILL). Light olive brown, moist, hard, SANDY SILT, trace gravel, non-plastic (FILL).	Fines = 61.6% A-4 (0), ML
	3D	13.5/12	5.00 - 6.13	13-21-50/1.5"	R					Fractured rock fragments, trace organics (roots) (FILL).	
	4D	24/12	7.00 - 9.00	12-26-20-13	46	83	47			Olive with dark grey, moist, hard, SANDY SILT, trace gravel, non-plastic (FILL).	
10	5D	24/22	10.00 - 12.00	7-9-11-15	20	36	59	138.8		Olive with orange mottled, moist, hard, CLAY, trace sand, medium plasticity (CLAY). Pp 3.0 to 3.5 tsf	WC = 21% Fines = 99.4% LL = 32 PL = 17 PI = 15 LI = 0.3 A-6 (15), CL
15	6D	24/13	15.00 - 17.00	19-24-16-45	40	72	71	134.8		Grayish brown, wet, very dense, SAND and GRAVEL, little silt, and fractured rock fragments (GLACIAL TILL).	WC = 13.4% Fines = 20.0% A-1-b (0), SM/GM
20	R-1	60/40.8	19.00 - 24.00	RQD = 15%				130.5		Bedrock encountered at 17.8 feet bgs Top of Bedrock at Elev. 130.5 ft R1 (19.0' - 24.0'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, slightly weathered with signs of chemical weathering; discontinuities low angle to steep dipping, close to very close spacing, rough to very rough, open to tight, highly fractured average from 19 ft to 21.3 ft [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 68% recovery 15% RQD Rock Core Rate (min:sec) 19.0 - 20.0 ft (2:11) 20.0 - 21.0 ft (1:11) 21.0 - 22.0 ft (1:55) 22.0 - 23.0 ft (1:49) 23.0 - 24.0 ft (1:56) R2 (24.0' - 29.0'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, very strong to strong, fresh; discontinuities low angle dipping, very	
25	R-2	60/60	24.00 - 29.00	RQD = 60%							
30								119.3			
Remarks:											
1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.											
2. As-drilled boring locations and ground surface elevations were provided by HNTB.											
3. Water level reading taken on 7/25/24 at 4:07 am was made after the rock coring.											
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.											
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.											
								Page 1 of 2			
								Boring No.: BB-BSA-111			

<b>Maine Department of Transportation</b> Soil/Rock Exploration Log US CUSTOMARY UNITS	<b>Project:</b> MaineDOT I-95 Bridges Over Stillwater Avenue <b>Location:</b> Bangor, Maine	<b>Boring No.:</b> BB-BSA-111 <b>WIN:</b> 027176.00
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<b>Driller:</b> Seaboard <b>Operator:</b> Ryan H. <b>Logged By:</b> D. Burgess <b>Date Start/Finish:</b> 7/25/24 (0:44); 7/25/24 (4:25) <b>Boring Location:</b> N: 482728.68, E: 1735418.07	<b>Elevation (ft.):</b> 148.27 <b>Datum:</b> Maine East Zone <b>Rig Type:</b> Diedrich D-50 <b>Drilling Method:</b> SSA, Cased Wash <b>Casing ID/OD:</b> 4" (ID)	<b>Auger ID/OD:</b> <b>Sampler:</b> Standard Split Spoon <b>Hammer Wt./Fall:</b> 140lb/30in <b>Core Barrel:</b> NX <b>Water Level*:</b> 14.75' 4:07 7/25/24
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<b>Hammer Efficiency Factor:</b> 1.087	<b>Hammer Type:</b> Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>	
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person	S <sub>u</sub> = Peak/Remolded Field Vane Undrained Shear Strength (psf) S <sub>u(lab)</sub> = Lab Vane Undrained Shear Strength (psf) q <sub>p</sub> = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N <sub>60</sub> = SPT N-uncorrected Corrected for Hammer Efficiency N <sub>60</sub> = (Hammer Efficiency Factor/60%)*N-uncorrected
T <sub>v</sub> = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test		

Depth (ft.)	Sample Information									Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N <sub>60</sub>	Casing Blows	Elevation (ft.)				
30										close spacing, rough, tight, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = fair 100% recovery 60% RQD Rock Core Rate (min:sec) 24.0 - 25.0 ft (3:39) 25.0 - 26.0 ft (5:35) 26.0 - 27.0 ft (5:39) 27.0 - 28.0 ft (5:10) 28.0 - 29.0 ft (3:51)		
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**Remarks:**

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level reading taken on 7/25/24 at 4:07 am was made after the rock coring.

**APPENDIX B**

**Rock Core Photographs**

**APPENDIX B  
ROCK CORE PHOTOGRAPHS  
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE  
BANGOR, MAINE  
MAINEDOT WIN #027176.00**

Boring	Run	Depth Below Surface		Recovery		RQD		Rock Type	Box Row	Date Cored	
		Feet	Feet	Feet	%	Feet	%				
BB-BSA-101	R1	31.5	- 32.4	0.8	/ 0.9	89	0.0 / 0.9	0	Metawacke	3	7/29/2024
	R2	32.4	- 32.9	0.5	/ 0.5	100	0.0 / 0.5	0	Metawacke	3	7/29/2024
	R3	32.9	- 36.5	3.6	/ 3.6	100	0.5 / 3.6	14	Metawacke	3	7/29/2024
	R4	36.5	- 41.5	5.0	/ 5.0	100	3.0 / 5.0	60	Metawacke	4	7/29/2024
BB-BSA-106	R1	63.8	- 64.8	0.3	/ 1.0	30	0 / 0.3	0	Metawacke	1	7/28/2024
	R2	64.8	- 69.1	4.3	/ 4.3	100	2 / 4.3	47	Metawacke	1	7/28/2024
	R3	69.1	- 74.1	5.0	/ 5.0	100	3.6 / 5.0	62	Metawacke	2	7/28/2024



- Notes:
1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
  2. Top of each core run is on the left and increases with depth to the right.

Prepared By: RJN  
Checked By: LMP  
Reviewed By: JDL

**APPENDIX B  
ROCK CORE PHOTOGRAPHS  
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE  
BANGOR, MAINE  
MAINEDOT WIN #027176.00**

Boring	Run	Depth Below Surface		Recovery		RQD		Rock Type	Box Row	Date Cored	
		Feet	Feet	Feet	%	Feet	%				
BB-BSA-102	R1	12.2	- 17.2	4.50	/ 5.0	90	3.7 / 5.0	73	Metawacke	3	5/8/2024
	R2	17.2	- 22.2	4.9	/ 5.0	98	4.9 / 5.0	98	Metawacke	4	5/8/2024
BB-BSA-108	R1	6.7	- 11.7	4.9	/ 5.0	98	3.0 / 5.0	59	Metawacke	1	5/7/2024
	R2	11.7	- 12.7	0.9	/ 1.0	92	0.4 / 1.0	40	Metawacke	2	5/7/2024
	R3	12.7	- 14.7	1.76	/ 2.0	88	0.38 / 2.0	19	Metawacke	2	5/7/2024
	R4	14.7	- 16.7	1.92	/ 2.0	96	0.74 / 2.0	37	Metawacke	2	5/7/2024



- Notes:
1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
  2. Top of each core run is on the left and increases with depth to the right.

Prepared By: RJN  
Checked By: LMP  
Reviewed By: JDL

**APPENDIX B  
ROCK CORE PHOTOGRAPHS  
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE  
BANGOR, MAINE  
MAINEDOT WIN #027176.00**

Boring	Run	Depth Below Surface		Recovery		RQD		Rock Type	Box Row	Date Cored	
		Feet	Feet	Feet	%	Feet	%				
BB-BSA-103	R1	7.2	- 12.2	5.0	/ 5.0	100	1.6 / 5.0	31	Metawacke	3	5/8/2024
	R2	12.2	- 17.2	5.0	/ 5.0	100	3.6 / 5.0	71	Metawacke	4	5/8/2024
BB-BSA-110	R1	5.3	- 10.3	4.8	/ 5.0	95	2.6 / 5.0	52	Metawacke	1	5/8/2024
	R2	10.3	- 15.3	5.0	/ 5.0	100	3.6 / 5.0	72	Metawacke	2	5/8/2024

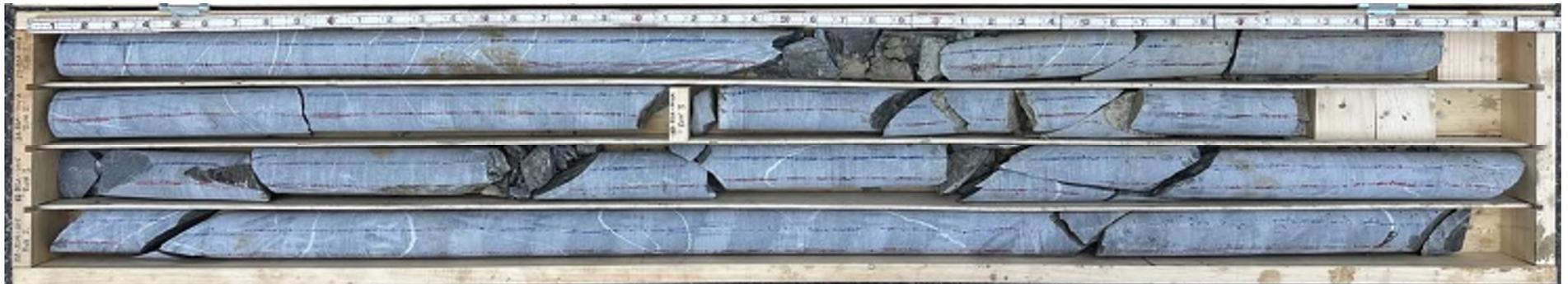


- Notes:
1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
  2. Top of each core run is on the left and increases with depth to the right.

Prepared By: RJN  
Checked By: LMP  
Reviewed By: JDL

**APPENDIX B  
ROCK CORE PHOTOGRAPHS  
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE  
BANGOR, MAINE  
MAINEDOT WIN #027176.00**

Boring	Run	Depth Below Surface		Recovery			RQD		Rock Type	Box Row	Date Cored	
		Feet	Feet	Feet	%	Feet	%					
BB-BSA-104A	R1	21.0	- 26.0	4.8	/ 5.0	95	2.8	/ 5.0	56	Metawacke	1	7/30/2024
	R2	26.0	- 28.8	2.1	/ 2.8	75	1.7	/ 2.8	61	Metawacke	2	7/30/2024
	R3	28.8	- 31.0	2.0	/ 2.2	91	0.5	/ 2.2	23	Metawacke	2	7/30/2024
BB-BSA-105	R1	26.4	- 31.4	5.0	/ 5.0	100	1.5	/ 5.0	30	Metawacke	3	7/31/2024
	R2	31.4	- 36.2	4.8	/ 4.8	100	3.6	/ 4.8	75	Metawacke	4	7/31/2024



- Notes:
1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
  2. Top of each core run is on the left and increases with depth to the right.

Prepared By: RJN  
Checked By: LMP  
Reviewed By: JDL

**APPENDIX B  
ROCK CORE PHOTOGRAPHS  
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE  
BANGOR, MAINE  
MAINEDOT WIN #027176.00**

Boring	Run	Depth Below Surface		Recovery			RQD			Rock Type	Box Row	Date Cored
		Feet	Feet	Feet	%	Feet	%					
BB-BSA-107	R1	63.4	- 67.2	0.6	/ 3.8	23	0.0	/ 3.8	0	Metawacke	1	7/23/2024
	R2	67.2	- 68.2	0.2	/ 1.0	17	0.0	/ 1.0	0	Metawacke	1	7/24/2024
	R3	68.2	- 72.2	3.8	/ 4.0	95	1.4	/ 4.0	35	Metawacke	1	7/24/2024
	R4	72.2	- 77.2	5.0	/ 5.0	100	2.0	/ 5.0	39	Metawacke	2	7/24/2024
BB-BSA-111	R1	19.0	- 24.0	3.4	/ 5.0	68	0.8	/ 5.0	15	Metawacke	3	7/24/2024
	R2	24.0	- 29.0	5.0	/ 5.0	100	3.0	/ 5.0	60	Metawacke	4	7/24/2024



Notes: 1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.  
2. Top of each core run is on the left and increases with depth to the right.

Prepared By: RJN  
Checked By: LMP  
Reviewed By: JDL

**APPENDIX B  
ROCK CORE PHOTOGRAPHS  
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE  
BANGOR, MAINE  
MAINEDOT WIN #027176.00**

Boring	Run	Depth Below Surface		Recovery		RQD		Rock Type	Box Row	Date Cored	
		Feet	Feet	Feet	%	Feet	%				
BB-BSA109A	R1	4.0	- 8.8	4.3	/ 4.8	90	1.6 / 4.8	33	Metawacke	2	5/7/2024
	R2	8.8	- 13.9	4.8	/ 5.1	93	2.5 / 5.1	49	Metawacke	2,3	5/7/2024



- Notes:
1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
  2. Top of each core run is on the left and increases with depth to the right.

Prepared By: RJN  
Checked By: LMP  
Reviewed By: JDL

**APPENDIX C**

**Laboratory Test Results**



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	---	Sample Type:	---
Sample ID:	---	Test Date:	08/12/24
Depth :	---	Test Id:	780399
		Tested By:	ajl
		Checked By:	ank

## Moisture Content of Soil and Rock - ASTM D2216

Boring ID	Sample ID	Depth	Description	Moisture Content, %
BB-BSA-101	4D	7-9 ft	Moist, olive brown sandy silt with gravel	11.1
BB-BSA-101	6D	15-17 ft	Moist, olive brown silty sand with gravel	10.7
BB-BSA-101	8D	25-27 ft	Moist, dark grayish brown silty gravel with sand	9.6
BB-BSA-104	4D	7-9 ft	Moist, dark grayish brown silty sand with gravel	6.5
BB-BSA-104	5D	10-12 ft	Moist, grayish brown sandy silt	11.1
BB-BSA-104	7D	20-22 ft	Moist, greenish gray silt with sand	16.4
BB-BSA-105	6D	15-17 ft	Moist, grayish brown sandy silt	20.5
BB-BSA-105	7D	20-22ft	Moist, olive brown silty sand with gravel	11.7
BB-BSA-106	14D	55-57 ft	Moist, gray silty sand	46.5
BB-BSA-107	6D	10.7-12.7 ft	Moist, olive brown silt with sand	14.7

Notes: Temperature of Drying : 110° Celsius



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	---	Sample Type:	---
Sample ID:	---	Test Date:	08/14/24
Depth :	---	Test Id:	780423
		Tested By:	ajl
		Checked By:	ank

## Moisture Content of Soil and Rock - ASTM D2216

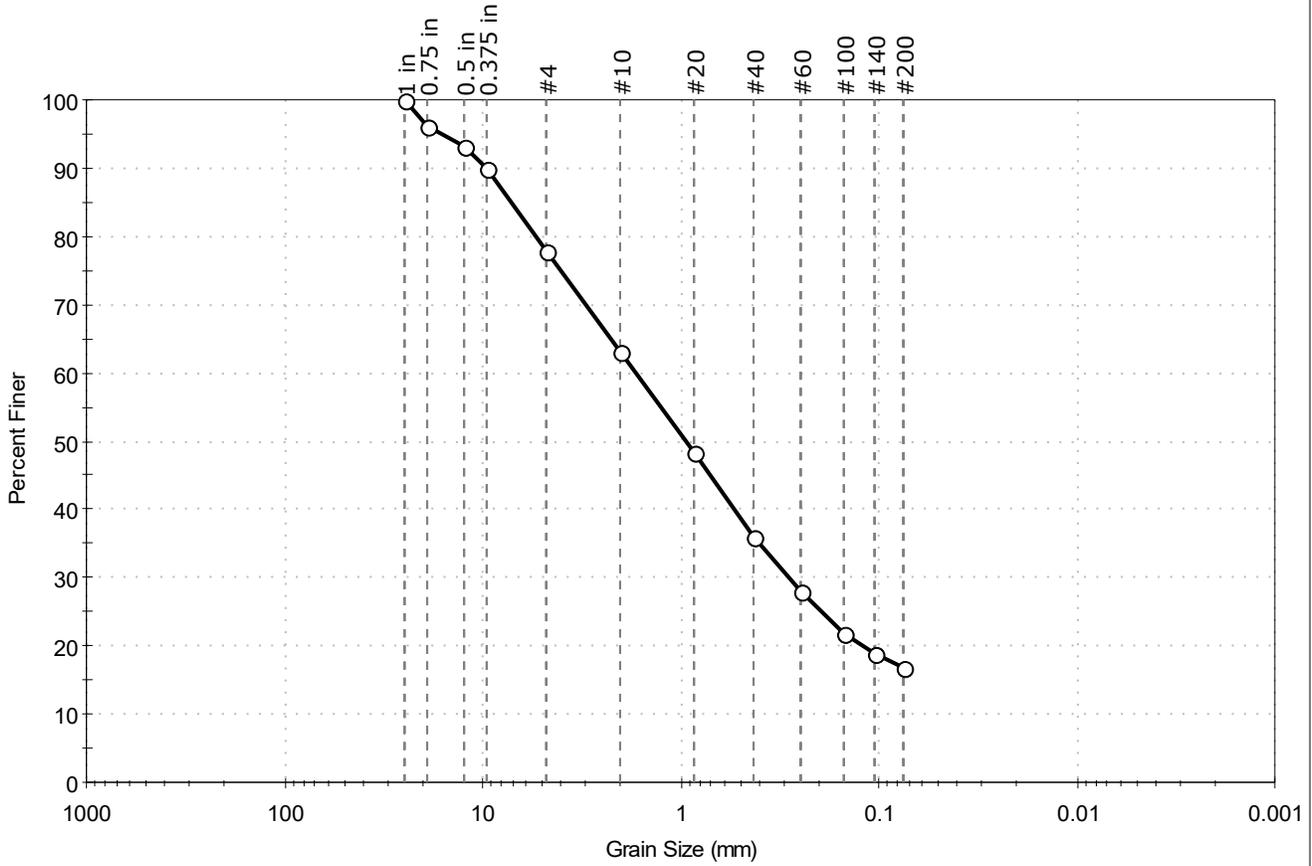
Boring ID	Sample ID	Depth	Description	Moisture Content, %
BB-BSA-107	15D	55-57 ft	Moist, grayish brown silty sand with gravel	10.6
BB-BSA-111	6D	15-17 ft	Moist, grayish brown silty sand with gravel	13.4

Notes: Temperature of Drying : 110° Celsius



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-101	Sample Type:	Jar
Sample ID:	1D	Test Date:	08/19/24
Depth :	0.7-2.7 ft	Checked By:	ank
Test Comment:	---		
Visual Description:	Moist, light olive brown silty sand with gravel		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	22.0	61.2	16.8

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	96		
0.5 in	12.50	93		
0.375 in	9.50	90		
#4	4.75	78		
#10	2.00	63		
#20	0.85	48		
#40	0.42	36		
#60	0.25	28		
#100	0.15	22		
#140	0.11	19		
#200	0.075	17		

<u>Coefficients</u>	
D <sub>85</sub> = 7.1397 mm	D <sub>30</sub> = 0.2832 mm
D <sub>60</sub> = 1.6778 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.9366 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

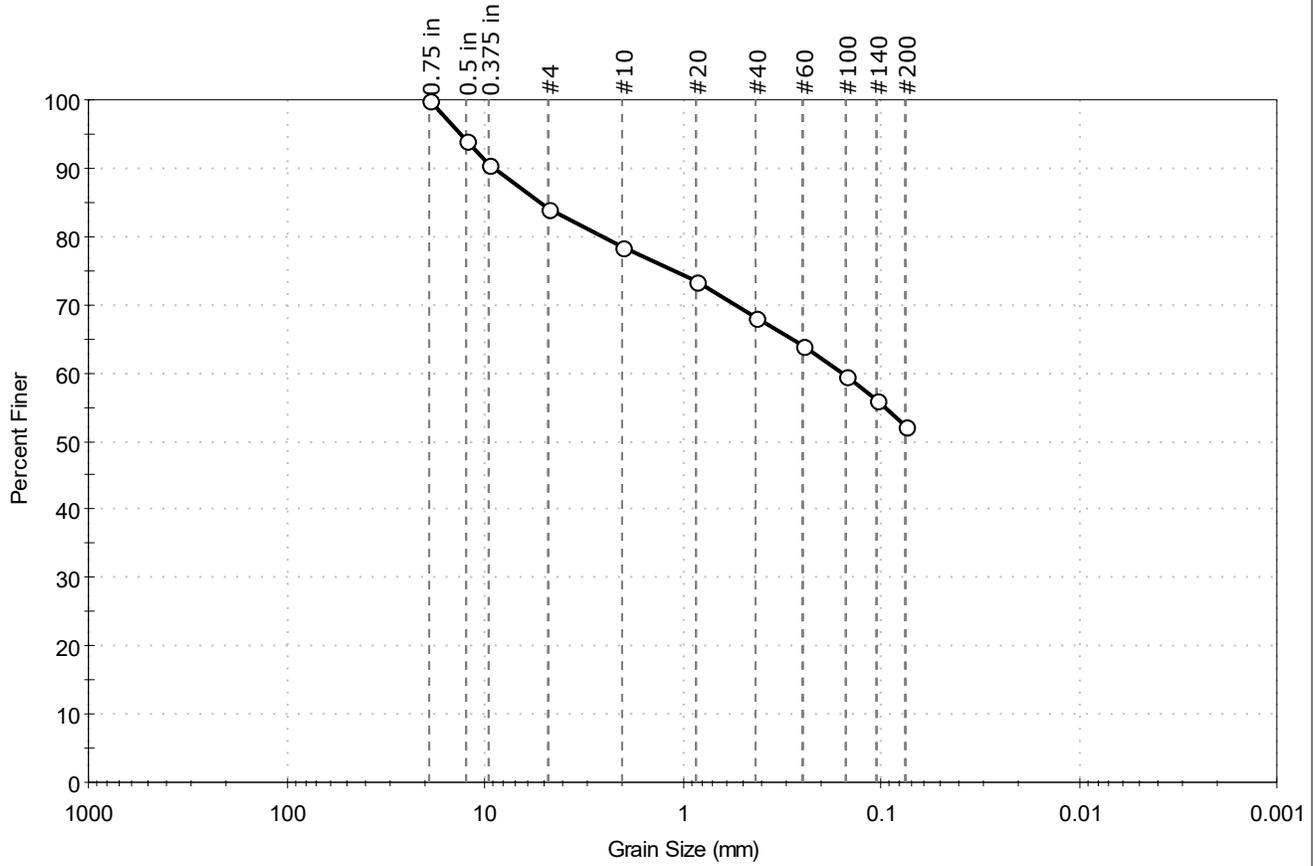
<u>Classification</u>	
ASTM	N/A
AASHTO	Stone Fragments, Gravel and Sand (A-1-b (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-101	Sample Type:	Jar
Sample ID:	4D	Test Date:	08/19/24
Depth:	7-9 ft	Test Id:	780402
Test Comment:	---		
Visual Description:	Moist, olive brown sandy silt with gravel		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	15.8	32.0	52.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	94		
0.375 in	9.50	91		
#4	4.75	84		
#10	2.00	79		
#20	0.85	73		
#40	0.42	68		
#60	0.25	64		
#100	0.15	59		
#140	0.11	56		
#200	0.075	52		

<u>Coefficients</u>	
D <sub>85</sub> = 5.2031 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.1591 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = N/A	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

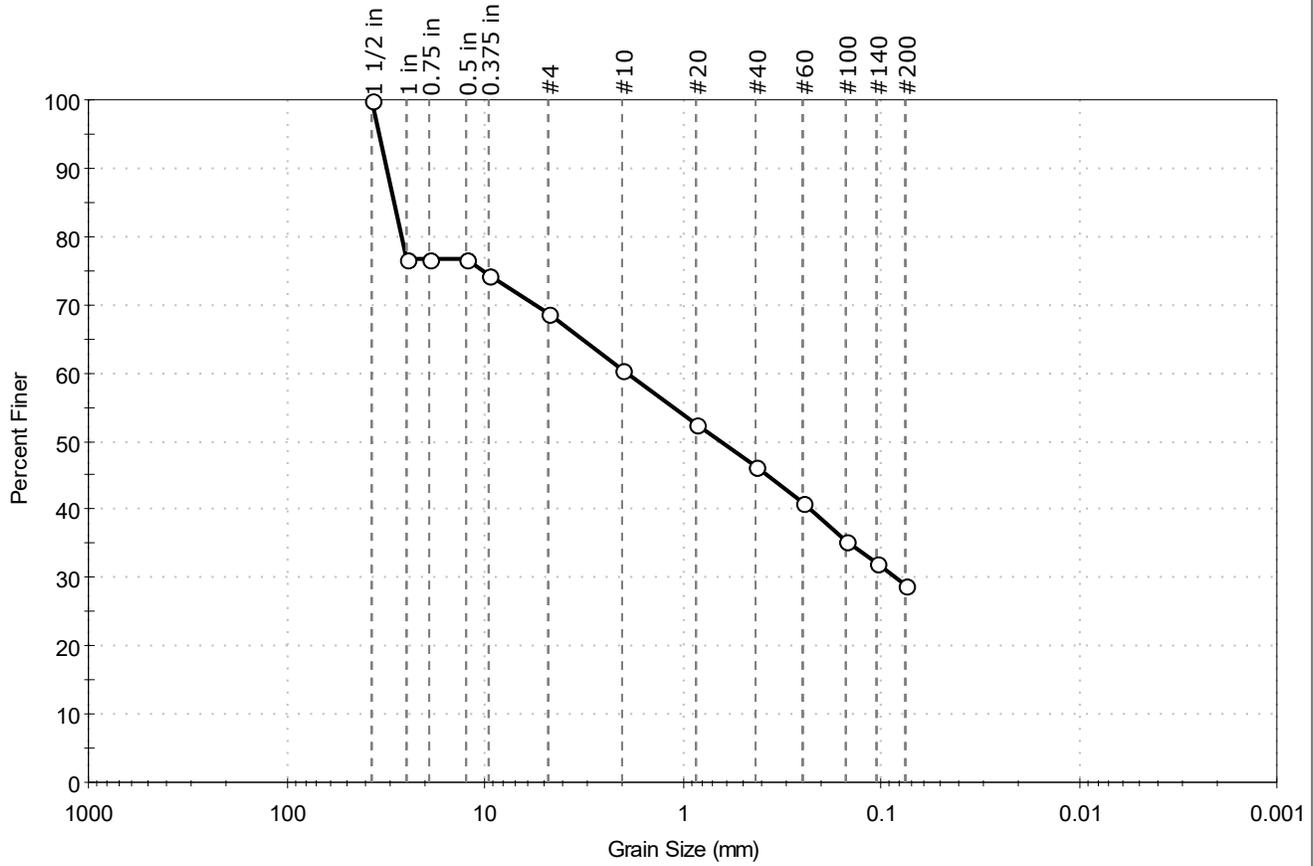
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-101	Sample Type:	Jar
Sample ID:	6D	Test Date:	08/16/24
Depth:	15-17 ft	Test Id:	780403
Test Comment:	---		
Visual Description:	Moist, olive brown silty sand with gravel		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	31.2	40.0	28.8

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 1/2 in	37.50	100		
1 in	25.00	77		
0.75 in	19.00	77		
0.5 in	12.50	77		
0.375 in	9.50	74		
#4	4.75	69		
#10	2.00	61		
#20	0.85	53		
#40	0.42	46		
#60	0.25	41		
#100	0.15	35		
#140	0.11	32		
#200	0.075	29		

Coefficients	
D <sub>85</sub> = 28.9113 mm	D <sub>30</sub> = 0.0851 mm
D <sub>60</sub> = 1.8753 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.6407 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

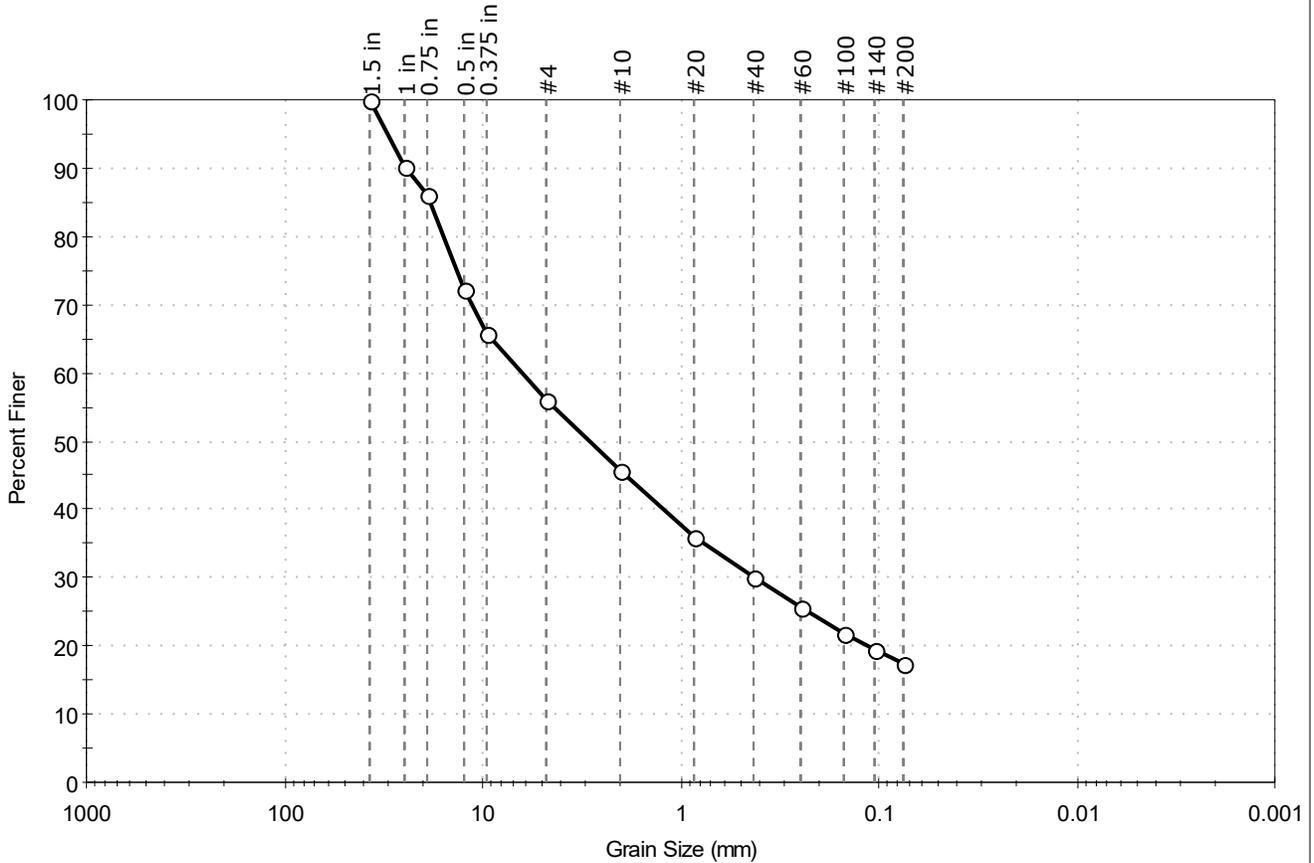
Classification	
ASTM	N/A
AASHTO	Silty Gravel and Sand (A-2-4 (0))

Sample/Test Description
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-101	Sample Type:	Jar
Sample ID:	8D	Test Date:	08/19/24
Depth:	25-27 ft	Test Id:	780404
Test Comment:	---		
Visual Description:	Moist, dark grayish brown silty gravel with sand		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	43.8	38.7	17.5

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1.5 in	37.50	100		
1 in	25.00	90		
0.75 in	19.00	86		
0.5 in	12.50	72		
0.375 in	9.50	66		
#4	4.75	56		
#10	2.00	46		
#20	0.85	36		
#40	0.42	30		
#60	0.25	26		
#100	0.15	22		
#140	0.11	19		
#200	0.075	18		

<u>Coefficients</u>	
D <sub>85</sub> = 18.3264 mm	D <sub>30</sub> = 0.4200 mm
D <sub>60</sub> = 6.2648 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 2.8644 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

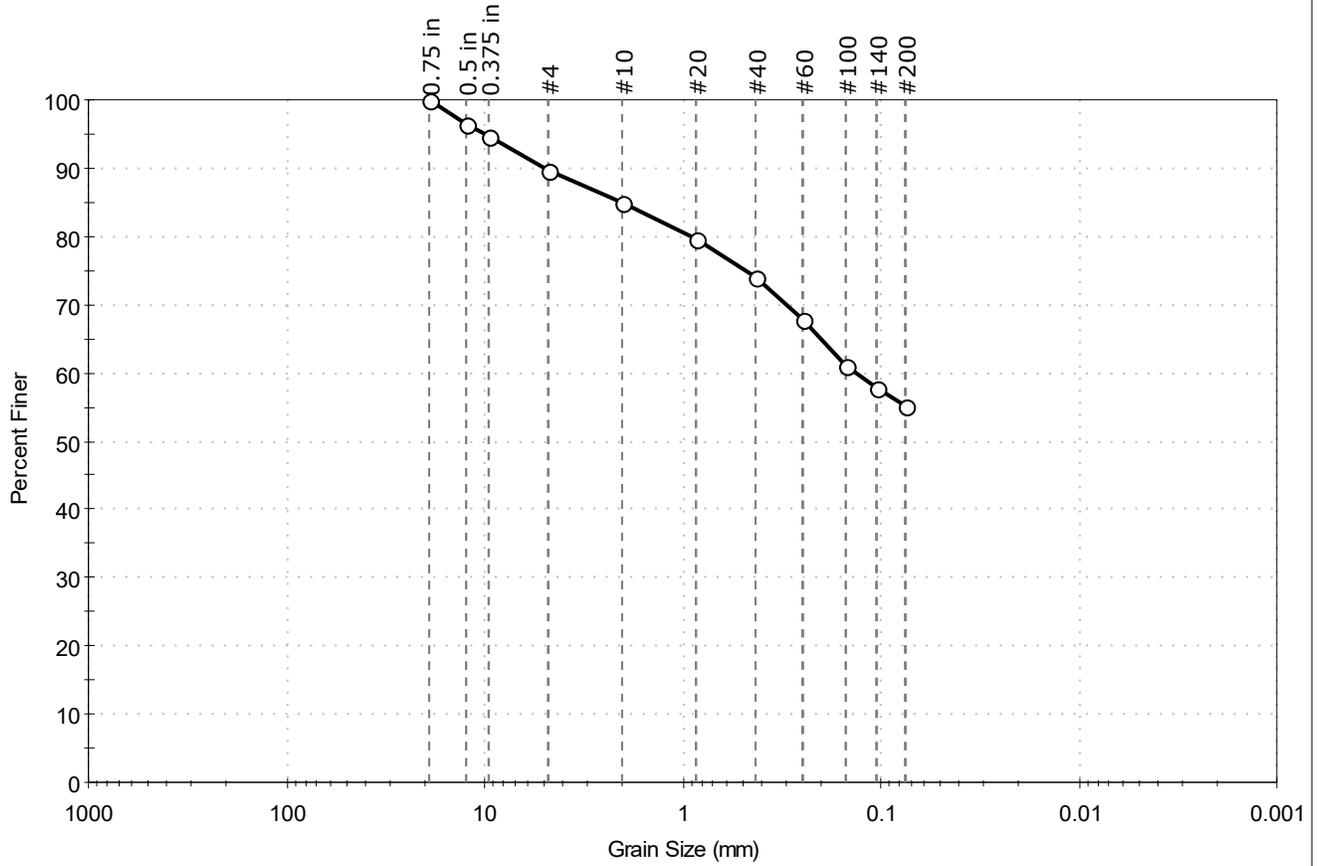
<u>Classification</u>	
ASTM	N/A
AASHTO	Stone Fragments, Gravel and Sand (A-1-b (0))

<u>Sample/Test Description</u>	
Sand/Gravel Particle Shape : ANGULAR	
Sand/Gravel Hardness : HARD	



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-104	Sample Type:	Jar
Sample ID:	2D	Test Date:	08/19/24
Depth :	2.8-4.8 ft	Test Id:	780405
Test Comment:	---		
Visual Description:	Moist, dark grayish brown sandy silt		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	10.4	34.3	55.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	96		
0.375 in	9.50	95		
#4	4.75	90		
#10	2.00	85		
#20	0.85	80		
#40	0.42	74		
#60	0.25	68		
#100	0.15	61		
#140	0.11	58		
#200	0.075	55		

<u>Coefficients</u>	
D <sub>85</sub> = 1.9913 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.1326 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = N/A	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

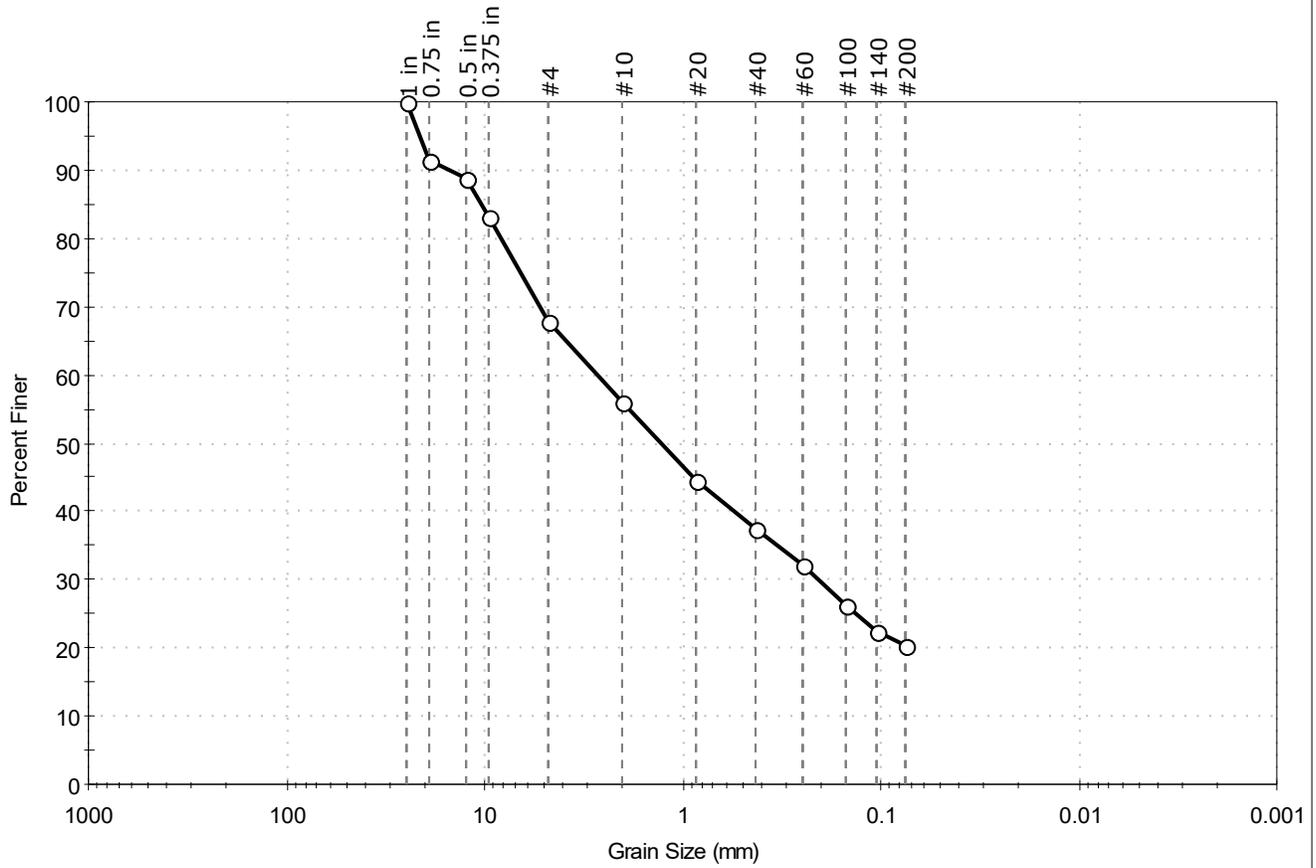
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-104	Sample Type:	Jar
Sample ID:	4D	Test Date:	08/19/24
Depth :	7-9 ft	Test Id:	780406
Test Comment:	---		
Visual Description:	Moist, dark grayish brown silty sand with gravel		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	32.0	47.6	20.4

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	92		
0.5 in	12.50	89		
0.375 in	9.50	83		
#4	4.75	68		
#10	2.00	56		
#20	0.85	45		
#40	0.42	37		
#60	0.25	32		
#100	0.15	26		
#140	0.11	23		
#200	0.075	20		

<u>Coefficients</u>	
D <sub>85</sub> = 10.3977 mm	D <sub>30</sub> = 0.2076 mm
D <sub>60</sub> = 2.6769 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 1.2727 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

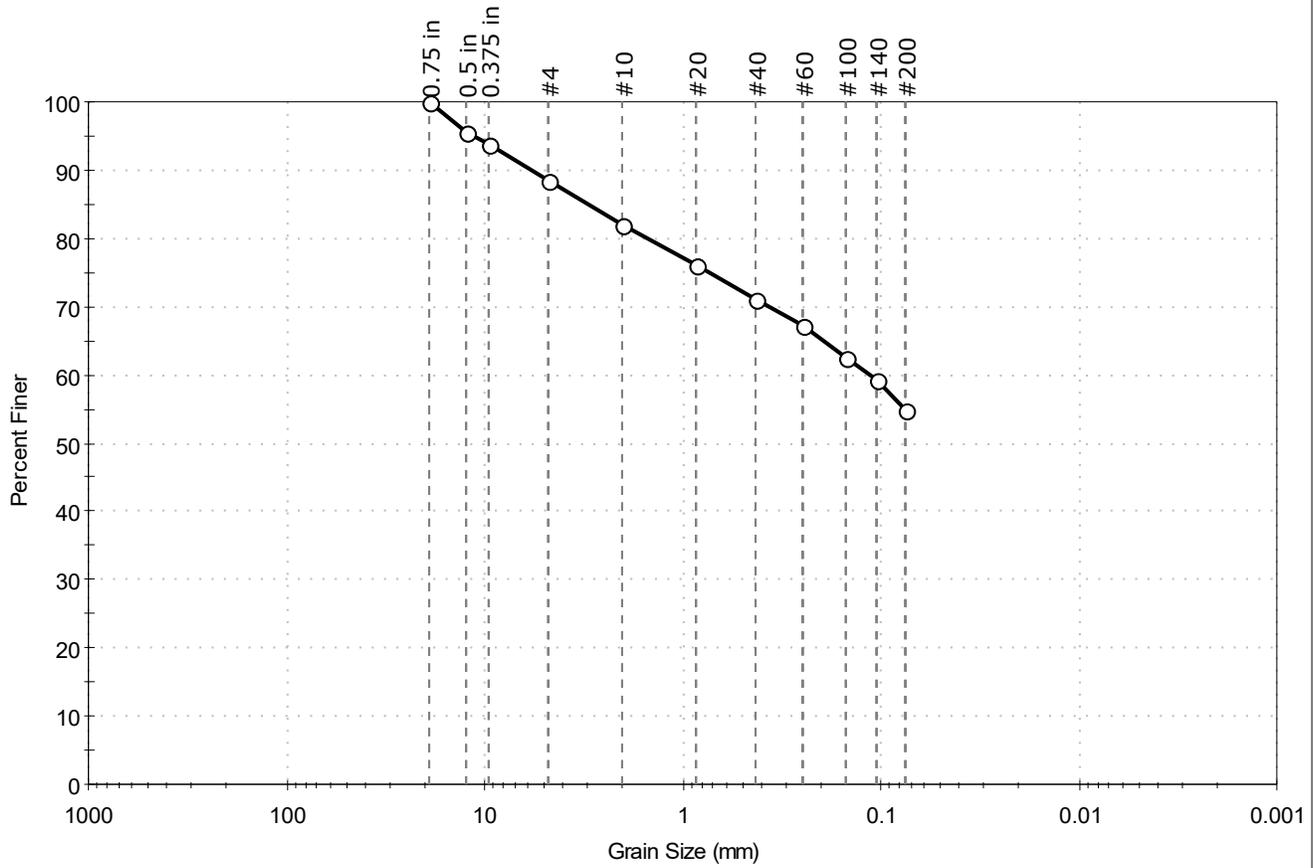
<u>Classification</u>	
ASTM	N/A
AASHTO	Stone Fragments, Gravel and Sand (A-1-b (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-104	Sample Type: Jar
Sample ID: 5D	Test Date: 08/19/24
Depth: 10-12 ft	Test Id: 780407
Test Comment: ---	Tested By: ajl
Visual Description: Moist, grayish brown sandy silt	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	11.6	33.5	54.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	96		
0.375 in	9.50	94		
#4	4.75	88		
#10	2.00	82		
#20	0.85	76		
#40	0.42	71		
#60	0.25	67		
#100	0.15	63		
#140	0.11	59		
#200	0.075	55		

<u>Coefficients</u>	
D <sub>85</sub> = 3.0173 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.1137 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = N/A	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

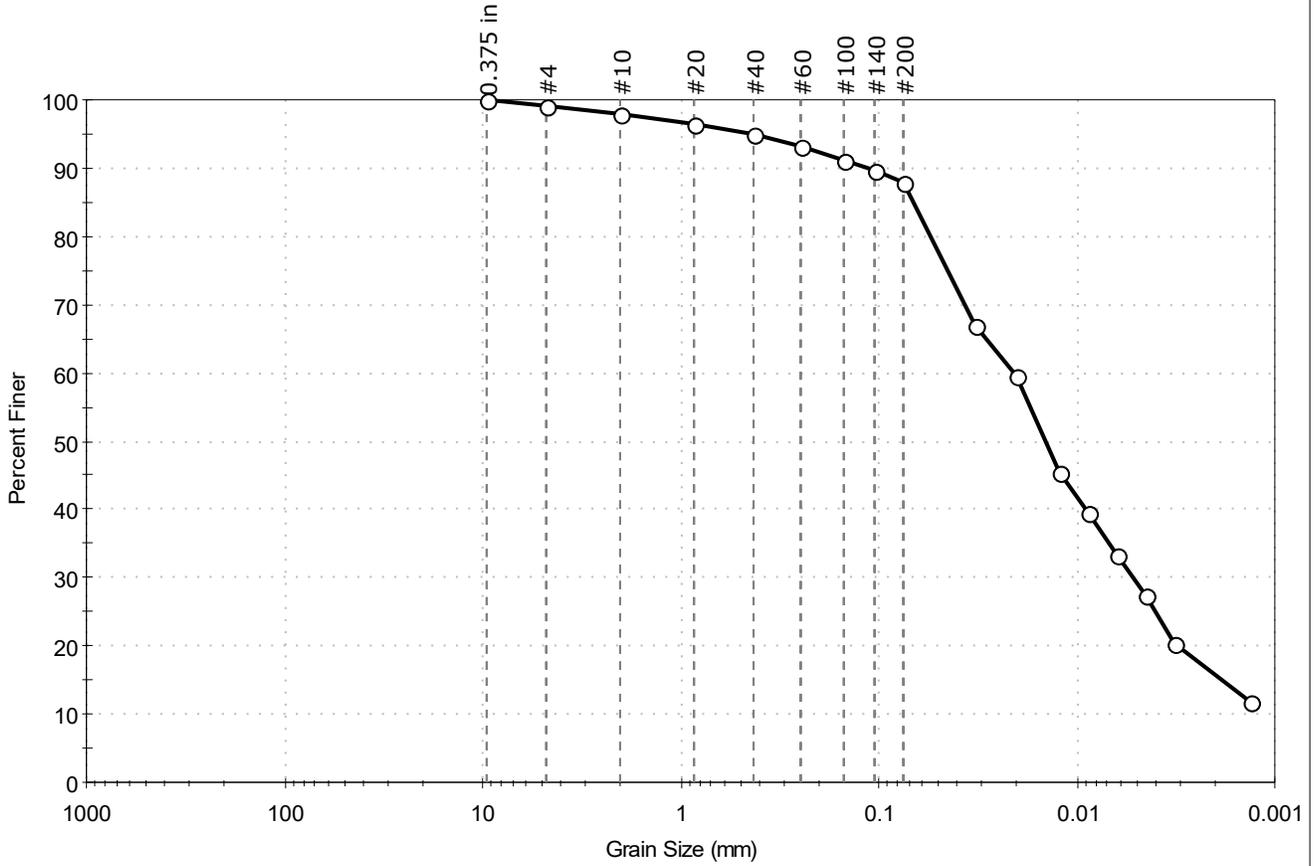
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-104	Sample Type: Jar
Sample ID: 6D	Test Date: 08/15/24
Depth: 15-17 ft	Test Id: 780410
Test Comment: ---	Tested By: ajl
Visual Description: Moist, grayish brown clay	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	1.0	11.2	87.8

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.375 in	9.50	100		
#4	4.75	99		
#10	2.00	98		
#20	0.85	96		
#40	0.42	95		
#60	0.25	93		
#100	0.15	91		
#140	0.11	90		
#200	0.075	88		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0324	67		
---	0.0201	60		
---	0.0122	45		
---	0.0088	39		
---	0.0063	33		
---	0.0045	27		
---	0.0032	20		
---	0.0013	12		

<b>Coefficients</b>	
D <sub>85</sub> = 0.0670 mm	D <sub>30</sub> = 0.0052 mm
D <sub>60</sub> = 0.0205 mm	D <sub>15</sub> = 0.0019 mm
D <sub>50</sub> = 0.0143 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

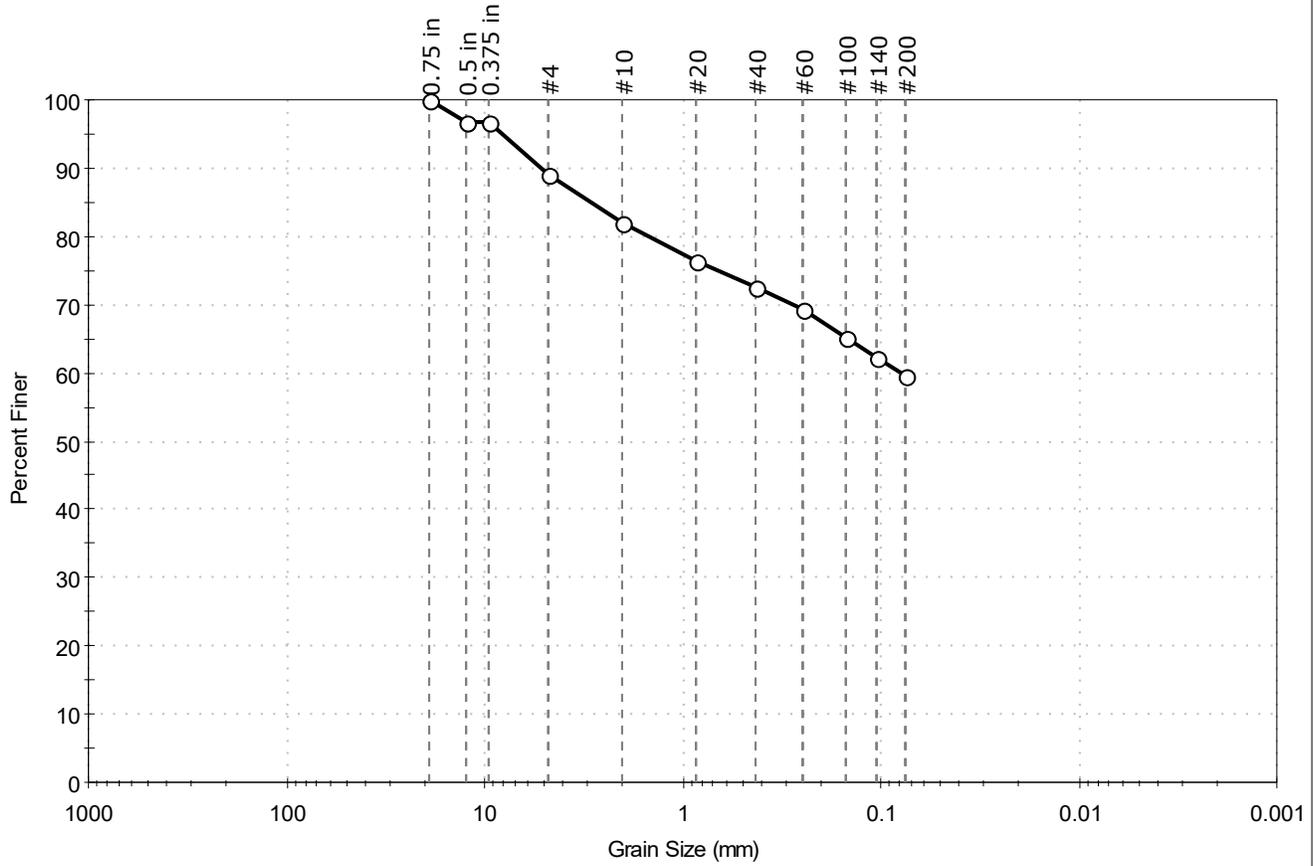
<b>Classification</b>	
<b>ASTM</b>	Lean CLAY (CL)
<b>AASHTO</b>	Clayey Soils (A-6 (10))

<b>Sample/Test Description</b>
Sand/Gravel Particle Shape : ---
Sand/Gravel Hardness : ---
Dispersion Device : Apparatus A - Mech Mixer
Dispersion Period : 1 minute
Est. Specific Gravity : 2.65
Separation of Sample: #200 Sieve



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-104	Sample Type: Jar
Sample ID: 7D	Test Date: 08/19/24
Depth: 20-22 ft	Test Id: 780408
Test Comment: ---	Tested By: ajl
Visual Description: Moist, greenish gray silt with sand	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	10.8	29.7	59.5

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	97		
0.375 in	9.50	97		
#4	4.75	89		
#10	2.00	82		
#20	0.85	76		
#40	0.42	72		
#60	0.25	69		
#100	0.15	65		
#140	0.11	62		
#200	0.075	59		

<u>Coefficients</u>	
D <sub>85</sub> = 2.8830 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.0799 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = N/A	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

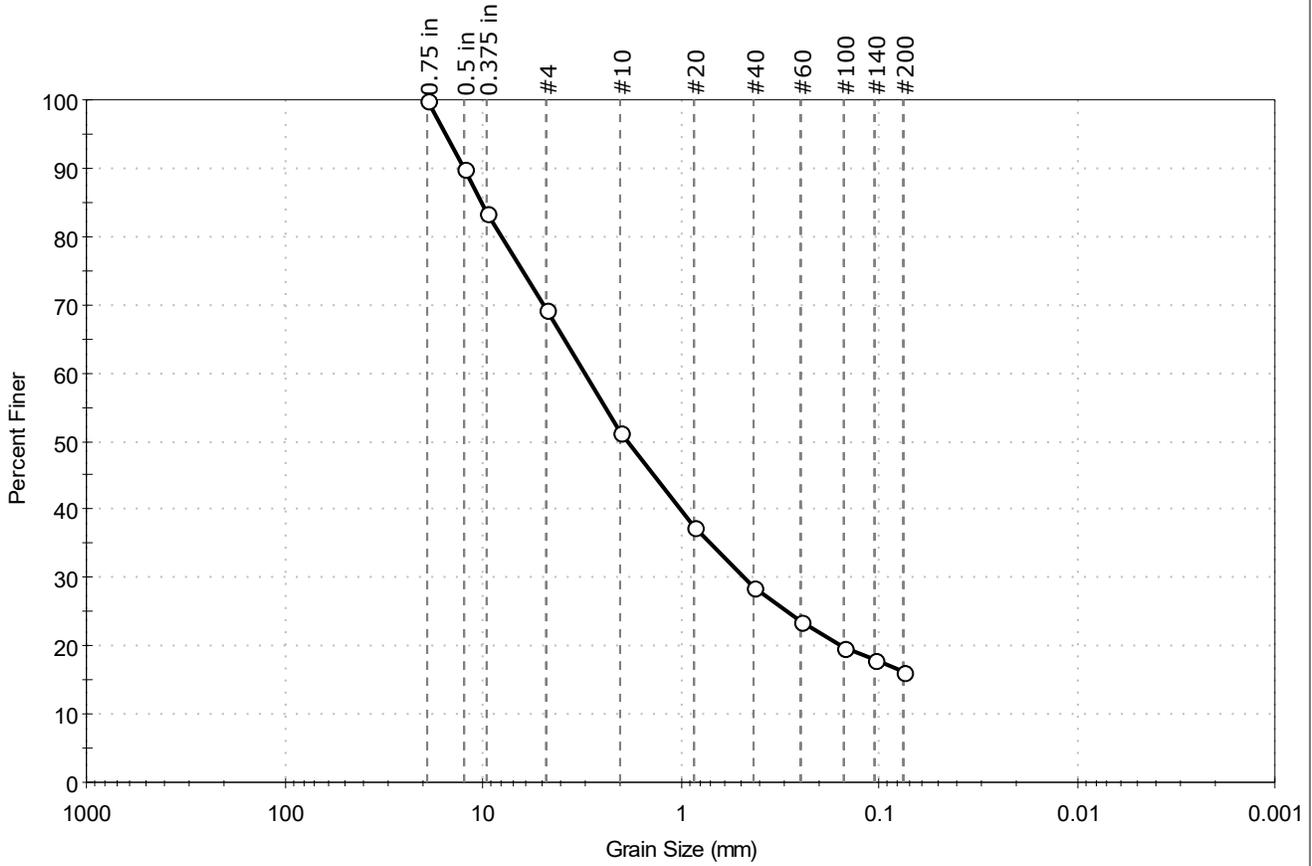
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-105	Sample Type:	Jar
Sample ID:	1D	Test Date:	08/19/24
Depth :	0.9-2.9 ft	Test Id:	780366
Test Comment:	---		
Visual Description:	Moist, olive brown silty sand with gravel		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	30.7	53.1	16.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	90		
0.375 in	9.50	83		
#4	4.75	69		
#10	2.00	51		
#20	0.85	37		
#40	0.42	29		
#60	0.25	24		
#100	0.15	20		
#140	0.11	18		
#200	0.075	16		

<u>Coefficients</u>	
D <sub>85</sub> = 10.1411 mm	D <sub>30</sub> = 0.4740 mm
D <sub>60</sub> = 3.0347 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 1.8370 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

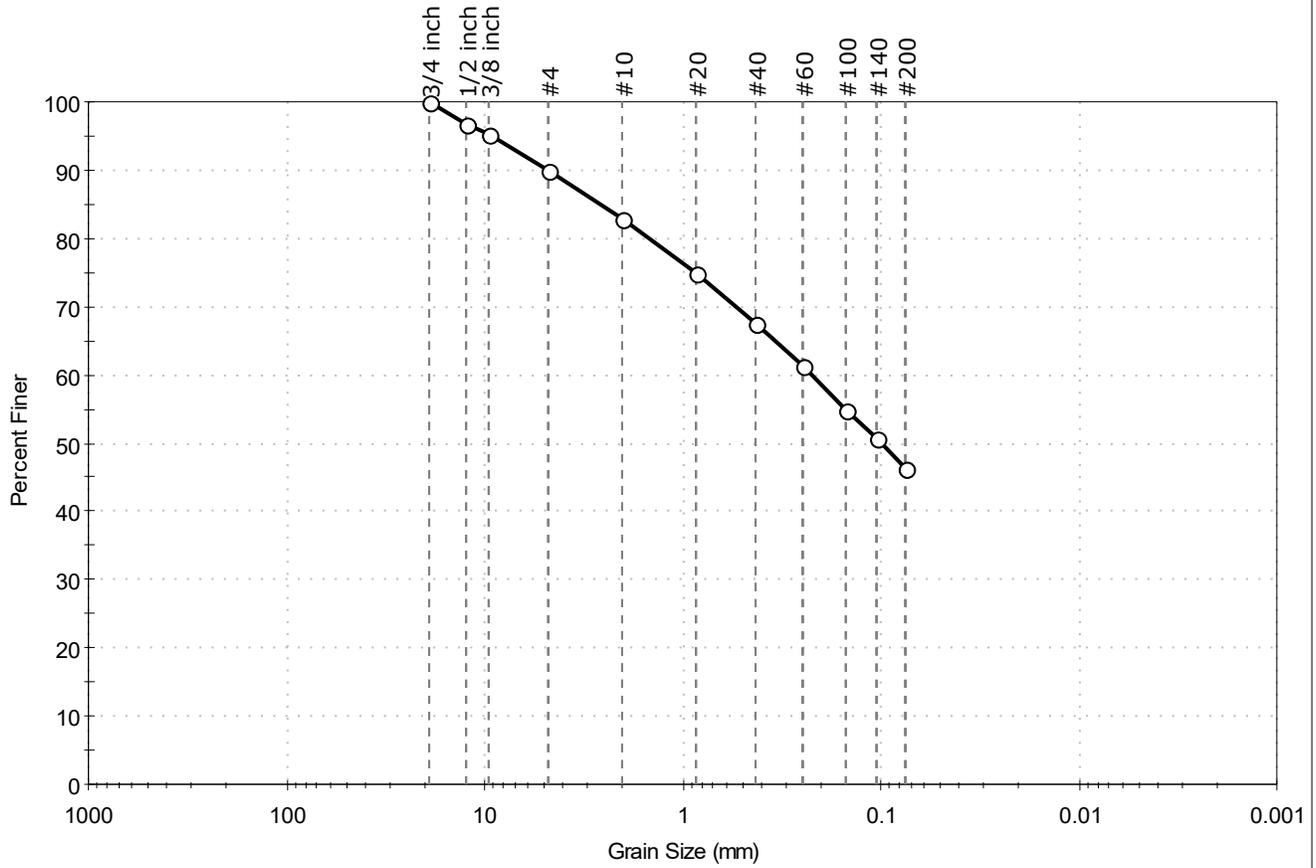
<u>Classification</u>	
ASTM	N/A
AASHTO	Stone Fragments, Gravel and Sand (A-1-b (0))

**Sample/Test Description**  
 Sand/Gravel Particle Shape : ANGULAR  
 Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-105	Sample Type:	Jar
Sample ID:	3D	Test Date:	08/19/24
Depth :	5-5.6 ft	Test Id:	780367
Test Comment:	---		
Visual Description:	Moist, dark grayish brown silty sand		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	10.0	43.6	46.4

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
3/4 inch	19.00	100		
1/2 inch	12.50	97		
3/8 inch	9.50	95		
#4	4.75	90		
#10	2.00	83		
#20	0.85	75		
#40	0.42	67		
#60	0.25	61		
#100	0.15	55		
#140	0.11	51		
#200	0.075	46		

<u>Coefficients</u>	
D <sub>85</sub> = 2.5683 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.2264 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.1002 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

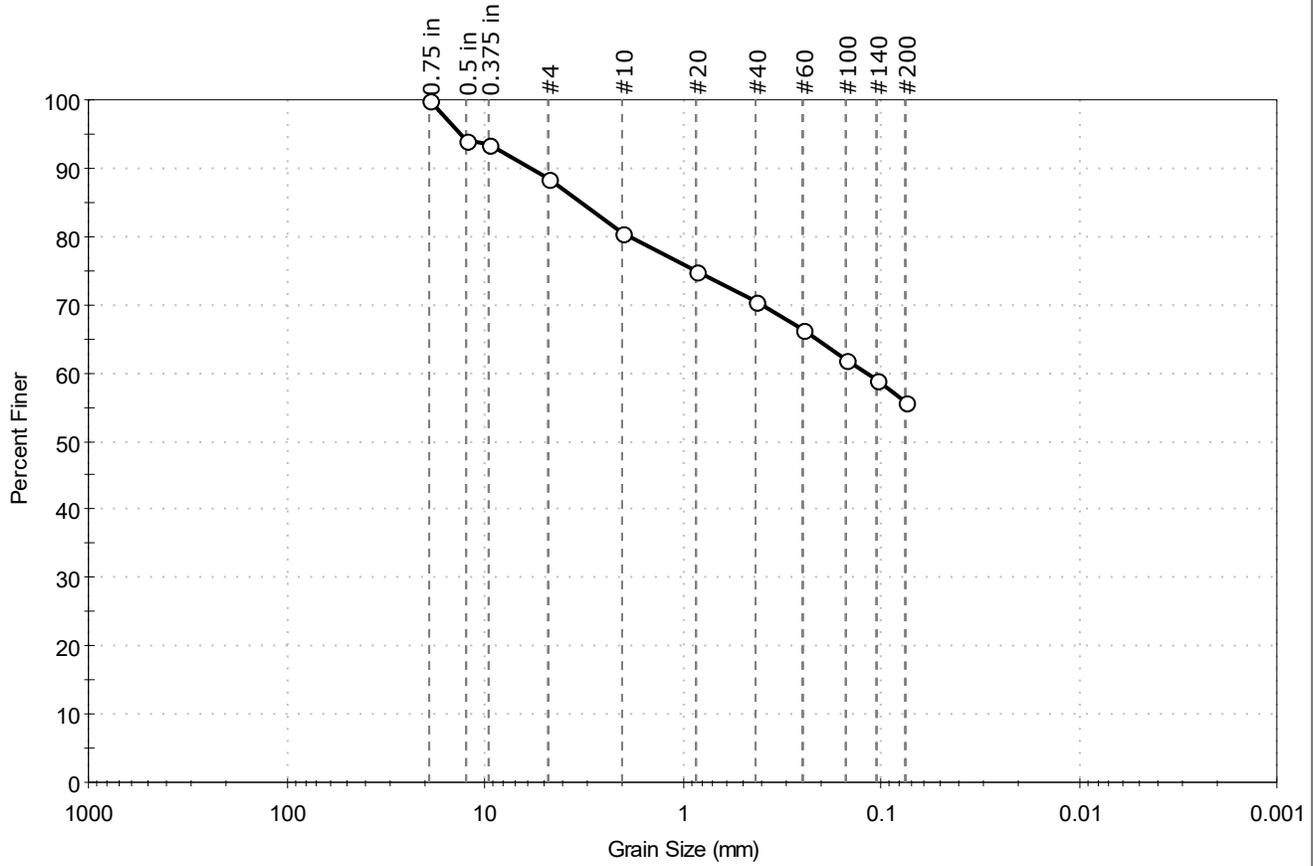
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-105	Sample Type: Jar
Sample ID: 6D	Test Date: 08/19/24
Depth: 15-17 ft	Test Id: 780368
Test Comment: ---	Tested By: ajl
Visual Description: Moist, grayish brown sandy silt	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	11.4	32.9	55.7

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	94		
0.375 in	9.50	93		
#4	4.75	89		
#10	2.00	81		
#20	0.85	75		
#40	0.42	70		
#60	0.25	67		
#100	0.15	62		
#140	0.11	59		
#200	0.075	56		

<u>Coefficients</u>	
D <sub>85</sub> = 3.2112 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.1201 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = N/A	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

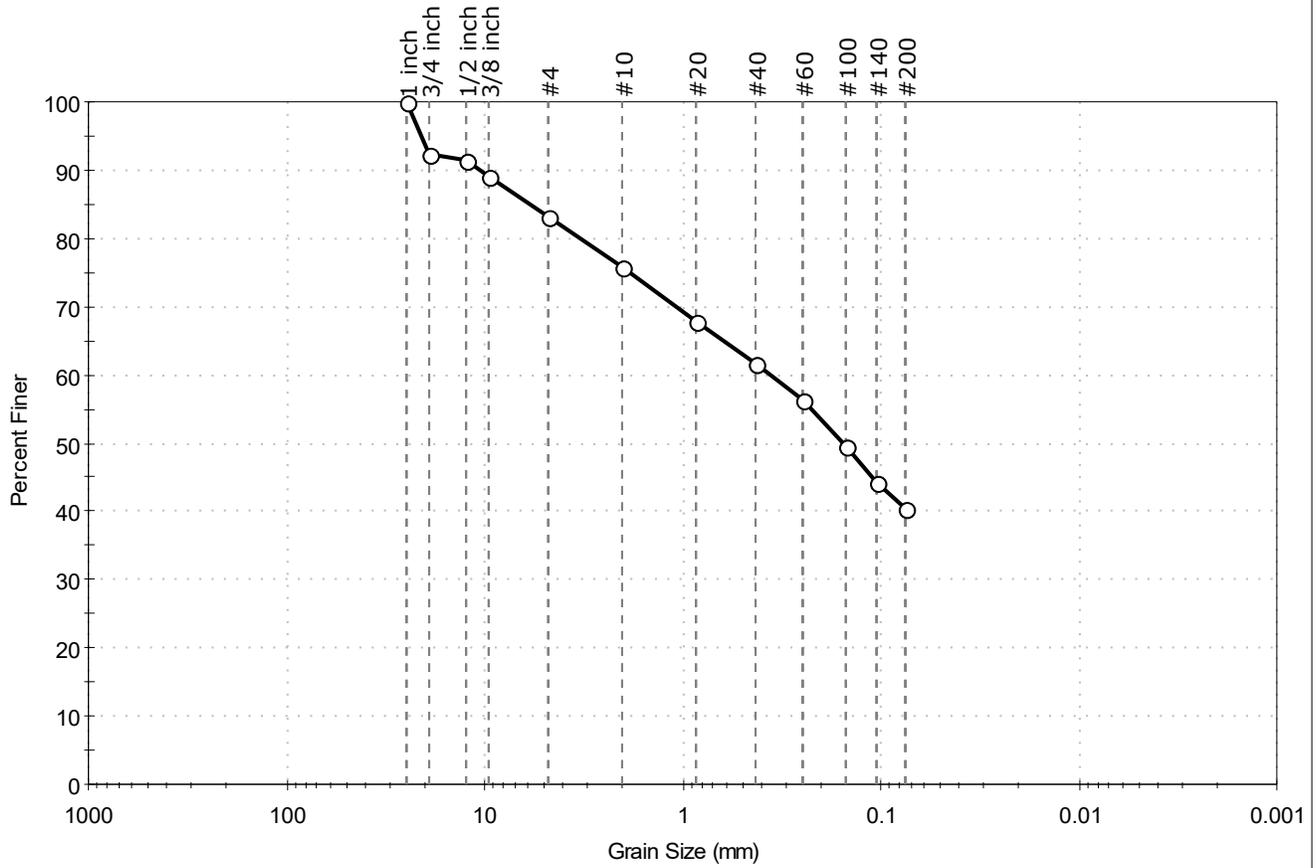
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-105	Sample Type:	Jar
Sample ID:	7D	Test Date:	08/19/24
Depth :	20-22ft	Test Id:	780369
Test Comment:	---		
Visual Description:	Moist, olive brown silty sand with gravel		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	16.9	42.8	40.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 inch	25.00	100		
3/4 inch	19.00	92		
1/2 inch	12.50	91		
3/8 inch	9.50	89		
#4	4.75	83		
#10	2.00	76		
#20	0.85	68		
#40	0.42	62		
#60	0.25	56		
#100	0.15	49		
#140	0.11	44		
#200	0.075	40		

<u>Coefficients</u>	
D <sub>85</sub> = 5.8920 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.3574 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.1564 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

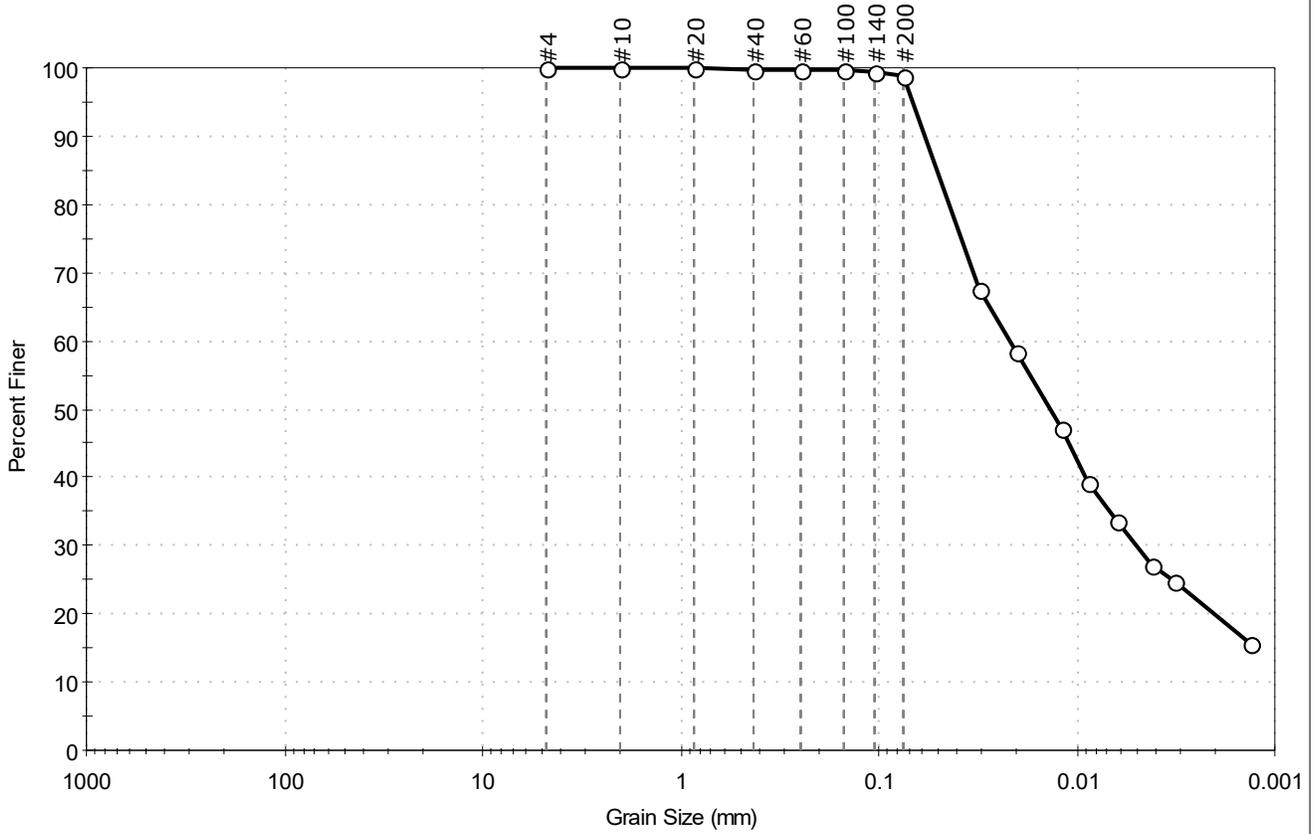
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-106	Sample Type:	Jar
Sample ID:	7D	Test Date:	08/15/24
Depth :	20-22 ft	Test Id:	780382
Test Comment:	---		
Visual Description:	Moist, light olive brown clay		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	1.1	98.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	100		
#140	0.11	99		
#200	0.075	99		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0314	67		
---	0.0203	58		
---	0.0121	47		
---	0.0087	39		
---	0.0062	34		
---	0.0042	27		
---	0.0032	25		
---	0.0013	16		

<u>Coefficients</u>	
D <sub>85</sub> = 0.0510 mm	D <sub>30</sub> = 0.0050 mm
D <sub>60</sub> = 0.0219 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.0137 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

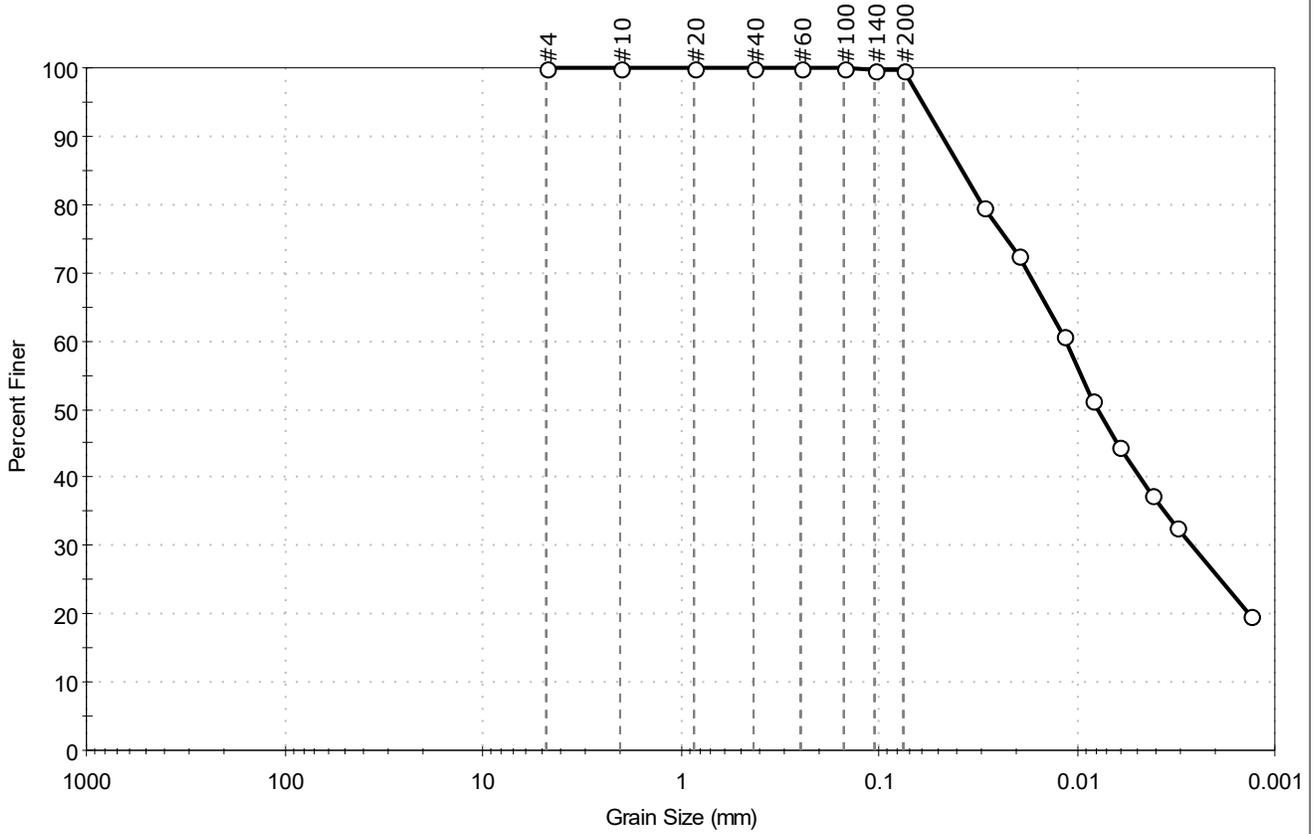
<u>Classification</u>	
<u>ASTM</u>	Lean CLAY (CL)
<u>AASHTO</u>	Clayey Soils (A-6 (19))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ---
Sand/Gravel Hardness : ---
Dispersion Device : Apparatus A - Mech Mixer
Dispersion Period : 1 minute
Est. Specific Gravity : 2.65
Separation of Sample: #200 Sieve



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-106	Sample Type: Jar
Sample ID: 8D	Test Date: 08/15/24
Depth: 25-27 ft	Test Id: 780383
Test Comment: ---	Tested By: ajl
Visual Description: Moist, grayish brown clay	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	0.3	99.7

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	100		
#140	0.11	100		
#200	0.075	100		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0298	80		
---	0.0196	73		
---	0.0117	61		
---	0.0084	51		
---	0.0061	44		
---	0.0042	37		
---	0.0031	33		
---	0.0013	20		

<b>Coefficients</b>	
D <sub>85</sub> = 0.0383 mm	D <sub>30</sub> = 0.0026 mm
D <sub>60</sub> = 0.0113 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.0079 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

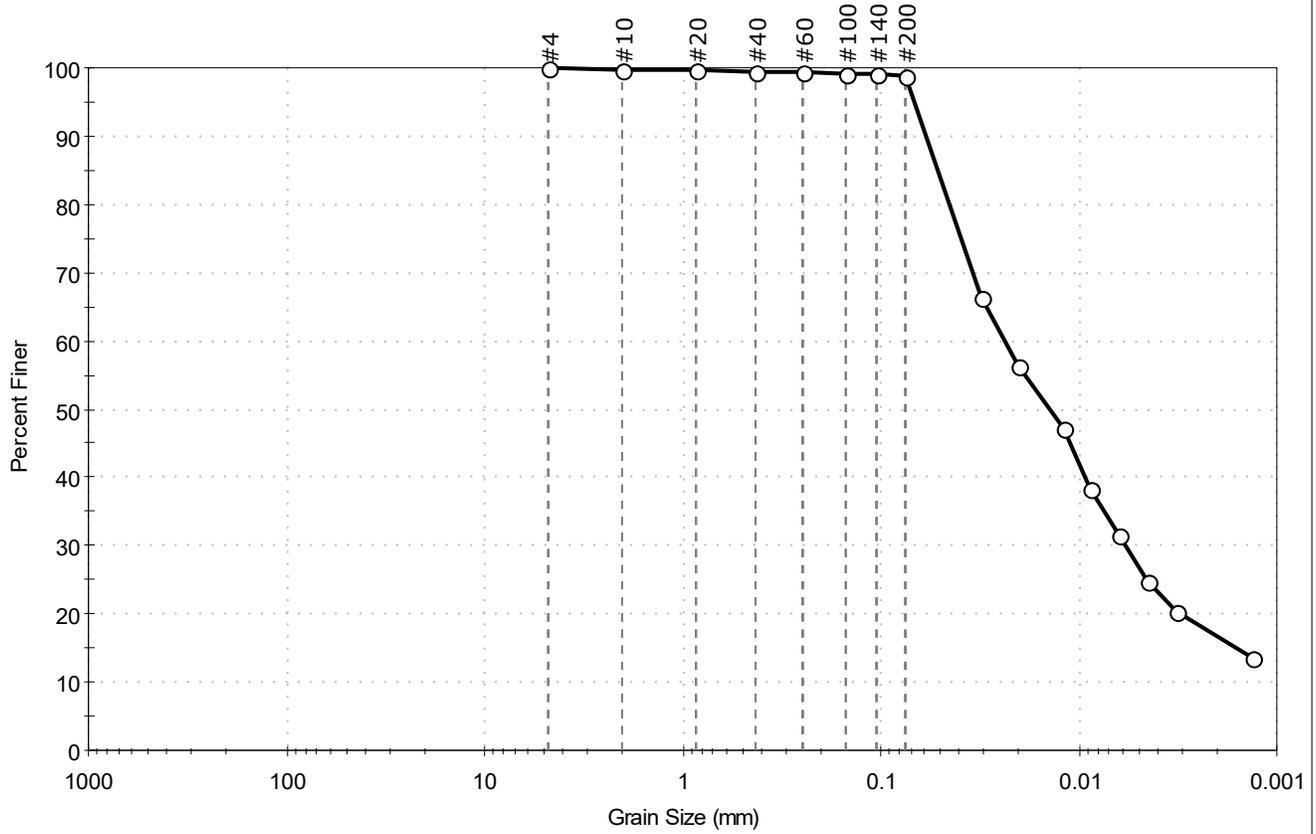
<b>Classification</b>	
<b>ASTM</b>	Lean CLAY (CL)
<b>AASHTO</b>	Clayey Soils (A-6 (18))

<b>Sample/Test Description</b>
Sand/Gravel Particle Shape : ---
Sand/Gravel Hardness : ---
Dispersion Device : Apparatus A - Mech Mixer
Dispersion Period : 1 minute
Est. Specific Gravity : 2.65
Separation of Sample: #200 Sieve



Client: WSP USA, Inc.  
 Project: MaineDOT I-95 Bridge over Stillwater  
 Location: Merrimack, NH  
 Project No: GTX-319180  
 Boring ID: BB-BSA-106  
 Sample Type: Jar  
 Tested By: ajl  
 Sample ID: 9D  
 Test Date: 08/15/24  
 Checked By: ank  
 Depth: 30-32 ft  
 Test Id: 780384  
 Test Comment: ---  
 Visual Description: Moist, gray clay  
 Sample Comment: ---

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	1.3	98.7

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	99		
#60	0.25	99		
#100	0.15	99		
#140	0.11	99		
#200	0.075	99		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0308	66		
---	0.0202	56		
---	0.0121	47		
---	0.0087	38		
---	0.0063	32		
---	0.0045	25		
---	0.0032	20		
---	0.0013	14		

<b>Coefficients</b>	
D <sub>85</sub> = 0.0515 mm	D <sub>30</sub> = 0.0058 mm
D <sub>60</sub> = 0.0236 mm	D <sub>15</sub> = 0.0016 mm
D <sub>50</sub> = 0.0141 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

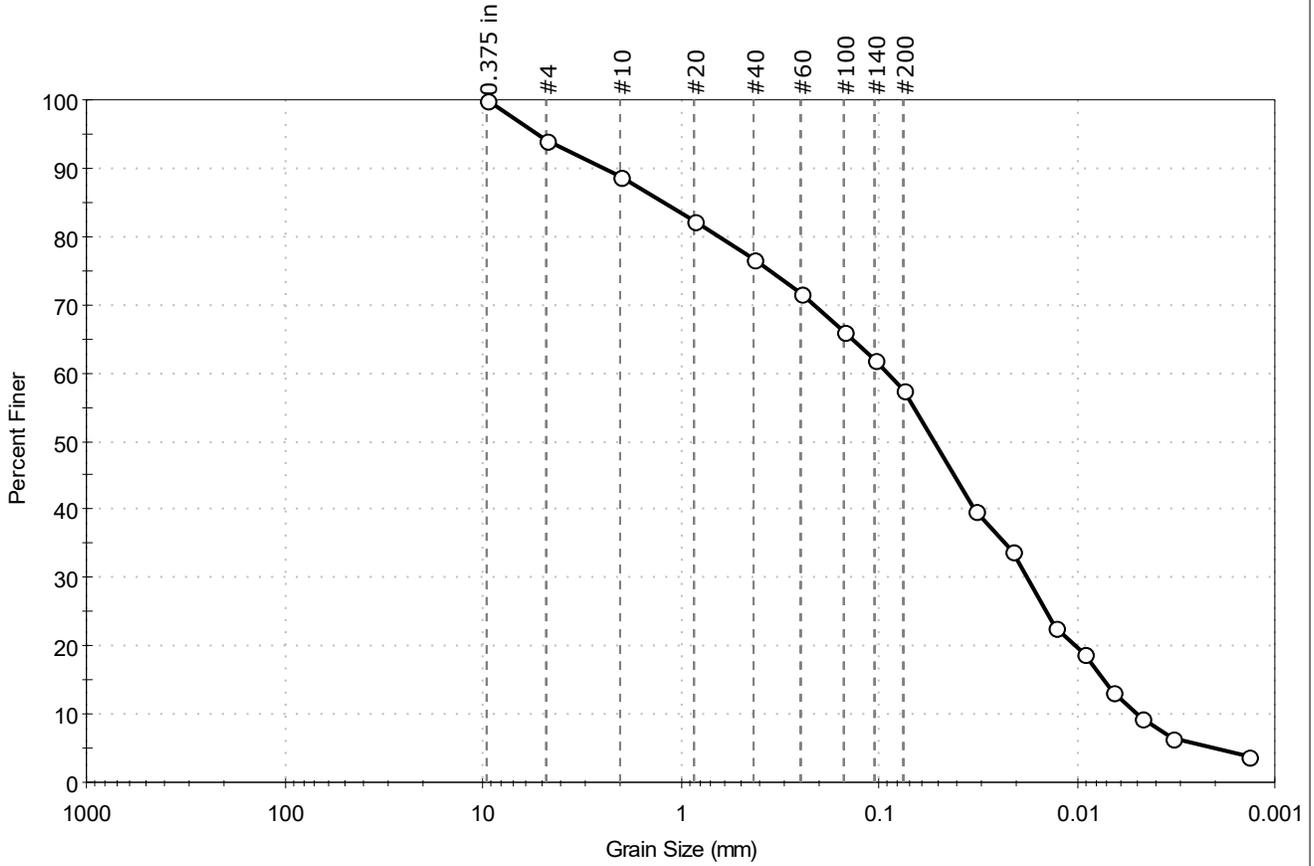
<b>Classification</b>	
<b>ASTM</b>	Lean CLAY (CL)
<b>AASHTO</b>	Clayey Soils (A-6 (9))

<b>Sample/Test Description</b>
Sand/Gravel Particle Shape : ---
Sand/Gravel Hardness : ---
Dispersion Device : Apparatus A - Mech Mixer
Dispersion Period : 1 minute
Est. Specific Gravity : 2.65
Separation of Sample: #200 Sieve



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-106	Sample Type:	Jar
Sample ID:	11D	Test Date:	08/15/24
Depth:	40-42 ft	Test Id:	780385
Test Comment:	---		
Visual Description:	Moist, gray sandy silt		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	6.0	36.4	57.6

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.375 in	9.50	100		
#4	4.75	94		
#10	2.00	89		
#20	0.85	82		
#40	0.42	77		
#60	0.25	72		
#100	0.15	66		
#140	0.11	62		
#200	0.075	58		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0327	40		
---	0.0212	34		
---	0.0128	23		
---	0.0091	19		
---	0.0065	13		
---	0.0047	9		
---	0.0033	7		
---	0.0014	4		

Coefficients	
D <sub>85</sub> = 1.2010 mm	D <sub>30</sub> = 0.0177 mm
D <sub>60</sub> = 0.0912 mm	D <sub>15</sub> = 0.0073 mm
D <sub>50</sub> = 0.0526 mm	D <sub>10</sub> = 0.0049 mm
C <sub>u</sub> = 18.612	C <sub>c</sub> = 0.701

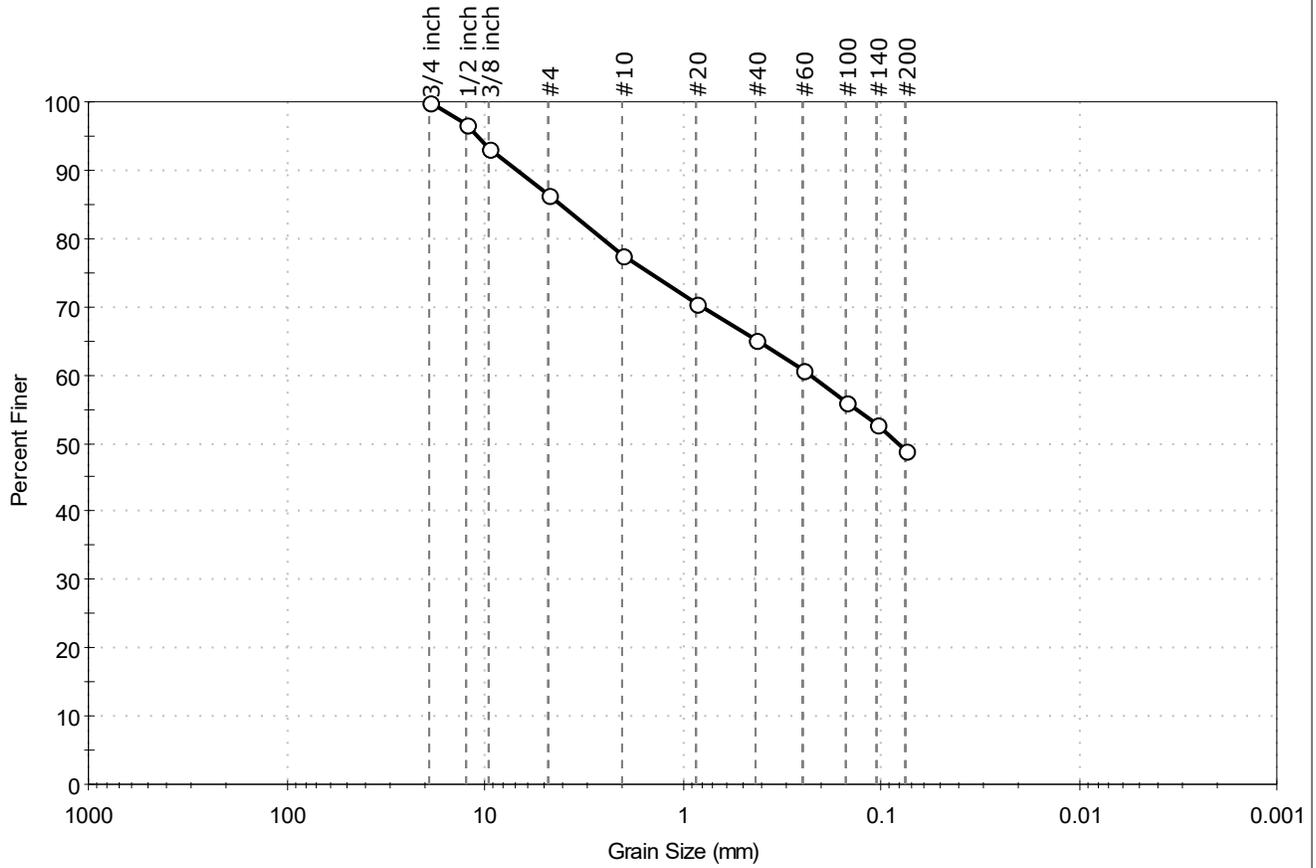
Classification	
ASTM	Sandy SILT (ML)
AASHTO	Silty Soils (A-4 (0))

Sample/Test Description
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD
Dispersion Device : Apparatus A - Mech Mixer
Dispersion Period : 1 minute
Est. Specific Gravity : 2.65
Separation of Sample: #200 Sieve



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-106	Sample Type: Jar
Sample ID: 14D	Test Date: 08/16/24
Depth: 55-57 ft	Test Id: 780380
Test Comment: ---	Tested By: ajl
Visual Description: Moist, gray silty sand	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	13.6	37.5	48.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
3/4 inch	19.00	100		
1/2 inch	12.50	97		
3/8 inch	9.50	93		
#4	4.75	86		
#10	2.00	77		
#20	0.85	70		
#40	0.42	65		
#60	0.25	61		
#100	0.15	56		
#140	0.11	53		
#200	0.075	49		

<u>Coefficients</u>	
D <sub>85</sub> = 4.1627 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.2272 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.0828 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

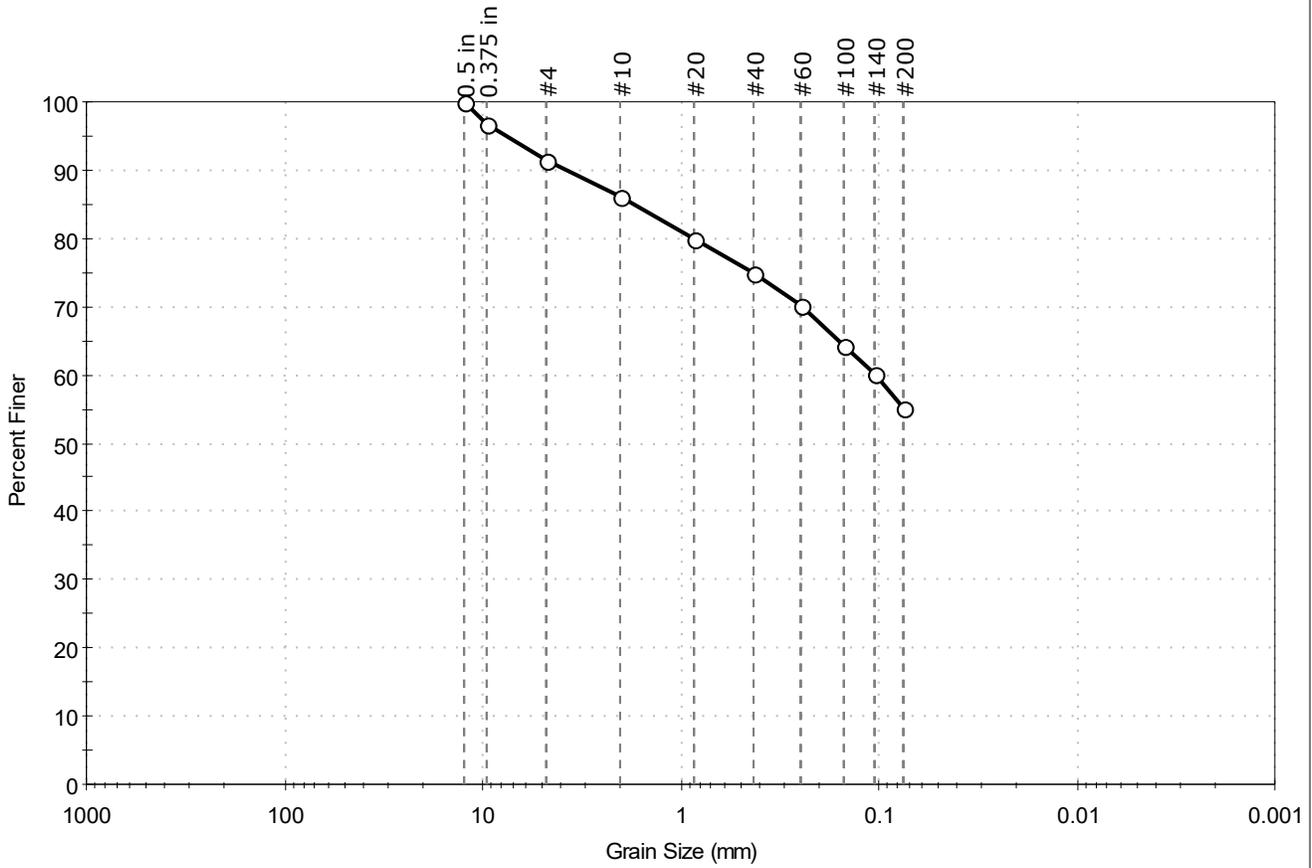
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-107	Sample Type: Jar
Sample ID: 3D	Test Date: 08/19/24
Depth: 4.7-6.7 ft	Test Id: 780391
Test Comment: ---	Tested By: ajl
Visual Description: Moist, grayish brown sandy silt	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	8.5	36.3	55.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.5 in	12.50	100		
0.375 in	9.50	97		
#4	4.75	92		
#10	2.00	86		
#20	0.85	80		
#40	0.42	75		
#60	0.25	70		
#100	0.15	64		
#140	0.11	60		
#200	0.075	55		

<u>Coefficients</u>	
D <sub>85</sub> = 1.6952 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.1052 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = N/A	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

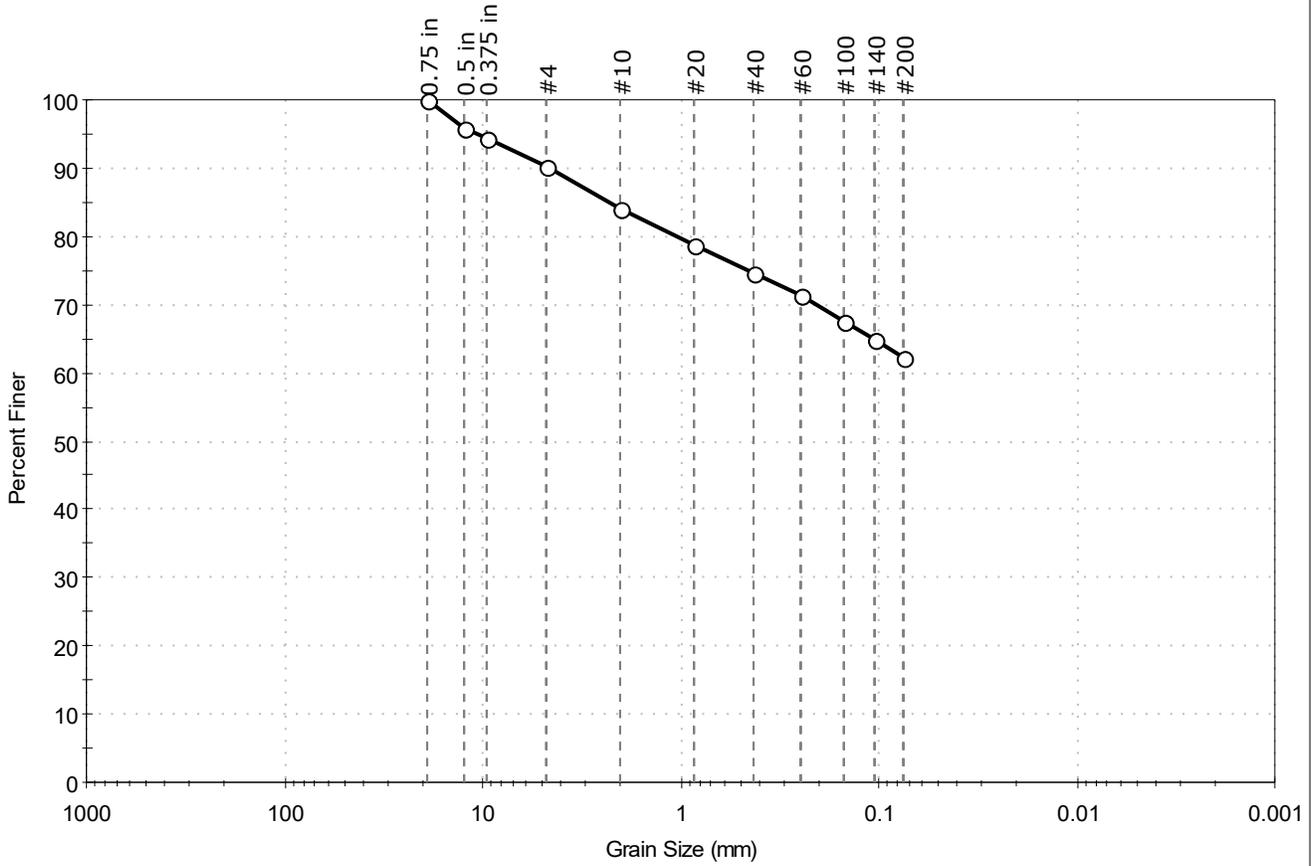
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-107	Sample Type:	Jar
Sample ID:	6D	Test Date:	08/19/24
Depth :	10.7-12.7 ft	Checked By:	ank
		Test Id:	780392
Test Comment:	---		
Visual Description:	Moist, olive brown silt with sand		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	9.7	28.0	62.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	96		
0.375 in	9.50	94		
#4	4.75	90		
#10	2.00	84		
#20	0.85	79		
#40	0.42	75		
#60	0.25	71		
#100	0.15	68		
#140	0.11	65		
#200	0.075	62		

<u>Coefficients</u>	
D <sub>85</sub> = 2.2895 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = N/A	D <sub>15</sub> = N/A
D <sub>50</sub> = N/A	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

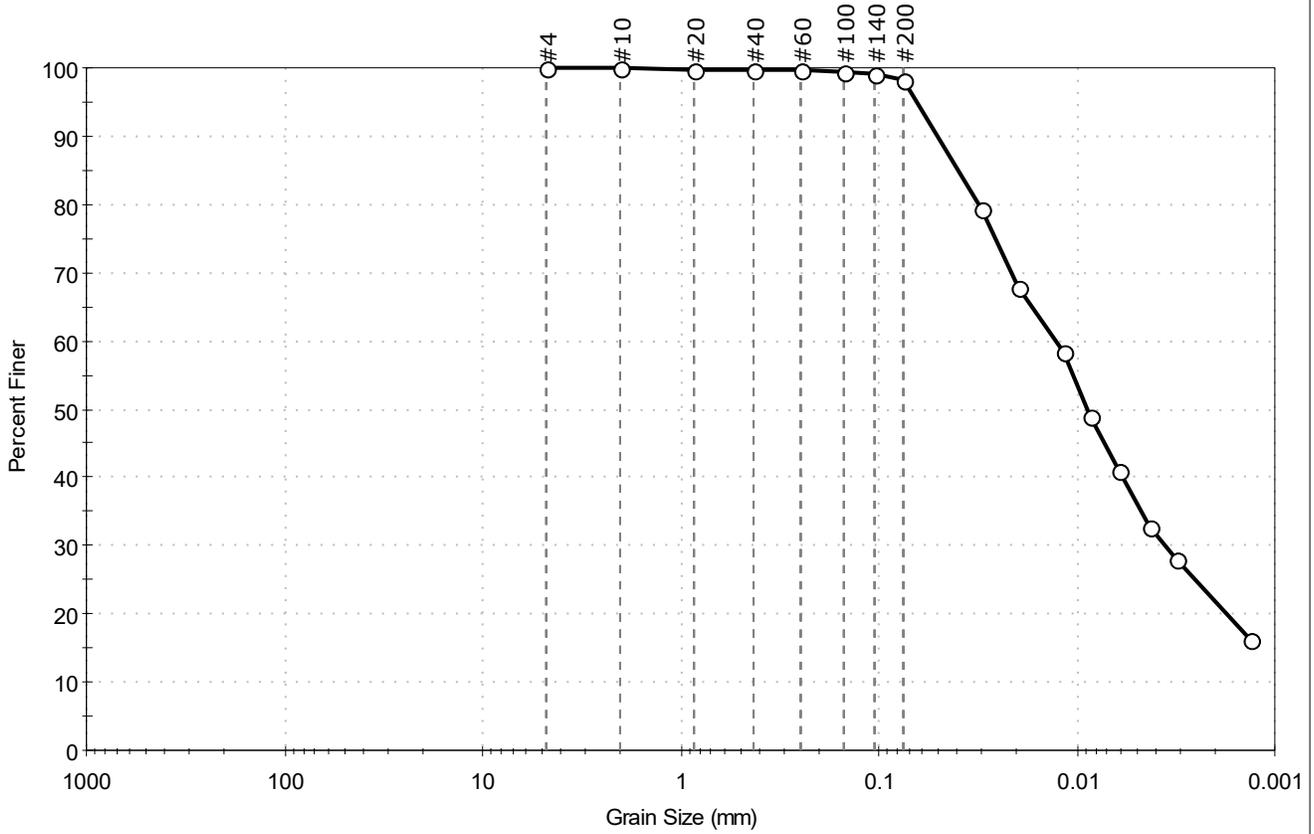
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH	Boring ID: BB-BSA-107	Sample Type: Jar
	Sample ID: 8D	Test Date: 08/15/24
	Depth: 20-22 ft	Test Id: 780395
Test Comment: ---	Visual Description: Moist, grayish brown clay	Checked By: ank
Sample Comment: ---		

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	1.7	98.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	99		
#140	0.11	99		
#200	0.075	98		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0303	79		
---	0.0196	68		
---	0.0117	58		
---	0.0085	49		
---	0.0061	41		
---	0.0043	33		
---	0.0032	28		
---	0.0013	16		

<b>Coefficients</b>	
D <sub>85</sub> = 0.0395 mm	D <sub>30</sub> = 0.0036 mm
D <sub>60</sub> = 0.0127 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.0088 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

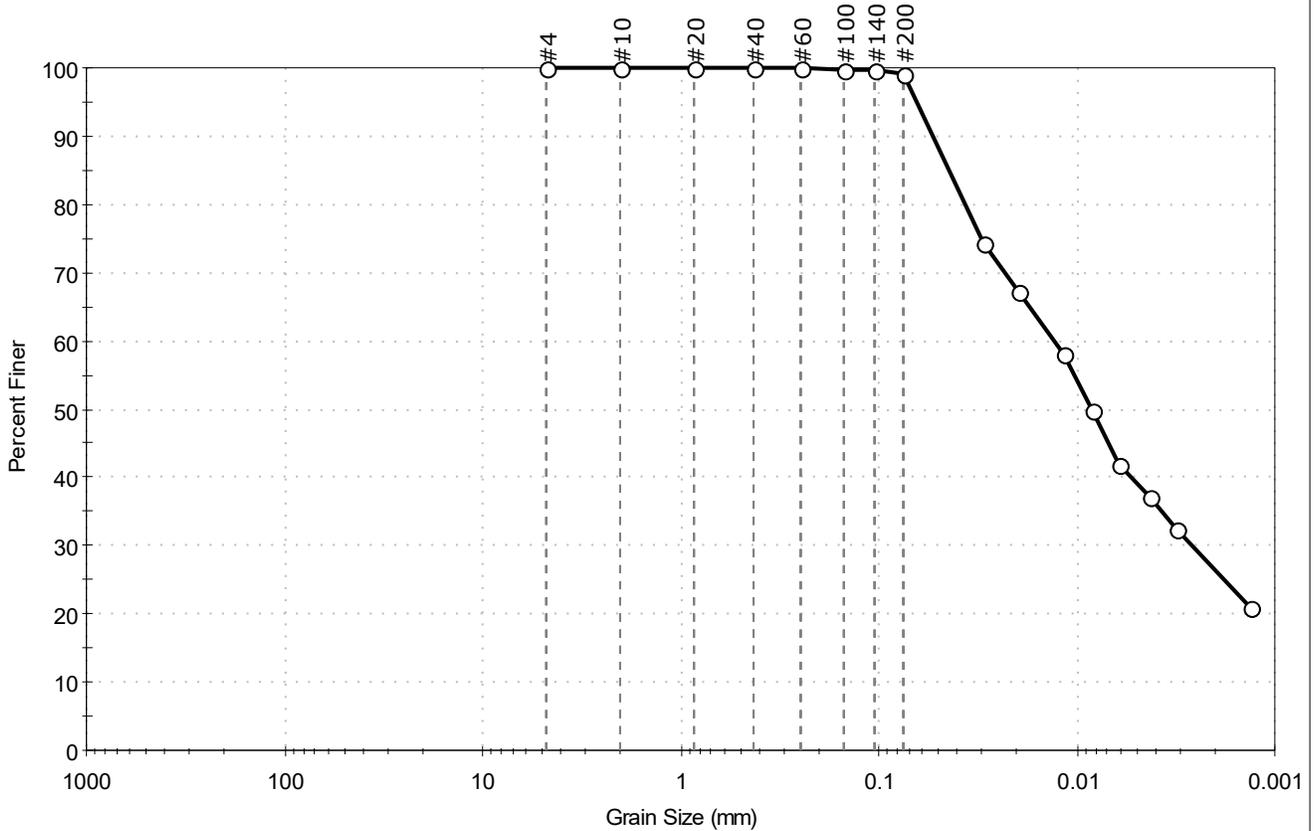
<b>Classification</b>	
<b>ASTM</b>	Lean CLAY (CL)
<b>AASHTO</b>	Clayey Soils (A-6 (15))

<b>Sample/Test Description</b>
Sand/Gravel Particle Shape : ---
Sand/Gravel Hardness : ---
Dispersion Device : Apparatus A - Mech Mixer
Dispersion Period : 1 minute
Est. Specific Gravity : 2.65
Separation of Sample: #200 Sieve



Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH	Boring ID: BB-BSA-107	Sample Type: Jar
	Sample ID: 9D	Test Date: 08/15/24
	Depth: 25-27 ft	Test Id: 780396
Test Comment: ---	Visual Description: Moist, olive brown clay	Checked By: ank
Sample Comment: ---		

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	0.7	99.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	100		
#140	0.11	100		
#200	0.075	99		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0295	74		
---	0.0198	67		
---	0.0117	58		
---	0.0083	50		
---	0.0061	42		
---	0.0043	37		
---	0.0031	33		
---	0.0013	21		

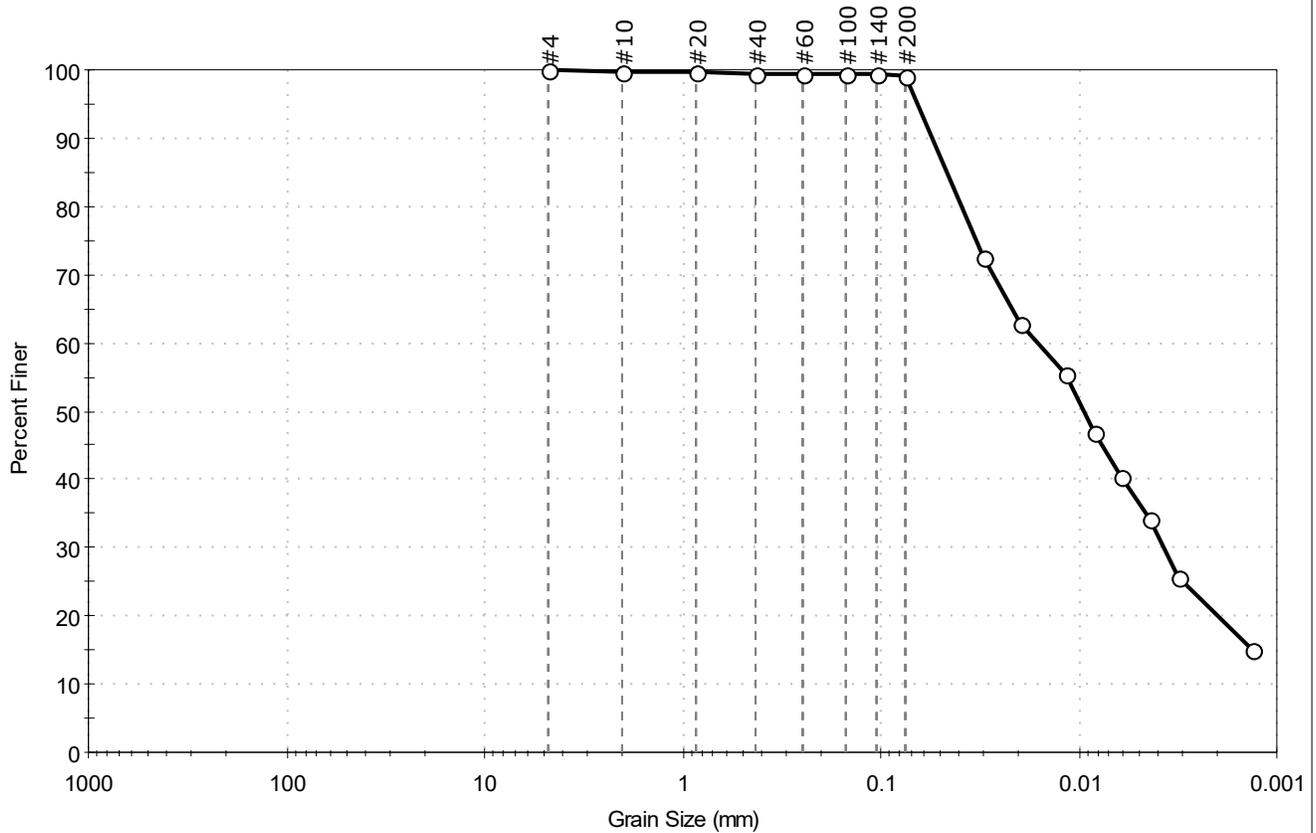
<b>Coefficients</b>	
D <sub>85</sub> = 0.0440 mm	D <sub>30</sub> = 0.0026 mm
D <sub>60</sub> = 0.0131 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.0084 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

<b>Classification</b>	
<b>ASTM</b>	Lean CLAY (CL)
<b>AASHTO</b>	Clayey Soils (A-6 (37))

<b>Sample/Test Description</b>
Sand/Gravel Particle Shape : ---
Sand/Gravel Hardness : ---
Dispersion Device : Apparatus A - Mech Mixer
Dispersion Period : 1 minute
Est. Specific Gravity : 2.65
Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH	Boring ID: BB-BSA-107	Sample Type: Jar
	Sample ID: 10D	Test Date: 08/15/24
	Depth: 30-32 ft	Test Id: 780397
Test Comment: ---	Visual Description: Moist, grayish brown clay	Checked By: ank
Sample Comment: ---		

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	0.9	99.1

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	99		
#100	0.15	99		
#140	0.11	99		
#200	0.075	99		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0305	73		
---	0.0196	63		
---	0.0117	55		
---	0.0085	47		
---	0.0061	41		
---	0.0044	34		
---	0.0032	26		
---	0.0013	15		

**Coefficients**

D <sub>85</sub> = 0.0465 mm	D <sub>30</sub> = 0.0037 mm
D <sub>60</sub> = 0.0160 mm	D <sub>15</sub> = 0.0013 mm
D <sub>50</sub> = 0.0095 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

**Classification**

ASTM    Lean CLAY (CL)

AASHTO    Clayey Soils (A-6 (11))

**Sample/Test Description**

Sand/Gravel Particle Shape : ---

Sand/Gravel Hardness : ---

Dispersion Device : Apparatus A - Mech Mixer

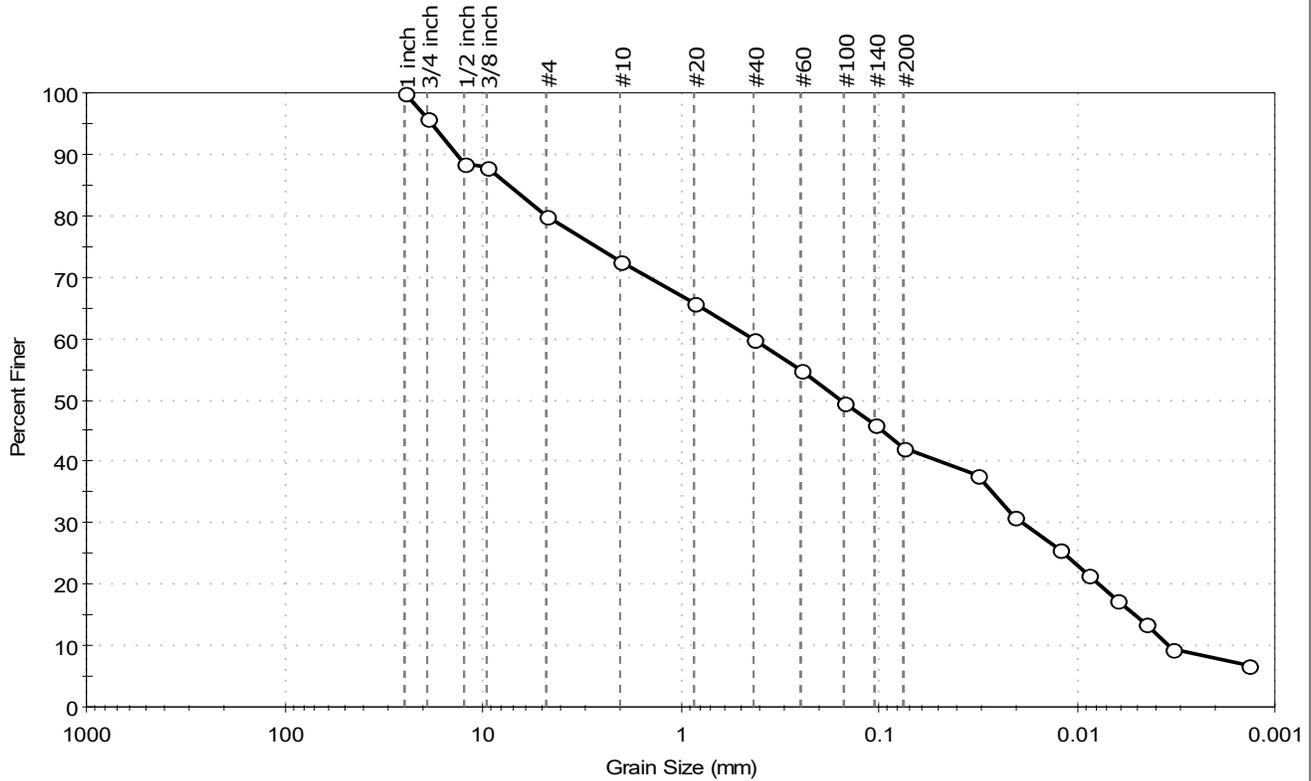
Dispersion Period : 1 minute

Est. Specific Gravity : 2.65

Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-107	Sample Type: Jar
Sample ID: 12D	Test Date: 08/15/24
Depth: 40-42 ft	Test Id: 781642
Test Comment: ---	Tested By: ajl
Visual Description: Moist, brownish gray silty clayey sand with gravel	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	19.9	38.0	42.1

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 inch	25.00	100		
3/4 inch	19.00	96		
1/2 inch	12.50	88		
3/8 inch	9.50	88		
#4	4.75	80		
#10	2.00	73		
#20	0.85	66		
#40	0.42	60		
#60	0.25	55		
#100	0.15	49		
#140	0.11	46		
#200	0.075	42		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0320	38		
---	0.0207	31		
---	0.0122	26		
---	0.0088	22		
---	0.0063	17		
---	0.0045	13		
---	0.0033	9		
---	0.0014	7		

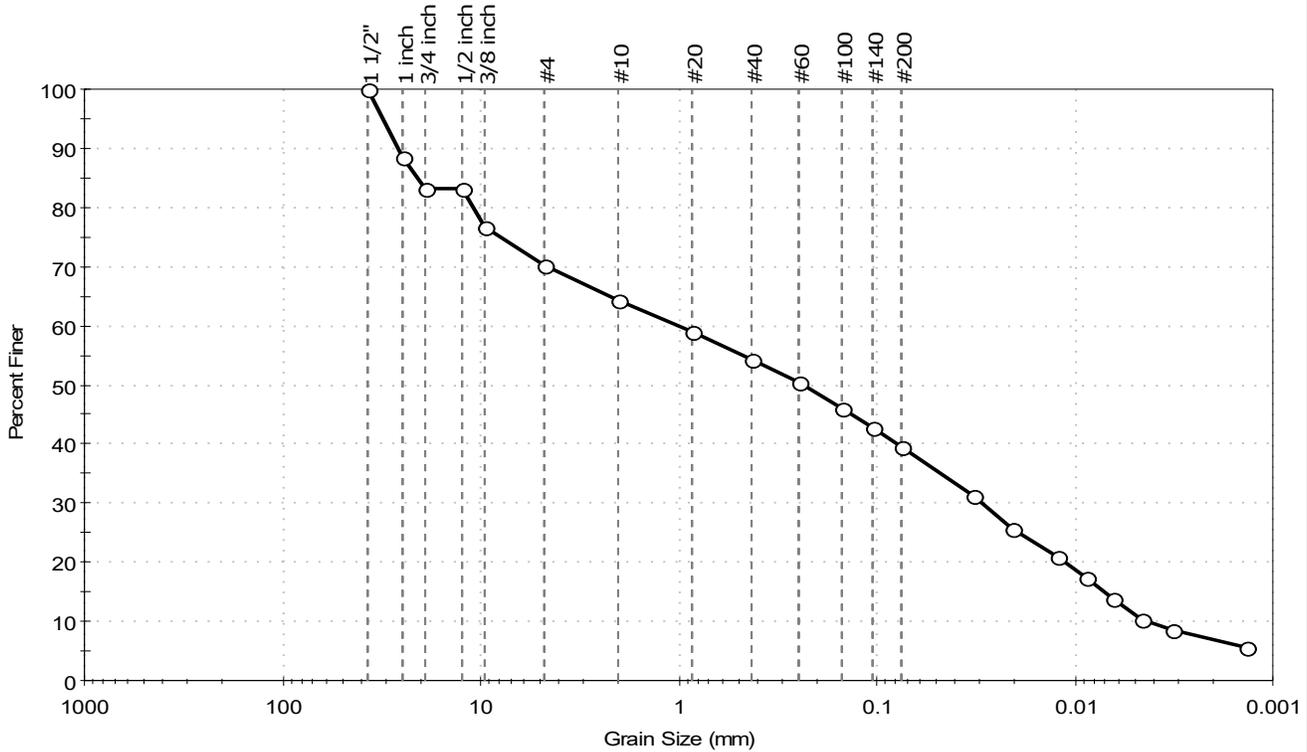
<u>Coefficients</u>	
D <sub>85</sub> = 7.3626 mm	D <sub>30</sub> = 0.0188 mm
D <sub>60</sub> = 0.4262 mm	D <sub>15</sub> = 0.0052 mm
D <sub>50</sub> = 0.1580 mm	D <sub>10</sub> = 0.0034 mm
C <sub>u</sub> = 125.353	C <sub>c</sub> = 0.244

<u>Classification</u>	
<u>ASTM</u>	Silty, Clayey SAND with Gravel (SC-SM)
<u>AASHTO</u>	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>	
Sand/Gravel Particle Shape : ANGULAR	
Sand/Gravel Hardness : HARD	
Dispersion Device : Apparatus A - Mech Mixer	
Dispersion Period : 1 minute	
Est. Specific Gravity : 2.65	
Separation of Sample: #200 Sieve	

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-107	Sample Type: Jar
Sample ID: 14D	Test Date: 08/15/24
Depth: 50-52 ft	Test Id: 780394
Test Comment: ---	Tested By: ajl
Visual Description: Moist, grayish brown clayey sand with gravel	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	29.9	30.5	39.6

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 1/2"	37.50	100		
1 inch	25.00	89		
3/4 inch	19.00	83		
1/2 inch	12.50	83		
3/8 inch	9.50	77		
#4	4.75	70		
#10	2.00	64		
#20	0.85	59		
#40	0.42	54		
#60	0.25	51		
#100	0.15	46		
#140	0.11	43		
#200	0.075	40		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0325	31		
---	0.0209	26		
---	0.0123	21		
---	0.0088	17		
---	0.0064	14		
---	0.0046	10		
---	0.0033	9		
---	0.0014	6		

<b>Coefficients</b>	
D <sub>85</sub> = 20.8858 mm	D <sub>30</sub> = 0.0294 mm
D <sub>60</sub> = 0.9990 mm	D <sub>15</sub> = 0.0071 mm
D <sub>50</sub> = 0.2343 mm	D <sub>10</sub> = 0.0042 mm
C <sub>u</sub> = 237.857	C <sub>c</sub> = 0.206

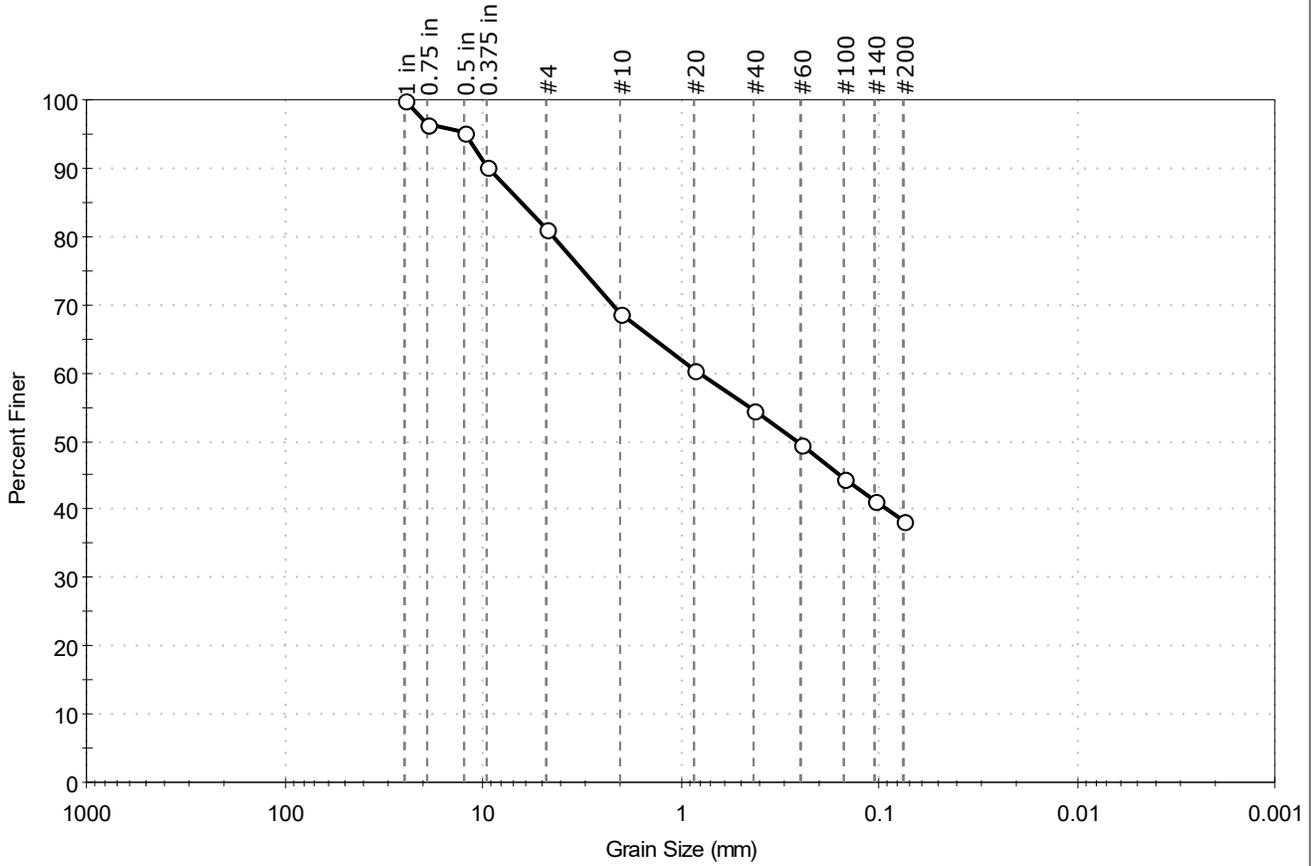
<b>Classification</b>	
<b>ASTM</b>	Clayey SAND with Gravel (SC)
<b>AASHTO</b>	Silty Soils (A-4 (0))

<b>Sample/Test Description</b>	
Sand/Gravel Particle Shape : ANGULAR	
Sand/Gravel Hardness : HARD	
Dispersion Device : Apparatus A - Mech Mixer	
Dispersion Period : 1 minute	
Est. Specific Gravity : 2.65	
Separation of Sample: #200 Sieve	



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-107	Sample Type: Jar
Sample ID: 15D	Test Date: 08/16/24
Depth: 55-57 ft	Test Id: 780393
Test Comment: ---	Tested By: ajl
Visual Description: Moist, grayish brown silty sand with gravel	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	19.0	42.7	38.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	96		
0.5 in	12.50	95		
0.375 in	9.50	90		
#4	4.75	81		
#10	2.00	69		
#20	0.85	61		
#40	0.42	55		
#60	0.25	50		
#100	0.15	45		
#140	0.11	41		
#200	0.075	38		

<u>Coefficients</u>	
D <sub>85</sub> = 6.3985 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.7963 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.2606 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

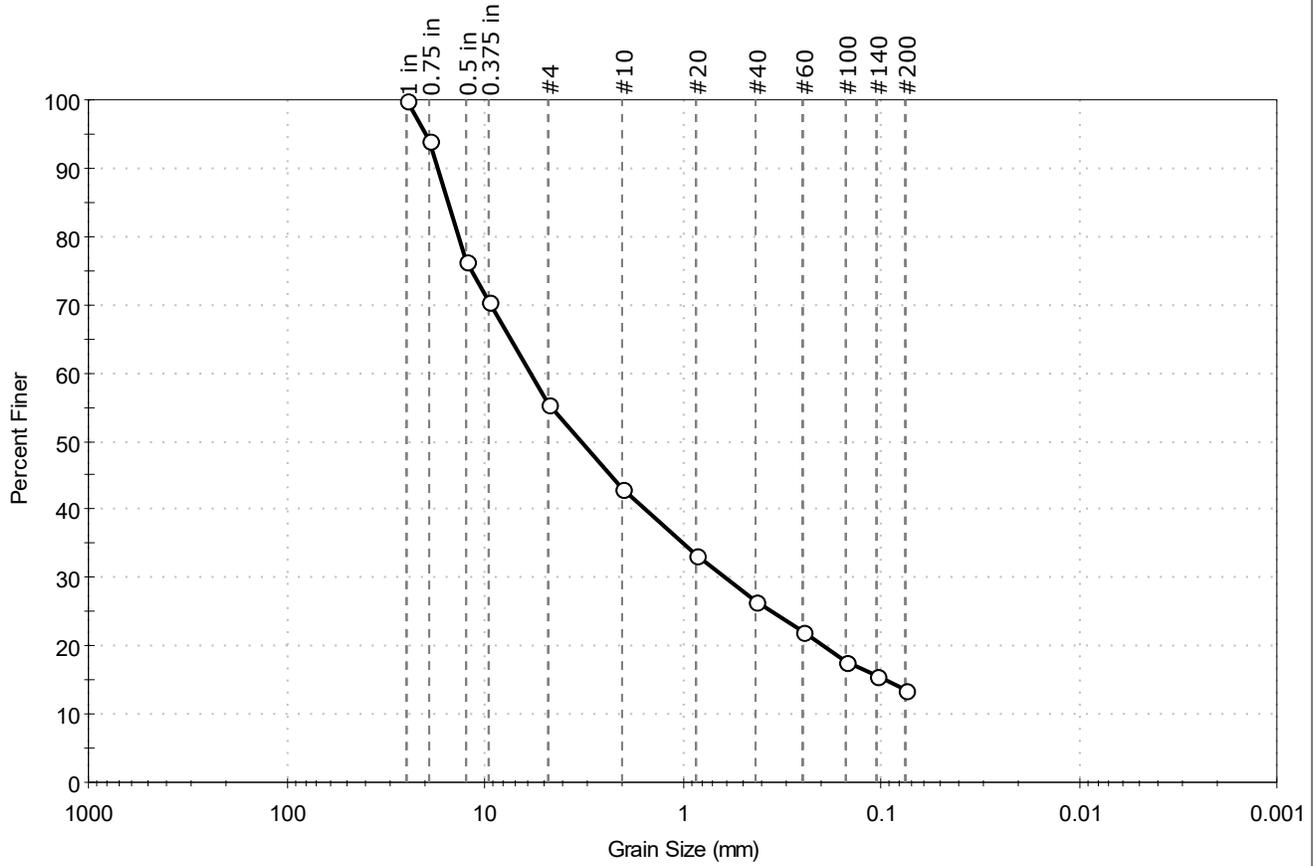
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-111	Sample Type:	Jar
Sample ID:	1D	Test Date:	08/16/24
Depth :	1-3 ft	Tested By:	ajl
		Checked By:	ank
Test Comment:	---		
Visual Description:	Moist, olive brown silty gravel with sand		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	44.5	42.0	13.5

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	94		
0.5 in	12.50	76		
0.375 in	9.50	70		
#4	4.75	55		
#10	2.00	43		
#20	0.85	33		
#40	0.42	27		
#60	0.25	22		
#100	0.15	18		
#140	0.11	16		
#200	0.075	13		

<u>Coefficients</u>	
D <sub>85</sub> = 15.3239 mm	D <sub>30</sub> = 0.5991 mm
D <sub>60</sub> = 5.8553 mm	D <sub>15</sub> = 0.0959 mm
D <sub>50</sub> = 3.2528 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

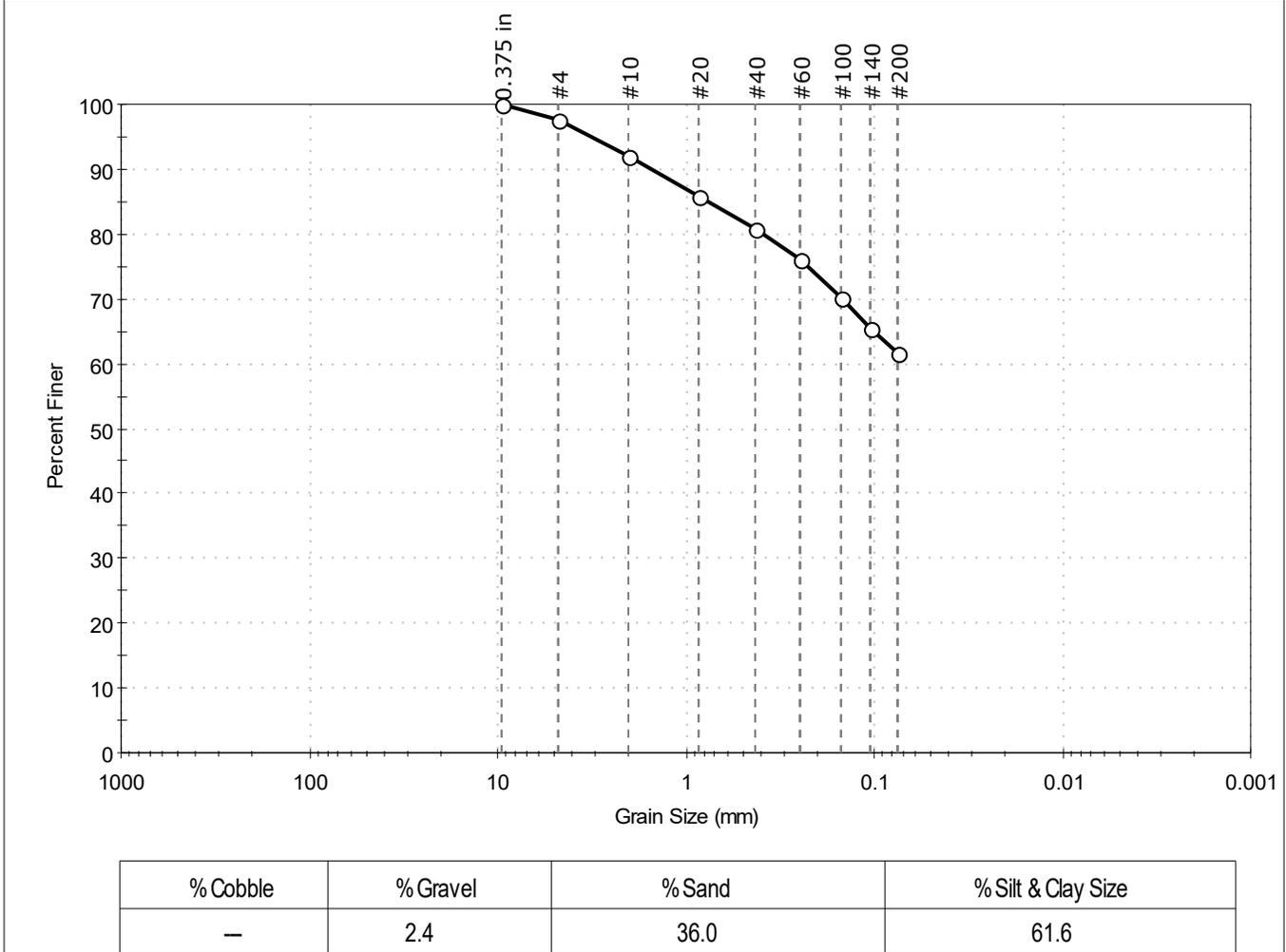
<u>Classification</u>	
ASTM	N/A
AASHTO	Stone Fragments, Gravel and Sand (A-1-a (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-111	Sample Type: Jar
Sample ID: 3D	Test Date: 08/19/24
Depth: 5-7 ft	Test Id: 780420
Test Comment: ---	Tested By: ajl
Visual Description: Moist, light olive brown sandy silt	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913



Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.375 in	9.50	100		
#4	4.75	98		
#10	2.00	92		
#20	0.85	86		
#40	0.42	81		
#60	0.25	76		
#100	0.15	70		
#140	0.11	66		
#200	0.075	62		

<b>Coefficients</b>	
D <sub>85</sub> = 0.7542 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = N/A	D <sub>15</sub> = N/A
D <sub>50</sub> = N/A	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

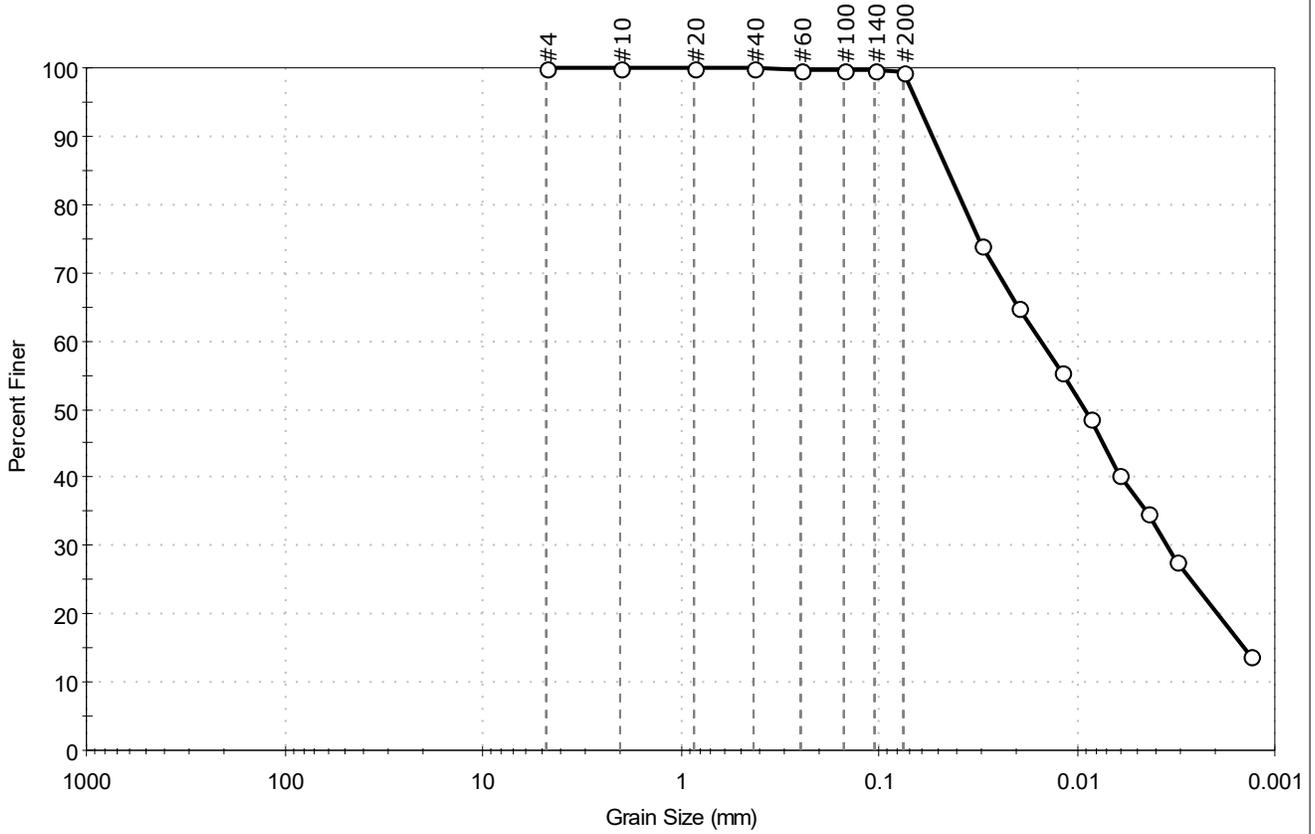
<b>Classification</b>	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

<b>Sample/Test Description</b>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-111	Sample Type: Jar
Sample ID: 5D	Test Date: 08/15/24
Depth: 10-12 ft	Test Id: 780422
Test Comment: ---	Tested By: ajl
Visual Description: Moist, olive brown clay	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	0.6	99.4

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	100		
#140	0.11	100		
#200	0.075	99		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0305	74		
---	0.0196	65		
---	0.0118	56		
---	0.0085	49		
---	0.0061	40		
---	0.0044	35		
---	0.0032	28		
---	0.0013	14		

<b>Coefficients</b>	
D <sub>85</sub> = 0.0450 mm	D <sub>30</sub> = 0.0035 mm
D <sub>60</sub> = 0.0151 mm	D <sub>15</sub> = 0.0014 mm
D <sub>50</sub> = 0.0091 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

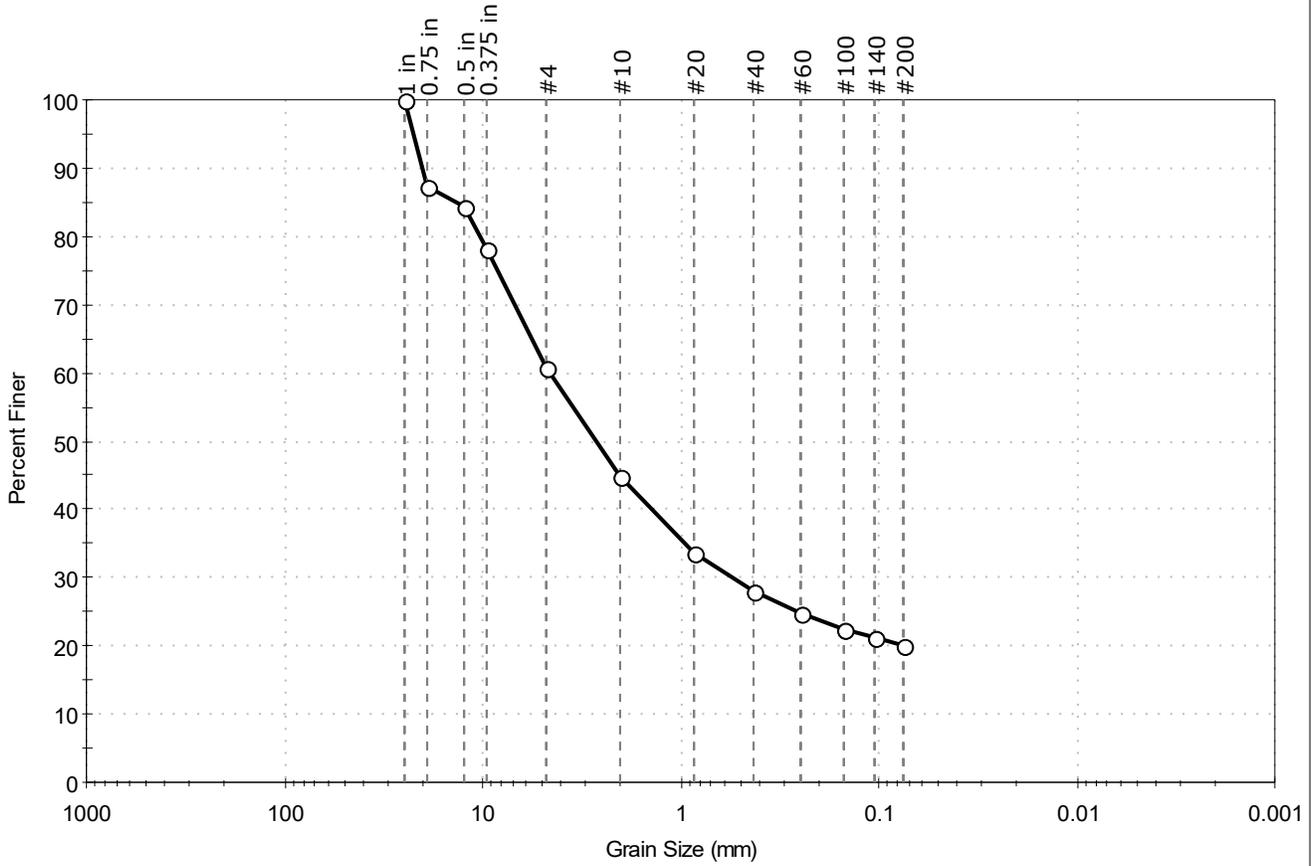
<b>Classification</b>	
<b>ASTM</b>	Lean CLAY (CL)
<b>AASHTO</b>	Clayey Soils (A-6 (15))

<b>Sample/Test Description</b>
Sand/Gravel Particle Shape : ---
Sand/Gravel Hardness : ---
Dispersion Device : Apparatus A - Mech Mixer
Dispersion Period : 1 minute
Est. Specific Gravity : 2.65
Separation of Sample: #200 Sieve



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-111	Sample Type:	Jar
Sample ID:	6D	Test Date:	08/16/24
Depth :	15-17 ft	Test Id:	780421
Test Comment:	---		
Visual Description:	Moist, grayish brown silty sand with gravel		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	39.3	40.7	20.0

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	87		
0.5 in	12.50	84		
0.375 in	9.50	78		
#4	4.75	61		
#10	2.00	45		
#20	0.85	34		
#40	0.42	28		
#60	0.25	25		
#100	0.15	22		
#140	0.11	21		
#200	0.075	20		

<u>Coefficients</u>	
D <sub>85</sub> = 13.6712 mm	D <sub>30</sub> = 0.5440 mm
D <sub>60</sub> = 4.5692 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 2.6581 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

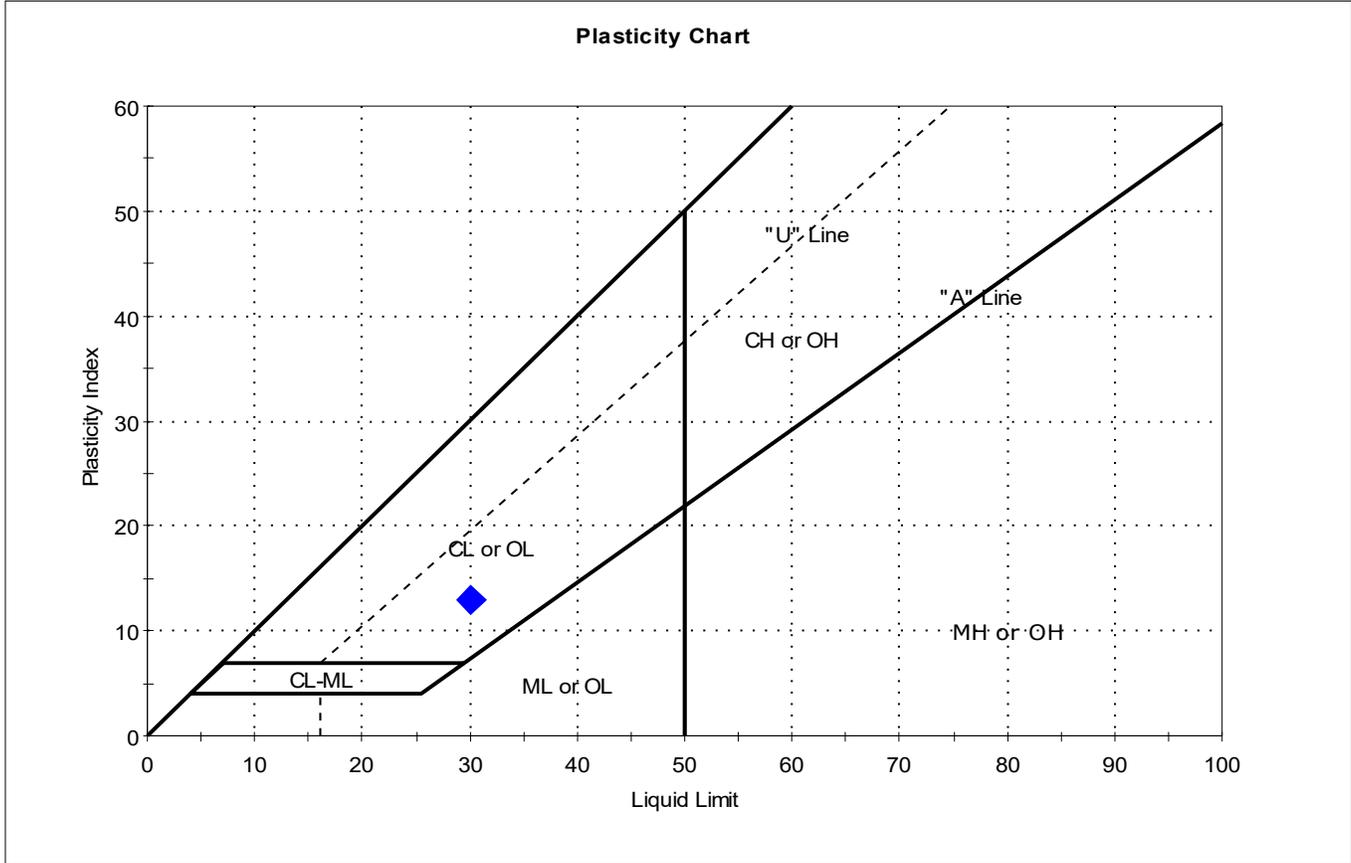
<u>Classification</u>	
ASTM	N/A
AASHTO	Stone Fragments, Gravel and Sand (A-1-b (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-104	Sample Type:	Jar
Sample ID:	6D	Test Date:	08/16/24
Depth:	15-17 ft	Test Id:	780409
Test Comment:	---		
Visual Description:	Moist, grayish brown clay		
Sample Comment:	---		

## Atterberg Limits - ASTM D4318



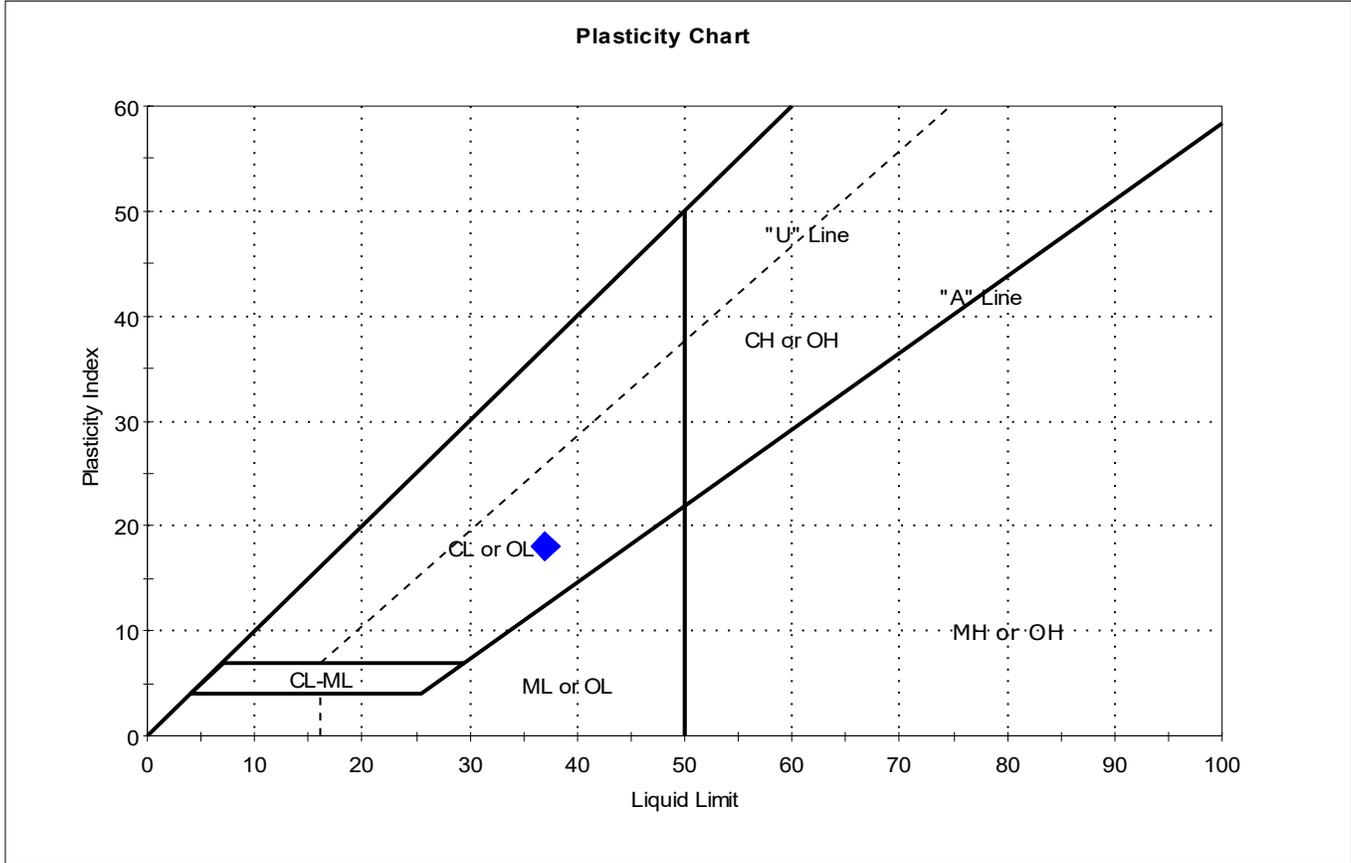
Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	6D	B-BSA-10	15-17 ft	25	30	17	13	0.6	Lean CLAY (CL)

Sample Prepared using the WET method  
 5% Retained on #40 Sieve  
 Dry Strength: VERY HIGH  
 Dilatancy: SLOW  
 Toughness: LOW



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-106	Sample Type:	Jar
Sample ID:	7D	Test Date:	08/19/24
Depth :	20-22 ft	Test Id:	780372
Test Comment:	---		
Visual Description:	Moist, light olive brown clay		
Sample Comment:	---		

## Atterberg Limits - ASTM D4318



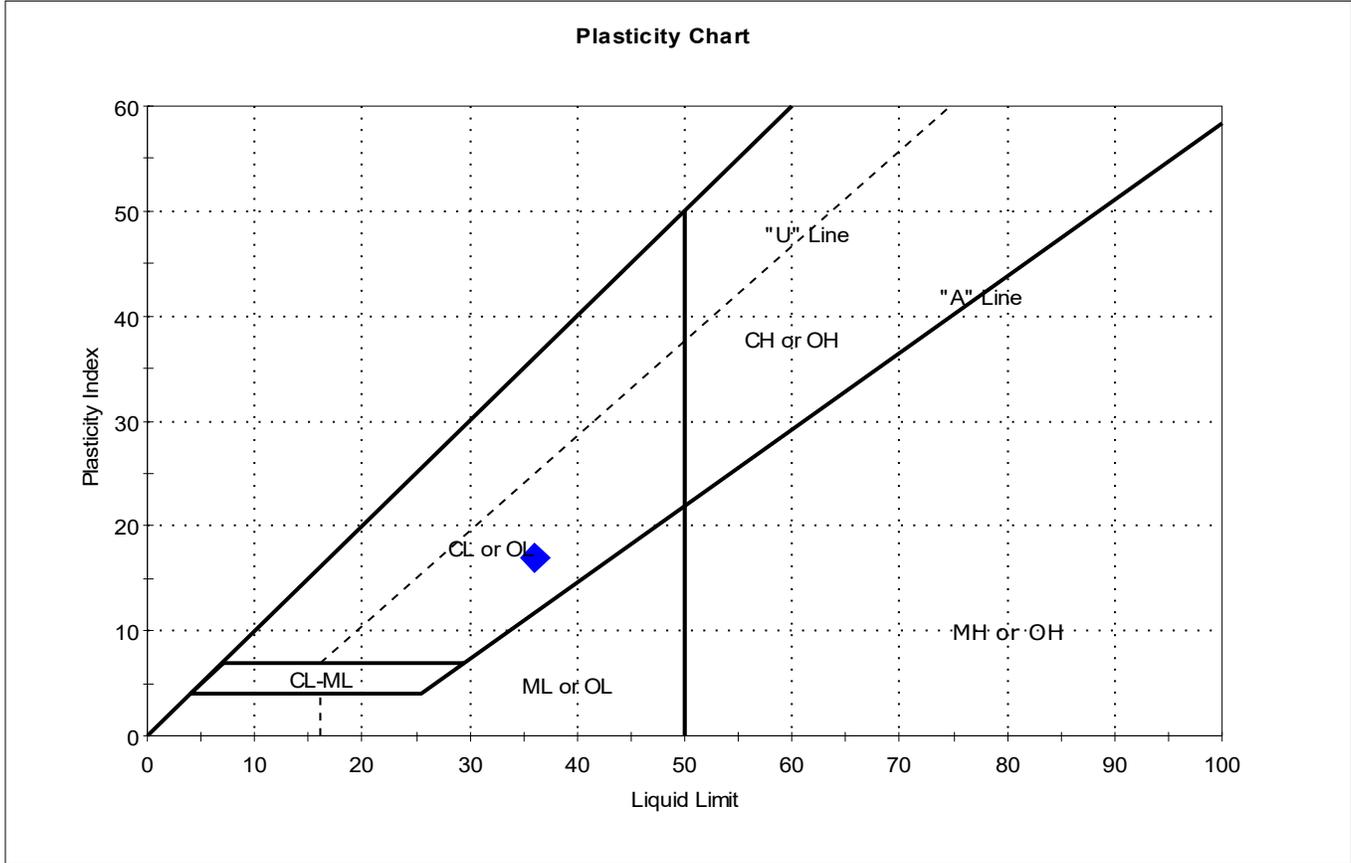
Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	7D	B-BSA-10	20-22 ft	26	37	19	18	0.4	Lean CLAY (CL)

Sample Prepared using the WET method  
 0% Retained on #40 Sieve  
 Dry Strength: VERY HIGH  
 Dilatancy: SLOW  
 Toughness: LOW



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-106	Sample Type:	Jar
Sample ID:	8D	Test Date:	08/19/24
Depth :	25-27 ft	Test Id:	780373
Test Comment:	---		
Visual Description:	Moist, grayish brown clay		
Sample Comment:	---		

## Atterberg Limits - ASTM D4318



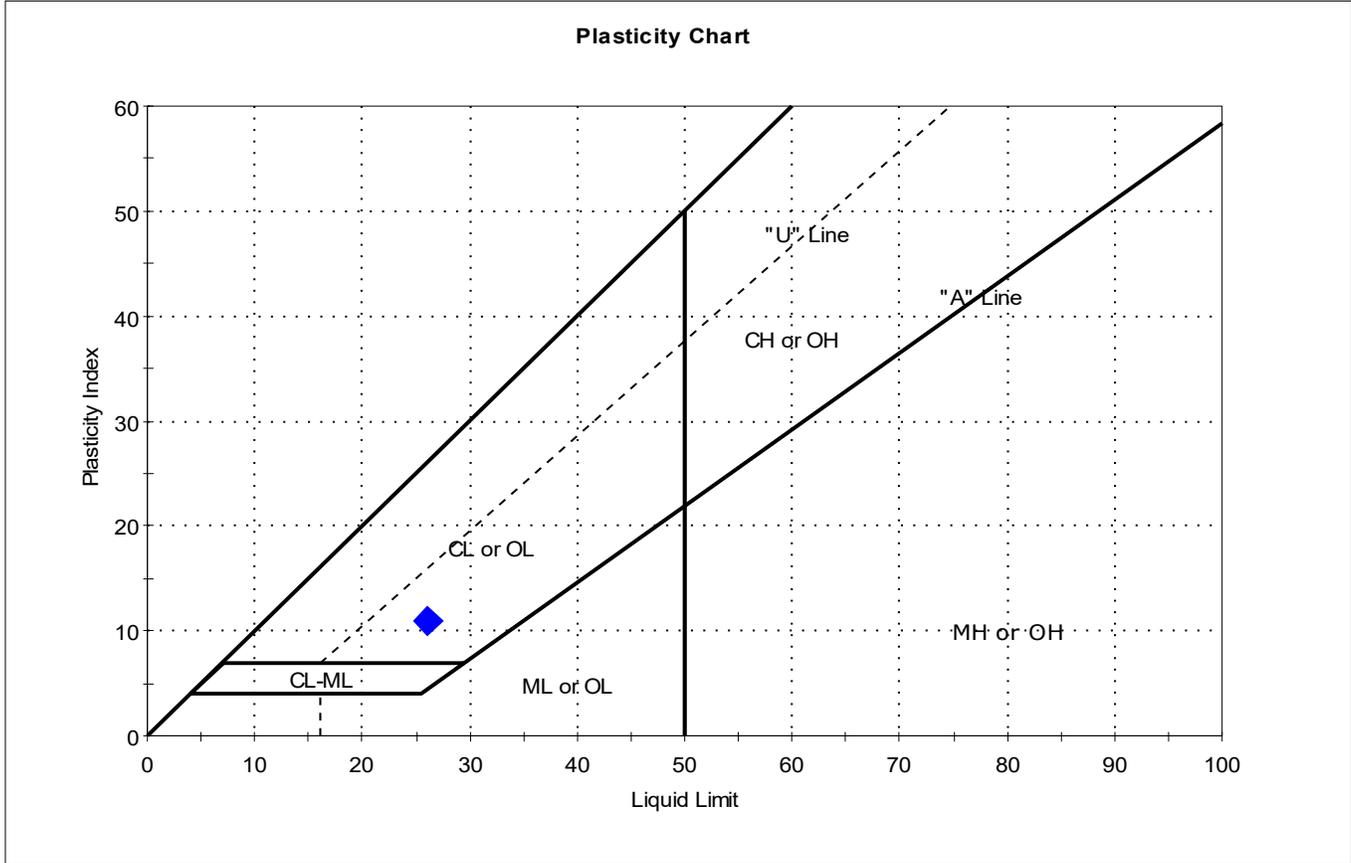
Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	8D	B-BSA-10	25-27 ft	28	36	19	17	0.5	Lean CLAY (CL)

Sample Prepared using the WET method  
 0% Retained on #40 Sieve  
 Dry Strength: VERY HIGH  
 Dilatancy: SLOW  
 Toughness: LOW



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-106	Sample Type:	Jar
Sample ID:	9D	Test Date:	08/16/24
Depth:	30-32 ft	Test Id:	780374
Test Comment:	---		
Visual Description:	Moist, gray clay		
Sample Comment:	---		

## Atterberg Limits - ASTM D4318



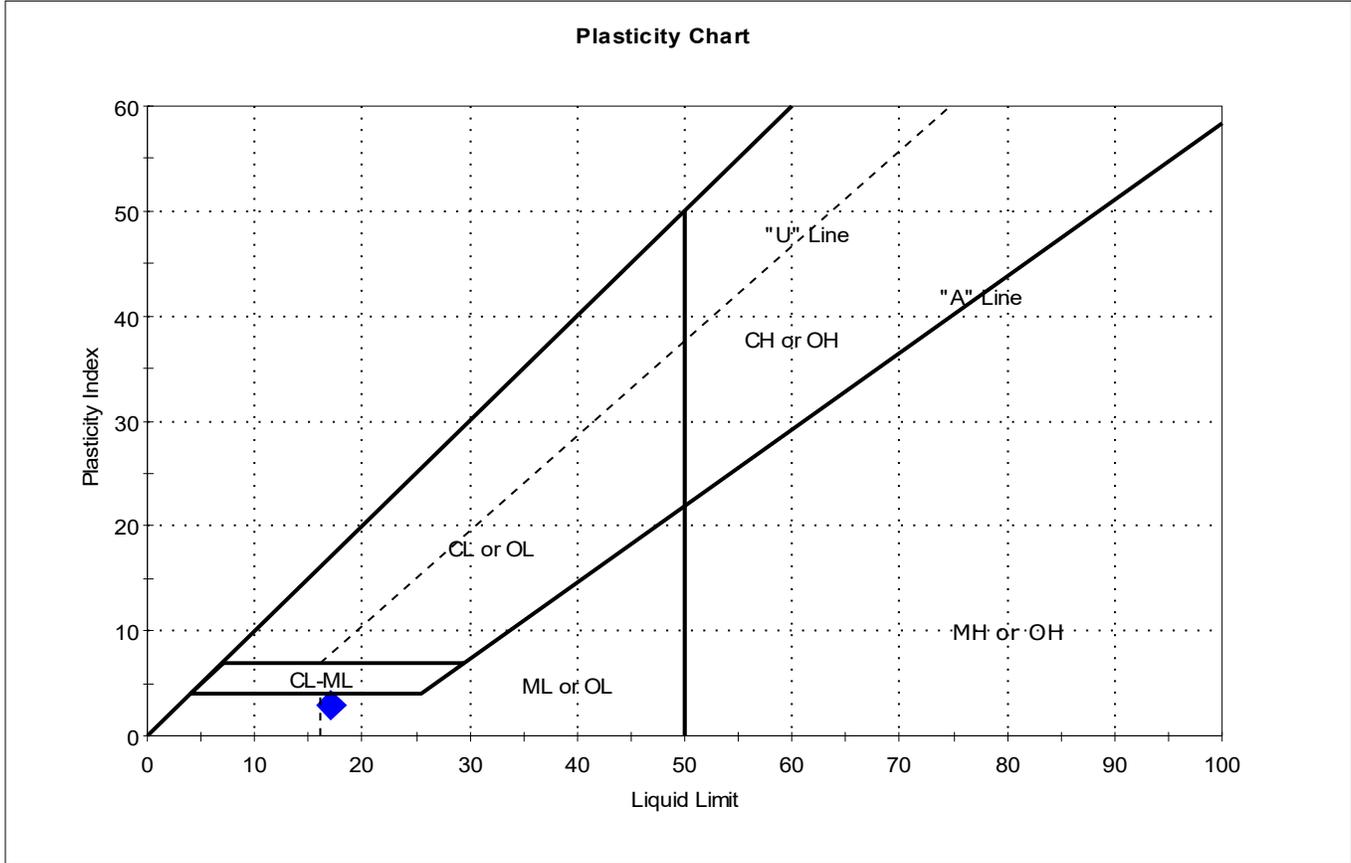
Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	9D	B-BSA-10	30-32 ft	29	26	15	11	1.3	Lean CLAY (CL)

Sample Prepared using the WET method  
 1% Retained on #40 Sieve  
 Dry Strength: VERY HIGH  
 Dilatancy: SLOW  
 Toughness: LOW



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-106	Sample Type:	Jar
Sample ID:	11D	Test Date:	08/16/24
Depth :	40-42 ft	Test Id:	780375
Test Comment:	---		
Visual Description:	Moist, gray sandy silt		
Sample Comment:	---		

## Atterberg Limits - ASTM D4318



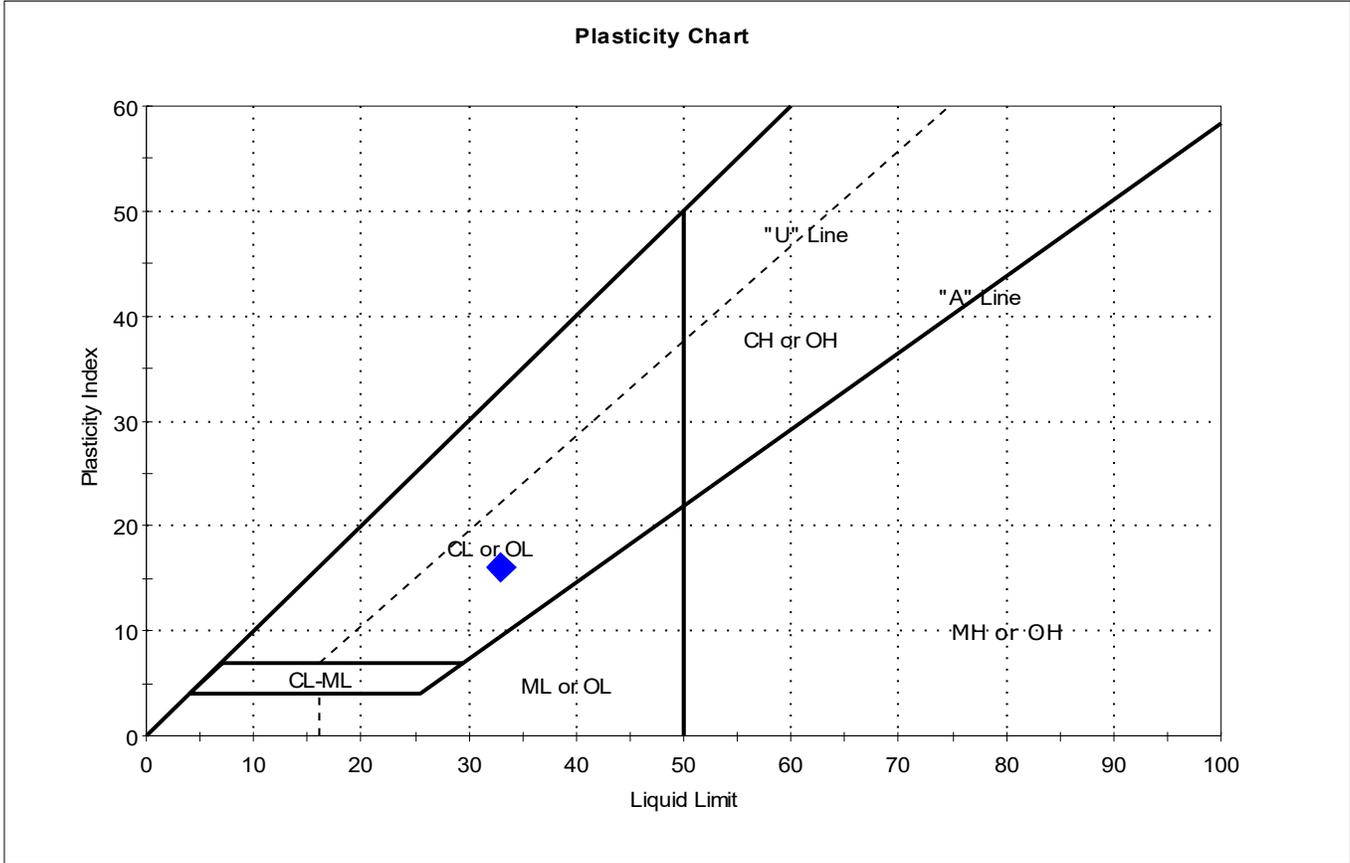
Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	11D	B-BSA-10	40-42 ft	11	17	14	3	-0.8	Sandy SILT (ML)

Sample Prepared using the WET method  
 23% Retained on #40 Sieve  
 Dry Strength: n/a  
 Dilatancy: n/a  
 Toughness: n/a



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-107	Sample Type:	Jar
Sample ID:	8D	Test Date:	08/19/24
Depth:	20-22 ft	Test Id:	780386
Test Comment:	---		
Visual Description:	Moist, grayish brown clay		
Sample Comment:	---		

## Atterberg Limits - ASTM D4318



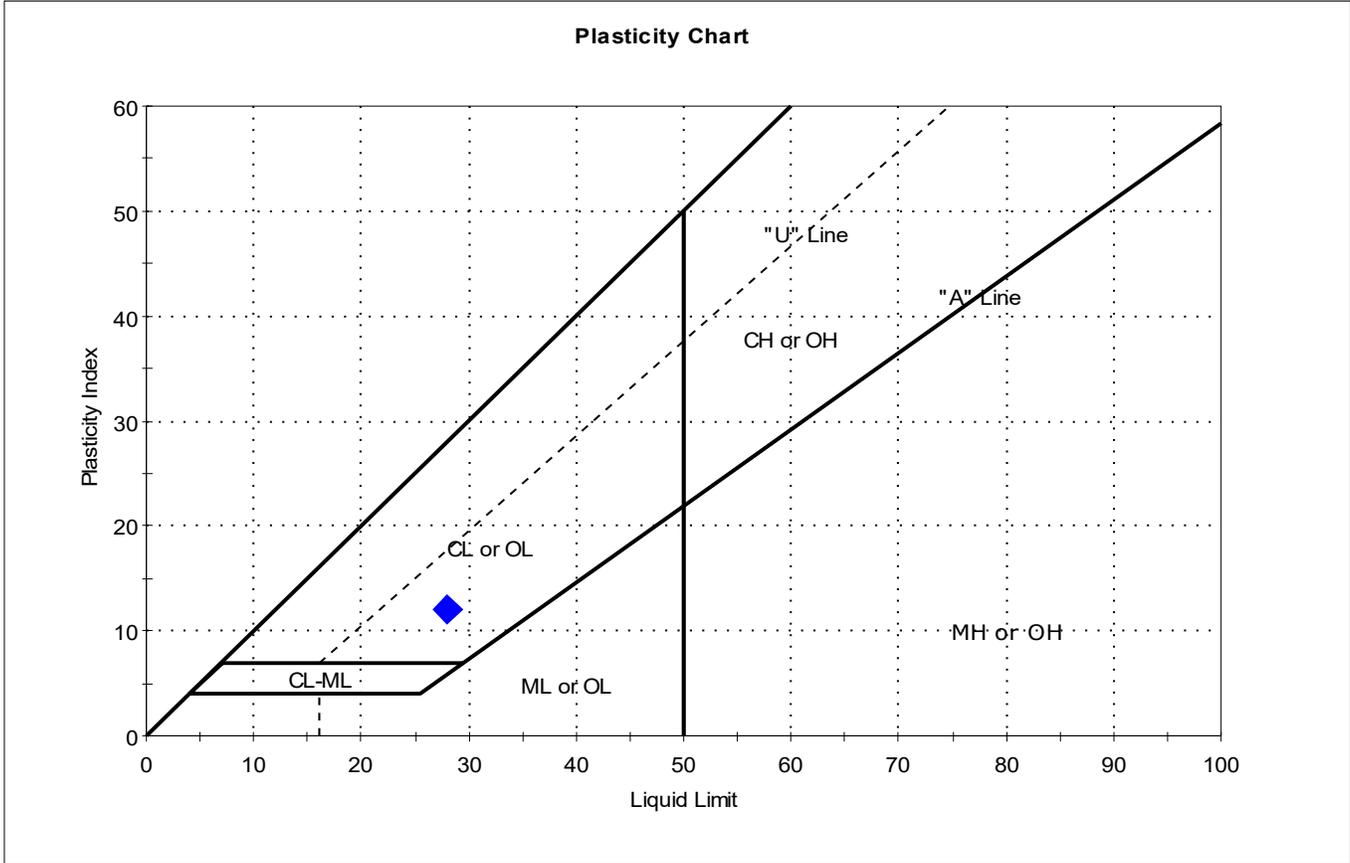
Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	8D	B-BSA-10	20-22 ft	24	33	17	16	0.4	Lean CLAY (CL)

Sample Prepared using the WET method  
 0% Retained on #40 Sieve  
 Dry Strength: VERY HIGH  
 Dilatancy: SLOW  
 Toughness: LOW



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-107	Sample Type:	Jar
Sample ID:	10D	Test Date:	08/19/24
Depth :	30-32 ft	Test Id:	780388
Test Comment:	---		
Visual Description:	Moist, grayish brown clay		
Sample Comment:	---		

## Atterberg Limits - ASTM D4318



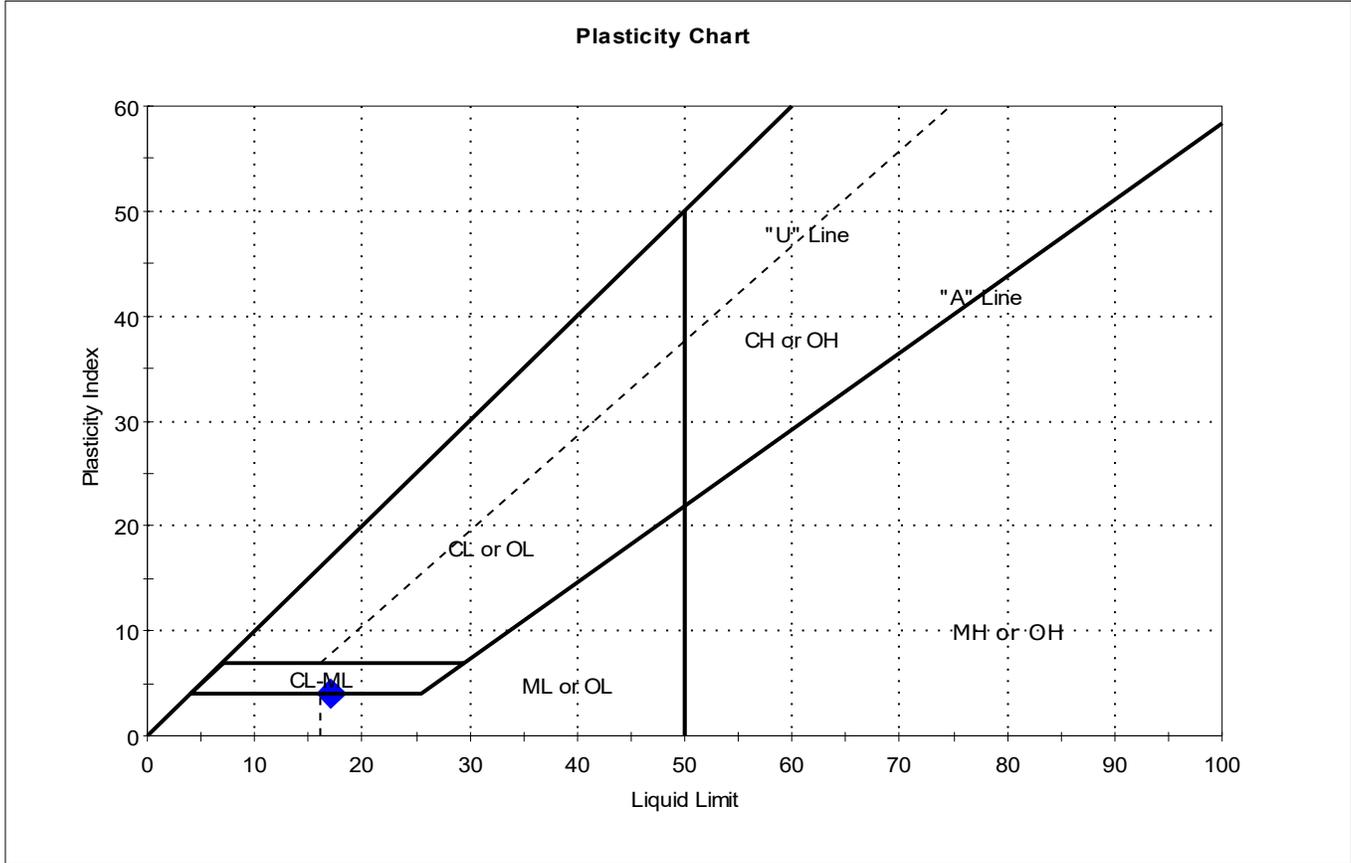
Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	10D	B-BSA-10	30-32 ft	28	28	16	12	1	Lean CLAY (CL)

Sample Prepared using the WET method  
 0% Retained on #40 Sieve  
 Dry Strength: VERY HIGH  
 Dilatancy: SLOW  
 Toughness: LOW



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-107	Sample Type:	Jar
Sample ID:	12D	Test Date:	08/16/24
Depth:	40-42 ft	Test Id:	780389
Test Comment:	---		
Visual Description:	Moist, brownish gray silty clayey sand with gravel		
Sample Comment:	---		

## Atterberg Limits - ASTM D4318



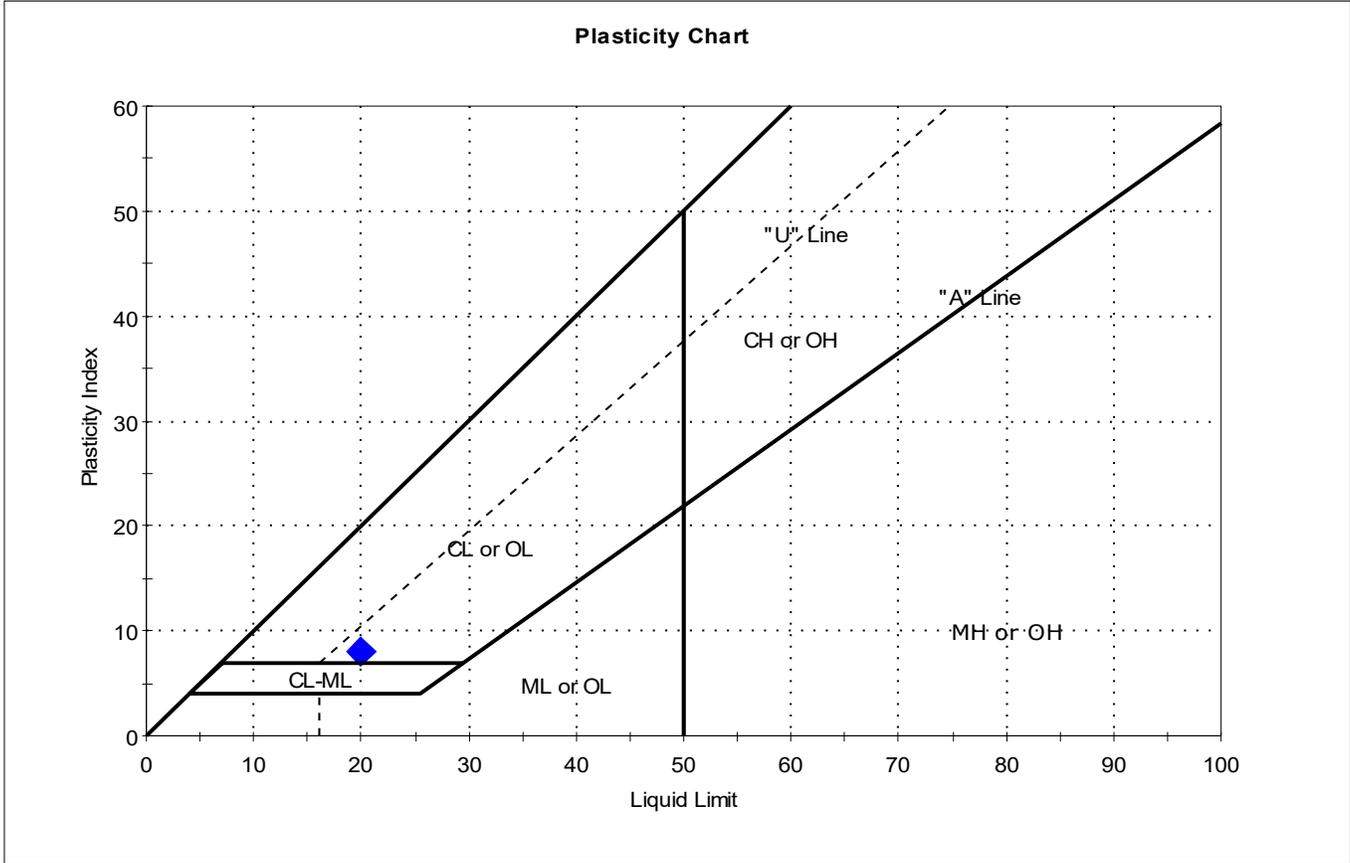
Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	12D	B-BSA-10	40-42 ft	10	17	13	4	-0.8	Silty, Clayey SAND with Gravel (SC-SM)

Sample Prepared using the WET method  
 40% Retained on #40 Sieve  
 Dry Strength: VERY HIGH  
 Dilatancy: SLOW  
 Toughness: LOW



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-107	Sample Type:	Jar
Sample ID:	14D	Test Date:	08/15/24
Depth :	50-52 ft	Test Id:	780390
Test Comment:	---		
Visual Description:	Moist, grayish brown clayey sand with gravel		
Sample Comment:	---		

## Atterberg Limits - ASTM D4318



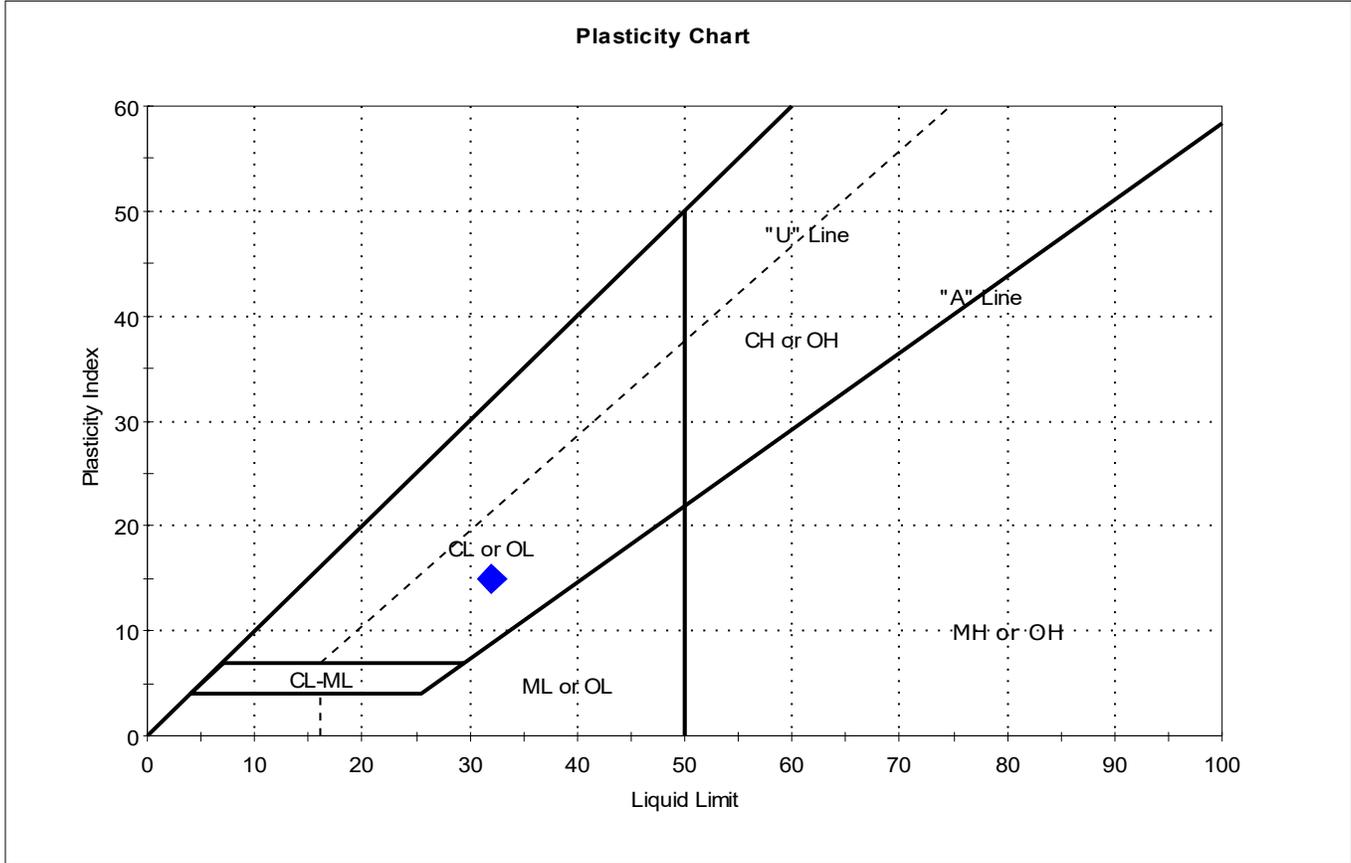
Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	14D	B-BSA-10	50-52 ft	10	20	12	8	-0.3	Clayey SAND with Gravel (SC)

Sample Prepared using the WET method  
 46% Retained on #40 Sieve  
 Dry Strength: VERY HIGH  
 Dilatancy: SLOW  
 Toughness: LOW



Client:	WSP USA, Inc.		Project No:	GTX-319180	
Project:	MaineDOT I-95 Bridge over Stillwater				
Location:	Merrimack, NH	Sample Type:	Jar	Tested By:	cam
Boring ID:	BB-BSA-111	Test Date:	08/16/24	Checked By:	ank
Sample ID:	5D	Test Id:	780417		
Depth :	10-12 ft				
Test Comment:	---				
Visual Description:	Moist, olive brown clay				
Sample Comment:	---				

## Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	5D	B-BSA-11	10-12 ft	21	32	17	15	0.3	Lean CLAY (CL)

Sample Prepared using the WET method  
 0% Retained on #40 Sieve  
 Dry Strength: VERY HIGH  
 Dilatancy: SLOW  
 Toughness: LOW



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	---	Sample Type:	---
Sample ID:	---	Test Date:	06/05/24
Depth :	---	Tested By:	ajl
		Checked By:	ank
		Test Id:	771711

## Moisture Content of Soil and Rock - ASTM D2216

Boring ID	Sample ID	Depth	Description	Moisture Content, %
BB-BSA-102	1D	1-3ft	Moist, brown silty sand with gravel	3.7
BB-BSA-102	2D	3-5ft	Moist, brown silty sand with gravel	8.6
BB-BSA-102	5D	9-11ft	Moist, light brown silty gravel with sand	15.5
BB-BSA-108	1D	0-2ft	Moist, yellowish brown silty sand with gravel	8.0
BB-BSA-109	2D	3-5ft	Moist, grayish brown silty gravel with sand	5.7
BB-BSA-109	4D	7-9ft	Moist, brown silty sand with gravel	11.7

Notes: Temperature of Drying : 110° Celsius



Client:	WSP USA, Inc.				
Project:	MaineDOT I-95 Bridge over Stillwater				
Location:	Merrimack, NH	Project No:	GTX-319180		
Boring ID:	---	Sample Type:	---	Tested By:	ajl
Sample ID:	---	Test Date:	06/07/24	Checked By:	ank
Depth :	---	Test Id:	771713		

## pH of Soil by ASTM D4972

Boring ID	Sample ID	Depth	Visual Description	pH of Soil in Distilled Water	pH of Soil in Calcium Chloride
BB-BSA-102	1D	1-3ft	Moist, brown silty sand with gravel	7.9	7.2
BB-BSA-109	2D	3-5ft	Moist, grayish brown silty gravel with sand	8.2	7.3

Notes: Sample Preparation: screened through #10 sieve  
Method A, pH meter used



Client:	WSP USA, Inc.
Project:	MaineDOT I-95 Bridge Over Stillwater
Location:	Merrimack, NH
GTX#:	319180
Test Date:	06/10/24
Due Date:	06/13/24
Tested By:	NMK
Checked By:	ank

**Laboratory Measurement of Soil Resistivity Using  
the Wenner Four-Electrode Method by ASTM G57  
(Laboratory Measurement)**

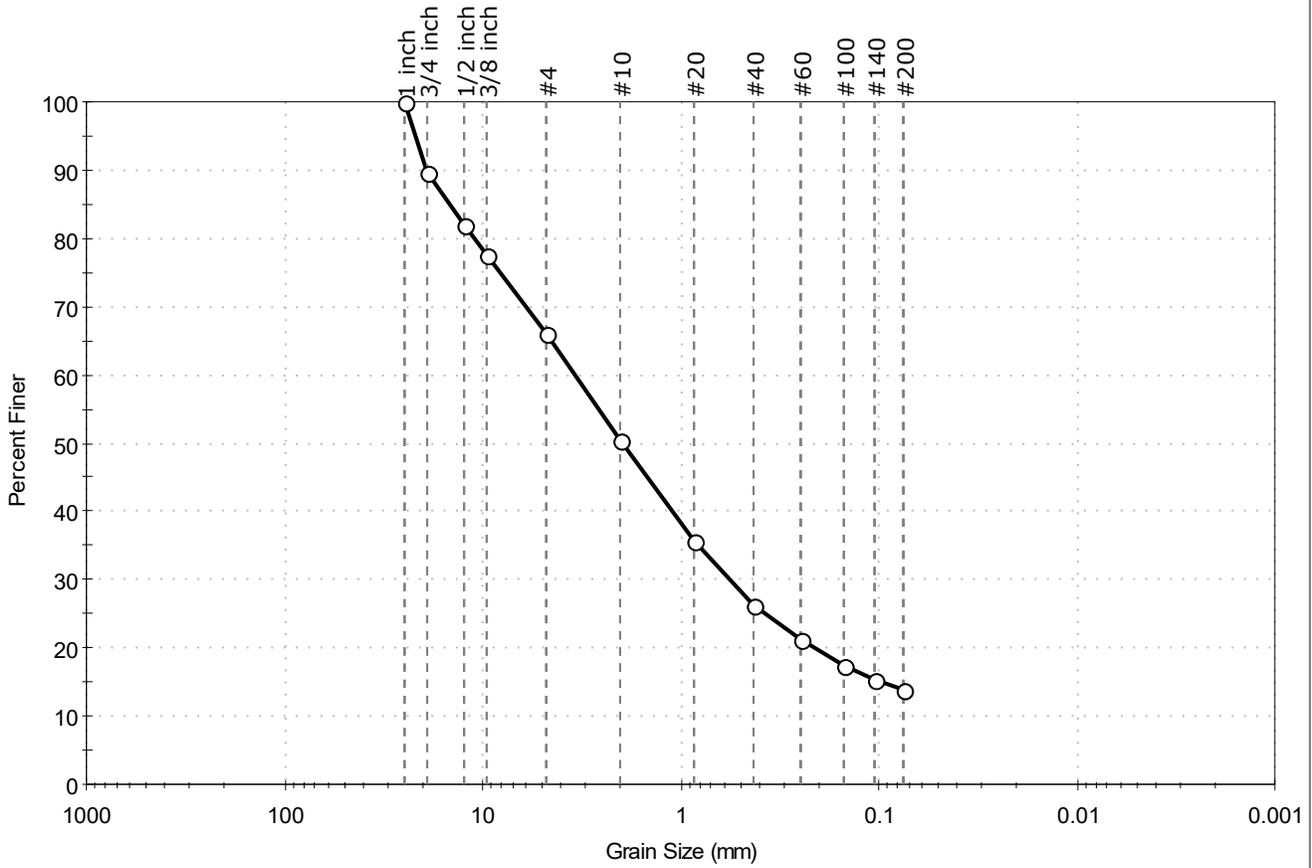
Boring ID	Sample ID	Depth, ft.	Sample Description	Electrical Resistivity, ohm-cm	Electrical Conductivity, (ohm-cm) <sup>-1</sup>
BB-BSA-102	1D	1-3 ft	Moist, brown silty gravel	1,202	8.32E-04

Notes: Test Equipment: Nilsson Model 400 Soil Resistance Meter, MC Miller Soil Box  
 Water added to sample to create a thick slurry prior to testing (saturated condition).  
 Electrical Conductivity is calculated as inverse of Electrical Resistivity (per ASTM G57)  
 Test conducted in standard laboratory atmosphere: 68-73 F



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-102	Sample Type: Jar
Sample ID: 1D	Test Date: 06/10/24
Depth: 1-3ft	Test Id: 771699
Test Comment: ---	Tested By: ajl
Visual Description: Moist, brown silty sand with gravel	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	34.0	52.0	14.0

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 inch	25.00	100		
3/4 inch	19.00	90		
1/2 inch	12.50	82		
3/8 inch	9.50	78		
#4	4.75	66		
#10	2.00	51		
#20	0.85	36		
#40	0.42	26		
#60	0.25	21		
#100	0.15	17		
#140	0.11	15		
#200	0.075	14		

<u>Coefficients</u>	
D <sub>85</sub> = 14.7631 mm	D <sub>30</sub> = 0.5584 mm
D <sub>60</sub> = 3.3977 mm	D <sub>15</sub> = 0.0975 mm
D <sub>50</sub> = 1.9370 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

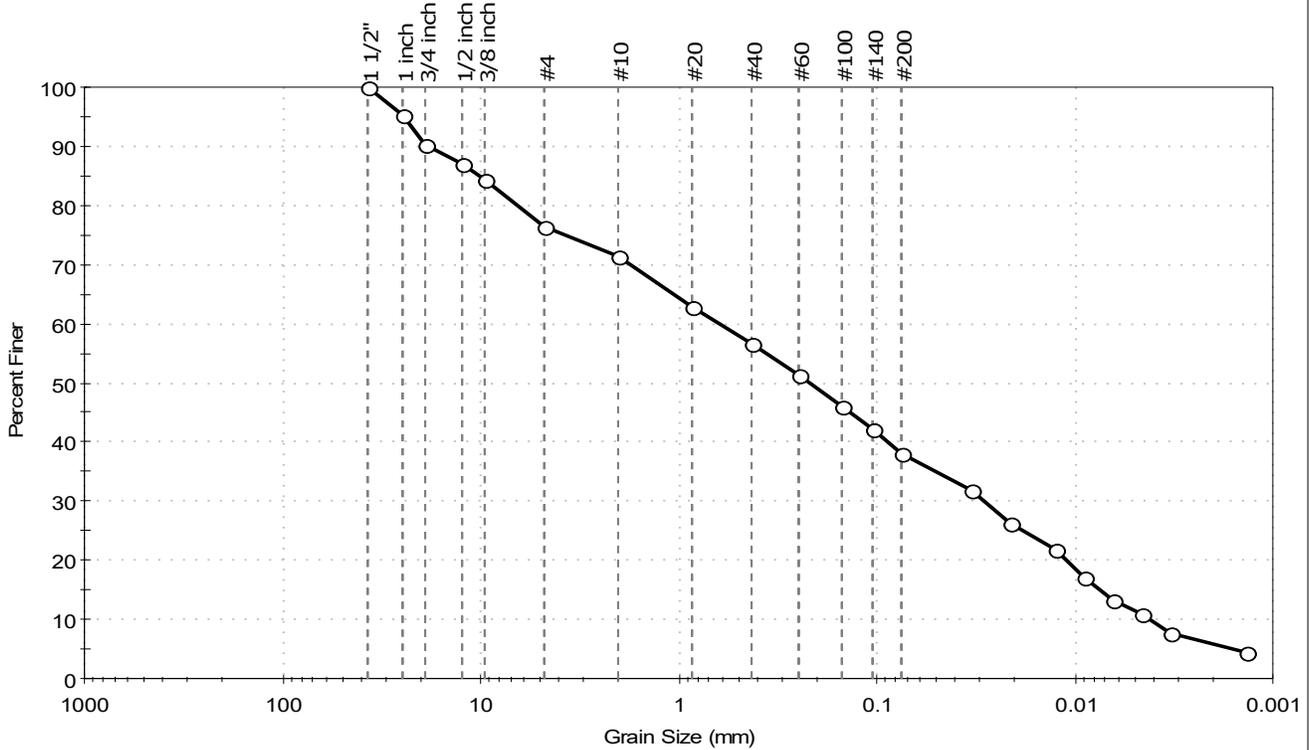
<u>Classification</u>	
ASTM	N/A
AASHTO	Stone Fragments, Gravel and Sand (A-1-b (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.  
 Project: MaineDOT I-95 Bridge over Stillwater  
 Location: Merrimack, NH  
 Project No: GTX-319180  
 Boring ID: BB-BSA-102  
 Sample Type: Jar  
 Tested By: ajl  
 Sample ID: 2D  
 Test Date: 06/11/24  
 Checked By: ank  
 Depth: 3-5ft  
 Test Id: 771725  
 Test Comment: ---  
 Visual Description: Moist, brown silty sand with gravel  
 Sample Comment: ---

## Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	23.6	38.4	38.0

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 1/2"	37.50	100		
1 inch	25.00	95		
3/4 inch	19.00	90		
1/2 inch	12.50	87		
3/8 inch	9.50	84		
#4	4.75	76		
#10	2.00	71		
#20	0.85	63		
#40	0.42	57		
#60	0.25	51		
#100	0.15	46		
#140	0.11	42		
#200	0.075	38		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0330	32		
---	0.0213	26		
---	0.0125	22		
---	0.0090	17		
---	0.0065	13		
---	0.0046	11		
---	0.0033	8		
---	0.0014	4		

Coefficients	
D <sub>85</sub> = 10.2078 mm	D <sub>30</sub> = 0.0286 mm
D <sub>60</sub> = 0.6168 mm	D <sub>15</sub> = 0.0074 mm
D <sub>50</sub> = 0.2201 mm	D <sub>10</sub> = 0.0042 mm
C <sub>u</sub> = 146.857	C <sub>c</sub> = 0.316

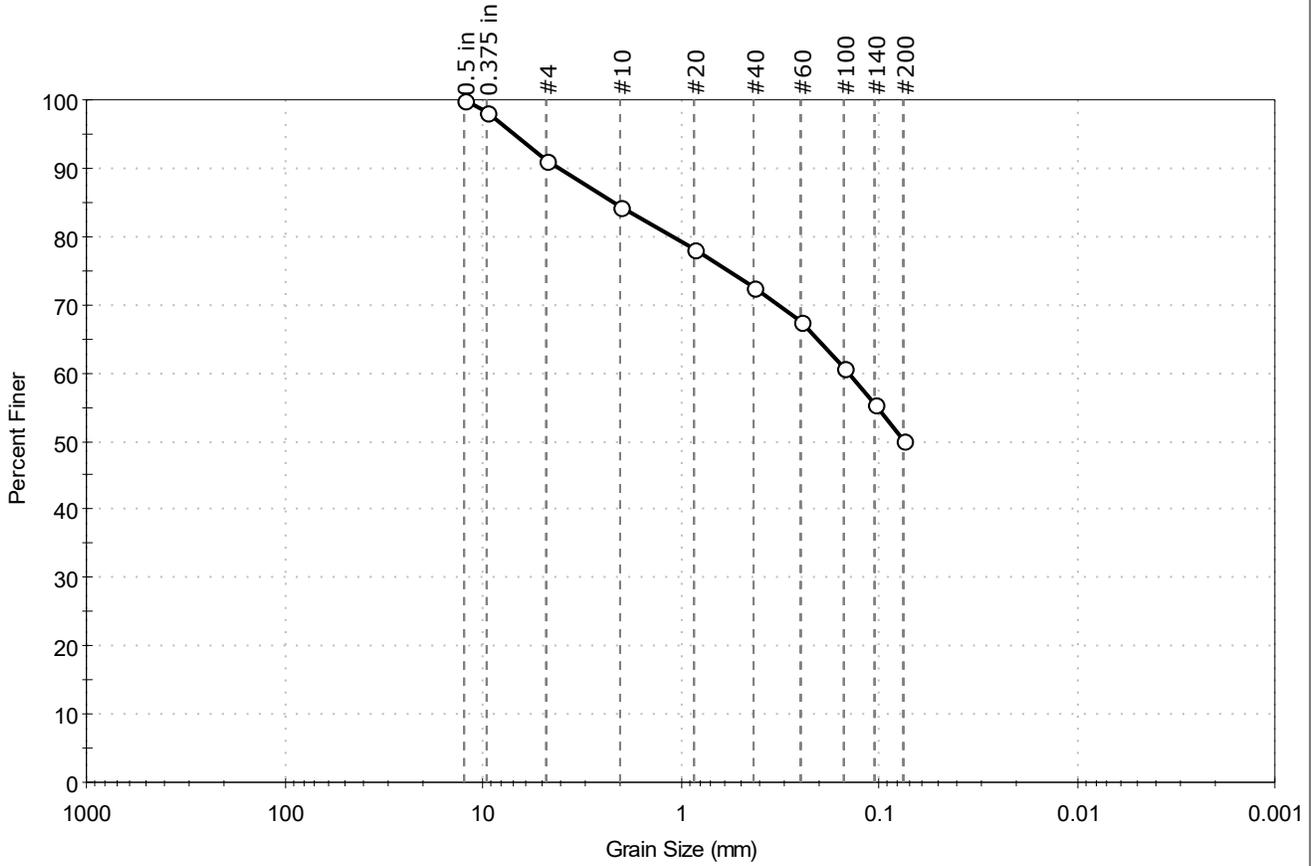
Classification	
ASTM	N/A
AASHTO	Silty Soils (A-4 (0))

Sample/Test Description
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD
Dispersion Device : Apparatus A - Mech Mixer
Dispersion Period : 1 minute
Est. Specific Gravity : 2.65
Separation of Sample: #200 Sieve



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-102	Sample Type:	Jar
Sample ID:	4D	Test Date:	06/11/24
Depth :	7-9ft	Test Id:	771701
Test Comment:	---		
Visual Description:	Moist, brown sandy silt		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	8.7	41.1	50.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.5 in	12.50	100		
0.375 in	9.50	98		
#4	4.75	91		
#10	2.00	84		
#20	0.85	78		
#40	0.42	73		
#60	0.25	67		
#100	0.15	61		
#140	0.11	55		
#200	0.075	50		

<u>Coefficients</u>	
D <sub>85</sub> = 2.1488 mm	D <sub>30</sub> = N/A
D <sub>60</sub> = 0.1431 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = N/A	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

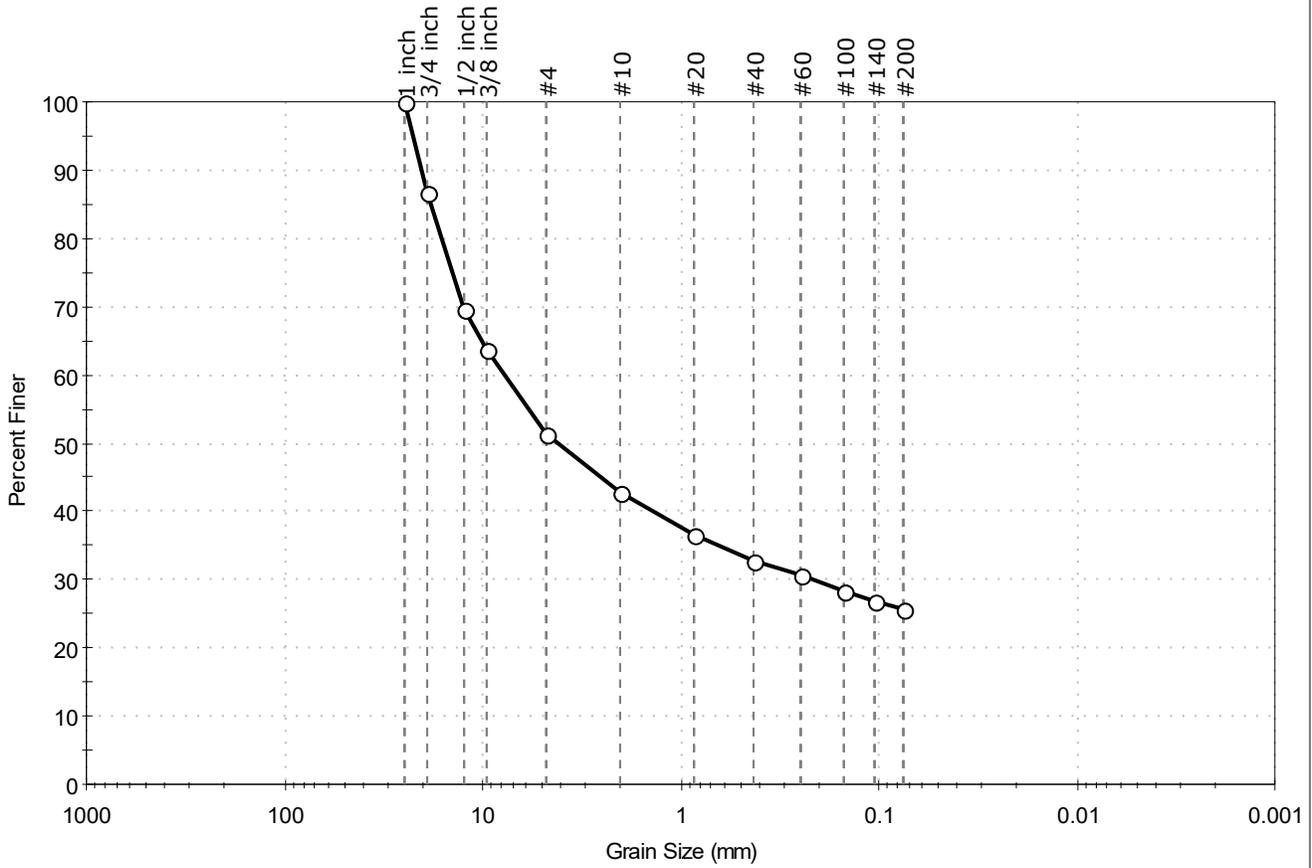
<u>Classification</u>	
<u>ASTM</u>	Sandy SILT (ML)
<u>AASHTO</u>	Silty Soils (A-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-102	Sample Type:	Jar
Sample ID:	5D	Test Date:	06/10/24
Depth :	9-11ft	Test Id:	771702
Test Comment:	---		
Visual Description:	Moist, light brown silty gravel with sand		
Sample Comment:	---		

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	48.7	25.7	25.6

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 inch	25.00	100		
3/4 inch	19.00	87		
1/2 inch	12.50	70		
3/8 inch	9.50	64		
#4	4.75	51		
#10	2.00	43		
#20	0.85	36		
#40	0.42	33		
#60	0.25	31		
#100	0.15	28		
#140	0.11	27		
#200	0.075	26		

<u>Coefficients</u>	
D <sub>85</sub> = 18.2066 mm	D <sub>30</sub> = 0.2200 mm
D <sub>60</sub> = 7.7553 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 4.1504 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

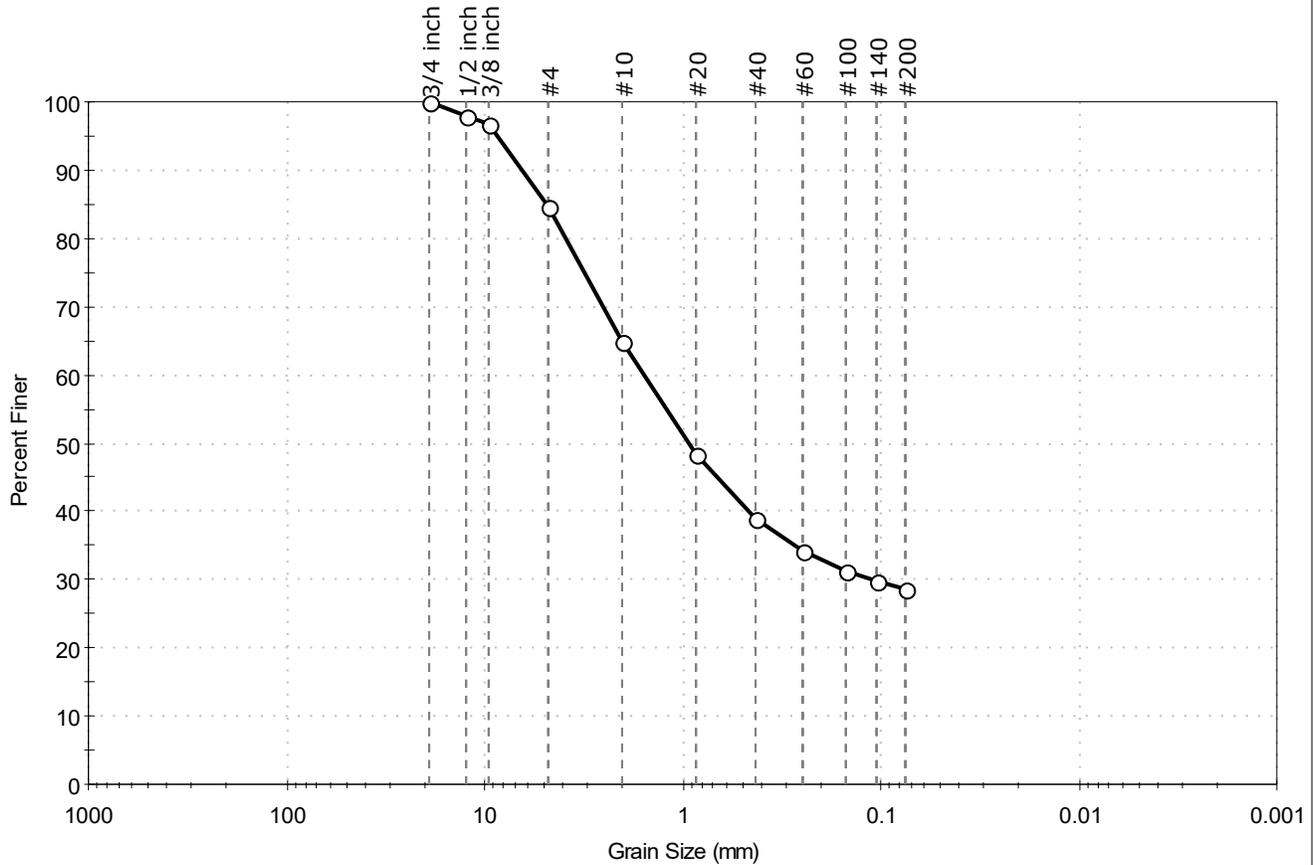
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Gravel and Sand (A-2-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.  
 Project: MaineDOT I-95 Bridge over Stillwater  
 Location: Merrimack, NH  
 Project No: GTX-319180  
 Boring ID: BB-BSA-108  
 Sample Type: Jar  
 Tested By: ajl  
 Sample ID: 1D  
 Test Date: 06/10/24  
 Checked By: ank  
 Depth: 0-2ft  
 Test Id: 771703  
 Test Comment: ---  
 Visual Description: Moist, yellowish brown silty sand with gravel  
 Sample Comment: ---

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	15.4	56.1	28.5

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
3/4 inch	19.00	100		
1/2 inch	12.50	98		
3/8 inch	9.50	97		
#4	4.75	85		
#10	2.00	65		
#20	0.85	48		
#40	0.42	39		
#60	0.25	34		
#100	0.15	31		
#140	0.11	30		
#200	0.075	28		

<u>Coefficients</u>	
D <sub>85</sub> = 4.8781 mm	D <sub>30</sub> = 0.1095 mm
D <sub>60</sub> = 1.5572 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 0.9286 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

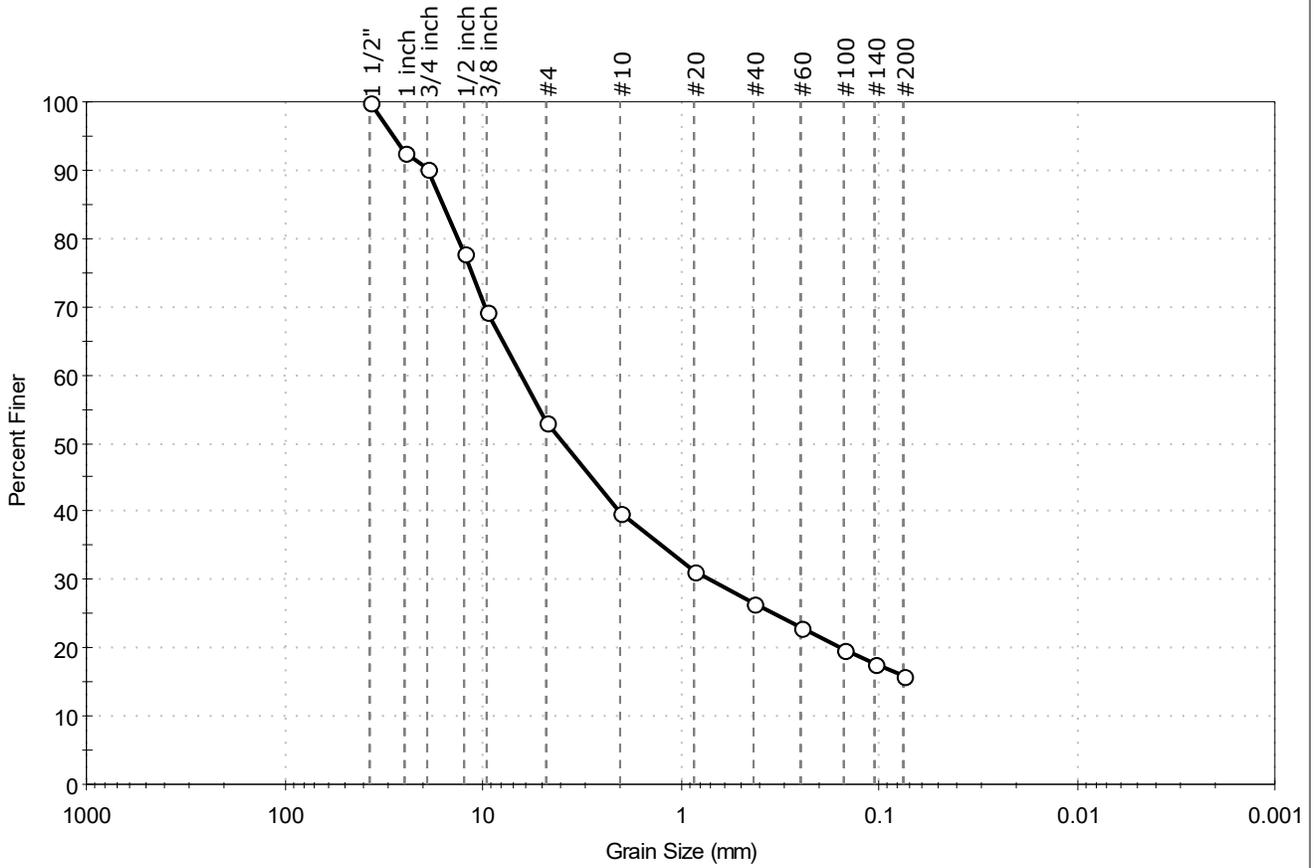
<u>Classification</u>	
ASTM	N/A
AASHTO	Silty Gravel and Sand (A-2-4 (0))

<u>Sample/Test Description</u>
Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.  
 Project: MaineDOT I-95 Bridge over Stillwater  
 Location: Merrimack, NH  
 Project No: GTX-319180  
 Boring ID: BB-BSA-109  
 Sample Type: Jar  
 Tested By: ajl  
 Sample ID: 2D  
 Test Date: 06/11/24  
 Checked By: ank  
 Depth: 3-5ft  
 Test Id: 771704  
 Test Comment: ---  
 Visual Description: Moist, grayish brown silty gravel with sand  
 Sample Comment: ---

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	46.8	37.3	15.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 1/2"	37.50	100		
1 inch	25.00	93		
3/4 inch	19.00	90		
1/2 inch	12.50	78		
3/8 inch	9.50	69		
#4	4.75	53		
#10	2.00	40		
#20	0.85	31		
#40	0.42	26		
#60	0.25	23		
#100	0.15	20		
#140	0.11	18		
#200	0.075	16		

<b>Coefficients</b>	
D <sub>85</sub> = 15.9069 mm	D <sub>30</sub> = 0.7017 mm
D <sub>60</sub> = 6.3678 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 3.8773 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

<b>Classification</b>	
ASTM	N/A
AASHTO	Stone Fragments, Gravel and Sand (A-1-b (0))

**Sample/Test Description**

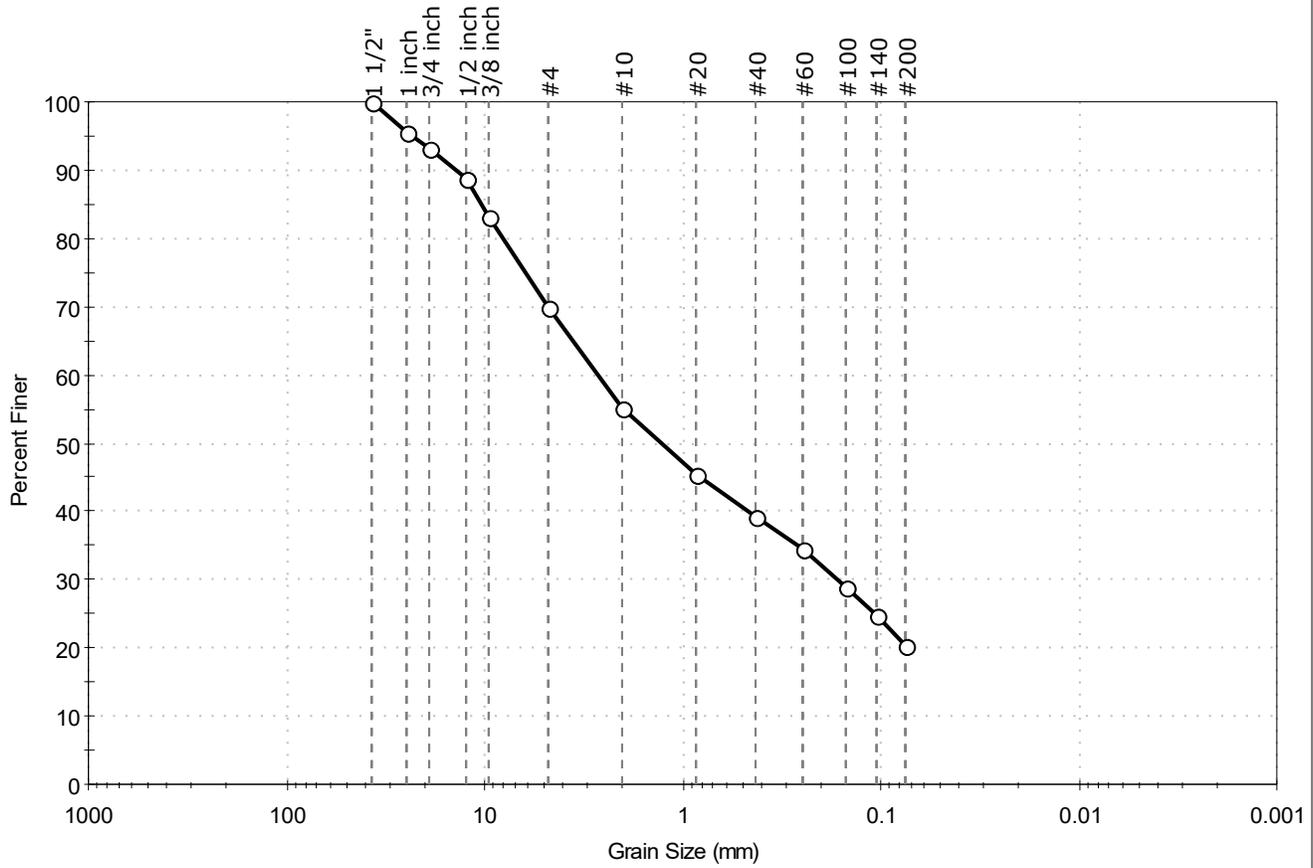
Sand/Gravel Particle Shape : ANGULAR

Sand/Gravel Hardness : HARD



Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-109	Sample Type: Jar
Sample ID: 4D	Test Date: 06/10/24
Depth: 7-9ft	Test Id: 771705
Test Comment: ---	Tested By: ajl
Visual Description: Moist, brown silty sand with gravel	Checked By: ank
Sample Comment: ---	

## Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	30.1	49.6	20.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 1/2"	37.50	100		
1 inch	25.00	96		
3/4 inch	19.00	93		
1/2 inch	12.50	89		
3/8 inch	9.50	83		
#4	4.75	70		
#10	2.00	55		
#20	0.85	45		
#40	0.42	39		
#60	0.25	35		
#100	0.15	29		
#140	0.11	25		
#200	0.075	20		

<u>Coefficients</u>	
D <sub>85</sub> = 10.4311 mm	D <sub>30</sub> = 0.1670 mm
D <sub>60</sub> = 2.6443 mm	D <sub>15</sub> = N/A
D <sub>50</sub> = 1.2721 mm	D <sub>10</sub> = N/A
C <sub>u</sub> = N/A	C <sub>c</sub> = N/A

<u>Classification</u>	
ASTM	N/A
AASHTO	Stone Fragments, Gravel and Sand (A-1-b (0))

<u>Sample/Test Description</u>	
Sand/Gravel Particle Shape : ANGULAR	
Sand/Gravel Hardness : HARD	



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-102	Sample Type:	Jar
Sample ID:	4D	Test Date:	06/10/24
Depth :	7-9ft	Checked By:	ank
		Test Id:	771698
Test Comment:	---		
Visual Description:	Moist, brown sandy silt		
Sample Comment:	---		

## Atterberg Limits - ASTM D4318

Sample Determined to be non-plastic

Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	4D	B-BSA-10	7-9ft	13	n/a	n/a	n/a	n/a	Sandy SILT (ML)

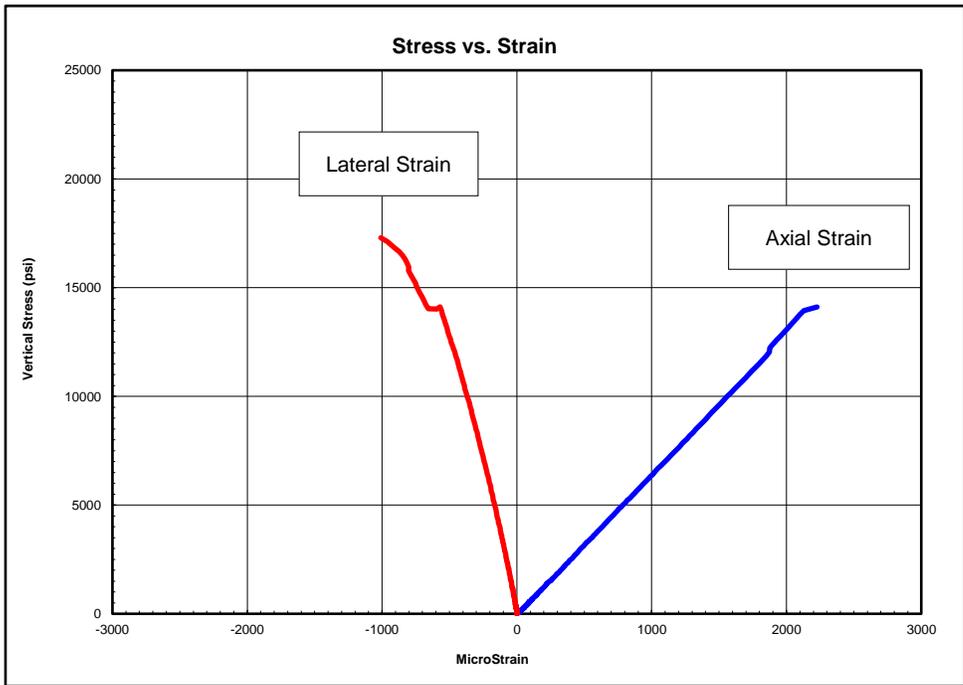
27% Retained on #40 Sieve  
 Dry Strength: n/a  
 Dilatancy: n/a  
 Toughness: n/a  
 The sample was determined to be Non-Plastic





Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	6/13/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-102
Sample ID:	R1
Depth, ft:	14.87-15.25
Sample Type:	rock core
Sample Description:	See photographs Intact material failure Best Effort end preparation performed

## Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 17,296 psi

The axial strain gauges failed before the peak value was attained. Young's Modulus and Poisson's Ratio could not be determined within the third stress range for this test.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
1700-6300	6,470,000	0.23
6300-11000	6,460,000	0.27
11000-15600	---	---

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature. The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes. Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed. Calculations assume samples are isotropic, which is not necessarily the case.



Client:	WSP USA, Inc.	Test Date:	6/12/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-102		
Sample ID:	R1		
Depth (ft):	14.87-15.25		
Visual Description:	See photographs		

**UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543**

<b>BULK DENSITY</b>				<b>DEVIATION FROM STRAIGHTNESS (Procedure S1)</b>			
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap $\leq$ 0.02 in.? <b>YES</b>			
Specimen Length, in:	4.38	4.38	4.38	Maximum difference must be < 0.020 in. <b>Straightness Tolerance Met? YES</b>			
Specimen Diameter, in:	1.97	1.97	1.97				
Specimen Mass, g:	593.5						
Bulk Density, lb/ft <sup>3</sup> :	169						
Length to Diameter Ratio:	2.2						
		<b>Minimum Diameter Tolerance Met?</b>	<b>YES</b>				
		<b>Length to Diameter Ratio Tolerance Met?</b>	<b>YES</b>				

<b>END FLATNESS AND PARALLELISM (Procedure FP1)</b>															
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00100	-0.00090	-0.00070	-0.00050	-0.00030	-0.00020	-0.00010	0.00000	0.00020	0.00030	0.00040	0.00040	0.00050	0.00050	0.00060
Diameter 2, in (rotated 90°)	0.00090	0.00080	0.00050	0.00040	0.00030	0.00020	0.00010	0.00000	0.00000	-0.00020	-0.00040	-0.00060	-0.00070	-0.00090	-0.00120
	Difference between max and min readings, in: 0° = 0.00160      90° = 0.00210														
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00090	-0.00080	-0.00050	-0.00030	-0.00030	-0.00020	0.00000	0.00000	0.00000	0.00010	0.00030	0.00040	0.00050	0.00060	0.00060
Diameter 2, in (rotated 90°)	-0.00100	-0.00090	-0.00070	-0.00040	-0.00030	-0.00020	0.00000	0.00000	0.00020	0.00030	0.00050	0.00060	0.00070	0.00070	0.00090
	Difference between max and min readings, in: 0° = 0.0015      90° = 0.0019 Maximum difference must be < 0.0020 in.      Difference = ± 0.00105 <b>Flatness Tolerance Met? NO</b>														

	<p><b>DIAMETER 1</b></p> <p>End 1: Slope of Best Fit Line: 0.00093 Angle of Best Fit Line: 0.05337</p> <p>End 2: Slope of Best Fit Line: 0.00083 Angle of Best Fit Line: 0.04764</p> <p>Maximum Angular Difference: 0.00573</p> <p><b>Parallelism Tolerance Met? NO</b> Spherically Seated</p> <hr/> <p><b>DIAMETER 2</b></p> <p>End 1: Slope of Best Fit Line: 0.00108 Angle of Best Fit Line: 0.06204</p> <p>End 2: Slope of Best Fit Line: 0.00107 Angle of Best Fit Line: 0.06139</p> <p>Maximum Angular Difference: 0.00065</p> <p><b>Parallelism Tolerance Met? YES</b> Spherically Seated</p>
--	--

<b>PERPENDICULARITY (Procedure P1)</b> (Calculated from End Flatness and Parallelism measurements above)					
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?
Diameter 1, in	0.00160	1.970	0.00081	0.047	YES
Diameter 2, in (rotated 90°)	0.00210	1.970	0.00107	0.061	YES
	Maximum angle of departure must be $\leq$ 0.25° <b>Perpendicularity Tolerance Met? YES</b>				
END 2					
Diameter 1, in	0.00150	1.970	0.00076	0.044	YES
Diameter 2, in (rotated 90°)	0.00190	1.970	0.00096	0.055	YES

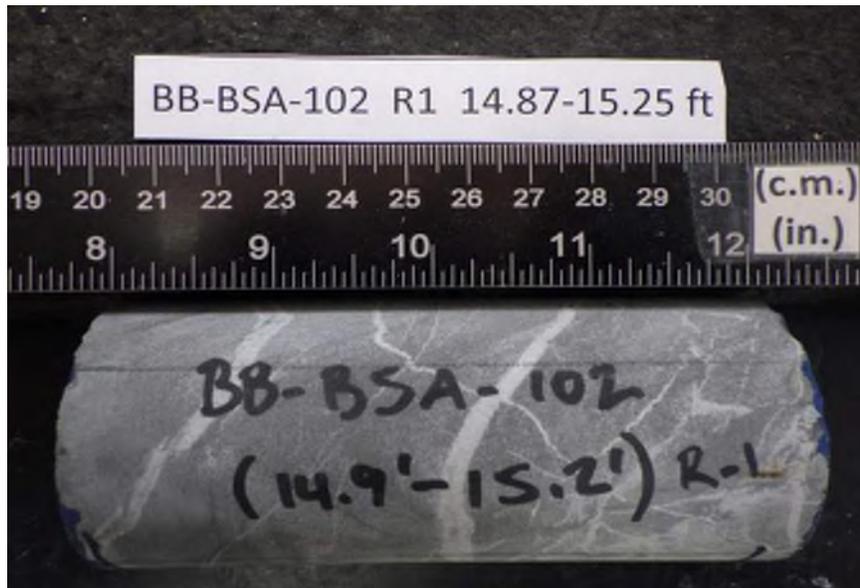


Client:	WSP USA, Inc.	Test Date:	6/12/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-102	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R1		
Depth (ft):	14.87-15.25		
Visual Description:	See photographs		

**BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO ASTM D4543**

<b>END FLATNESS</b>			
END 1			
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
END 2			
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
<b>End Flatness Tolerance Met? YES</b>			

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	6/13/2024
Tested By:	smd
Checked By:	jsc
Boring ID:	BB-BSA-102
Sample ID:	R1
Depth, ft:	14.87-15.25



After cutting and grinding

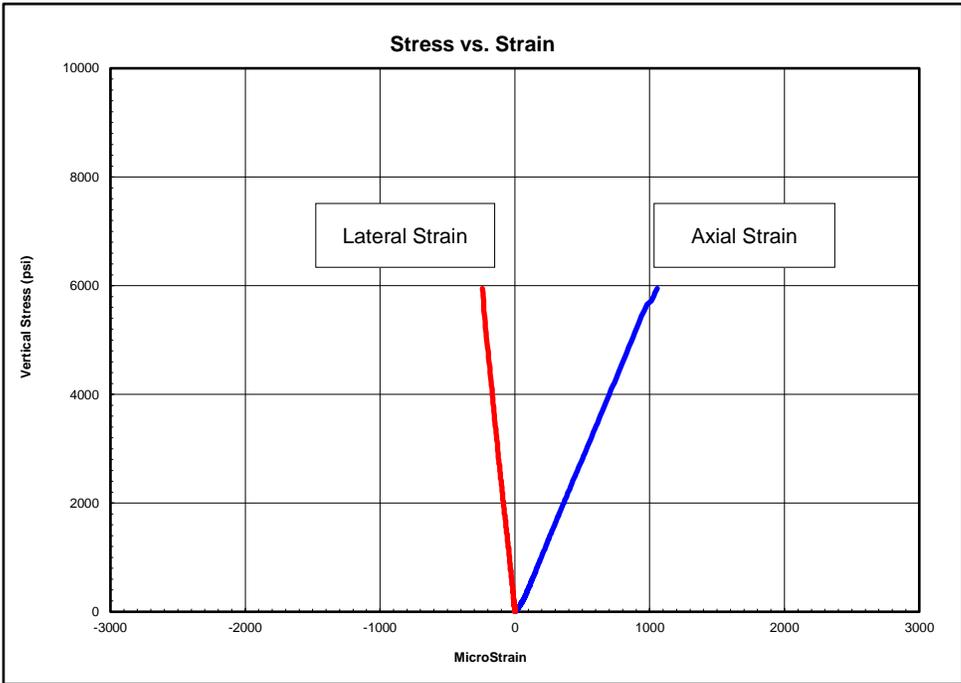


After break



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	6/13/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-110
Sample ID:	R1
Depth, ft:	5.93-6.31
Sample Type:	rock core
Sample Description:	See photographs Intact material and discontinuity failure Best Effort end preparation performed

## Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 5,948 psi

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
600-2200	6,020,000	0.26
2200-3800	5,880,000	0.25
3800-5400	6,000,000	0.25

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature. The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes. Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed. Calculations assume samples are isotropic, which is not necessarily the case.



Client:	WSP USA, Inc.	Test Date:	6/12/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-110		
Sample ID:	R1		
Depth (ft):	5.93-6.31		
Visual Description:	See photographs		

**UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543**

<b>BULK DENSITY</b>				<b>DEVIATION FROM STRAIGHTNESS (Procedure S1)</b>			
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap $\leq$ 0.02 in.? <b>YES</b>			
Specimen Length, in:	4.41	4.41	4.41	Maximum difference must be $<$ 0.020 in. <b>Straightness Tolerance Met? YES</b>			
Specimen Diameter, in:	1.97	1.97	1.97				
Specimen Mass, g:	604.37						
Bulk Density, lb/ft <sup>3</sup> :	171						
Length to Diameter Ratio:	2.2						
		<b>Minimum Diameter Tolerance Met?</b>	<b>YES</b>				
		<b>Length to Diameter Ratio Tolerance Met?</b>	<b>YES</b>				

<b>END FLATNESS AND PARALLELISM (Procedure FP1)</b>															
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00240	-0.00210	-0.00210	-0.00190	-0.00130	0.00000	0.00000	0.00000	0.00000	-0.00010	-0.00020	-0.00030	-0.00040	-0.00050	-0.00050
Diameter 2, in (rotated 90°)	-0.00120	-0.00110	-0.00100	-0.00090	-0.00060	-0.00030	-0.00010	0.00000	0.00020	0.00040	0.00060	0.00070	0.00080	0.00100	0.00110
	Difference between max and min readings, in: 0° = 0.00240      90° = 0.00230														
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Diameter 2, in (rotated 90°)	0.00110	0.00100	0.00080	0.00060	0.00050	0.00030	0.00010	0.00000	0.00000	-0.00020	-0.00040	-0.00070	-0.00090	-0.00100	-0.00140
	Difference between max and min readings, in: 0° = 0.0001      90° = 0.0025 Maximum difference must be $<$ 0.0020 in.      Difference = $\pm$ 0.00125 <b>Flatness Tolerance Met? NO</b>														

	<p><b>DIAMETER 1</b></p> <p>End 1: Slope of Best Fit Line: 0.00117 Angle of Best Fit Line: 0.06695</p> <p>End 2: Slope of Best Fit Line: 0.00008 Angle of Best Fit Line: 0.00442</p> <p>Maximum Angular Difference: 0.06253</p> <p><b>Parallelism Tolerance Met? NO</b> Spherically Seated</p> <hr/> <p><b>DIAMETER 2</b></p> <p>End 1: Slope of Best Fit Line: 0.00141 Angle of Best Fit Line: 0.08087</p> <p>End 2: Slope of Best Fit Line: 0.00134 Angle of Best Fit Line: 0.07694</p> <p>Maximum Angular Difference: 0.00393</p> <p><b>Parallelism Tolerance Met? YES</b> Spherically Seated</p>
--	--

<b>PERPENDICULARITY (Procedure P1)</b> (Calculated from End Flatness and Parallelism measurements above)					
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?
Diameter 1, in	0.00240	1.970	0.00122	0.070	YES
Diameter 2, in (rotated 90°)	0.00230	1.970	0.00117	0.067	YES
	Maximum angle of departure must be $\leq$ 0.25° <b>Perpendicularity Tolerance Met? YES</b>				
END 2					
Diameter 1, in	0.00010	1.970	0.00005	0.003	YES
Diameter 2, in (rotated 90°)	0.00250	1.970	0.00127	0.073	YES

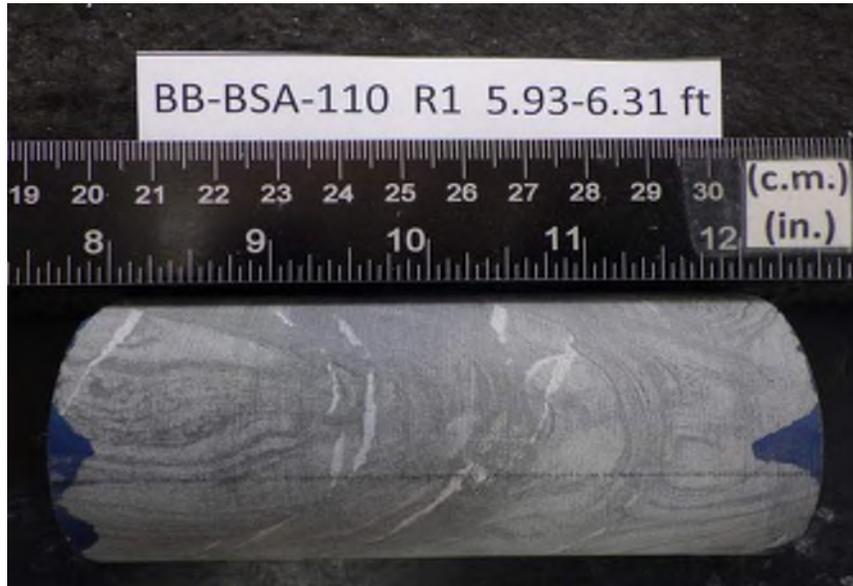


Client:	WSP USA, Inc.	Test Date:	6/12/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-110	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R1		
Depth (ft):	5.93-6.31		
Visual Description:	See photographs		

**BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO ASTM D4543**

<b>END FLATNESS</b>			
END 1			
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
END 2			
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
<b>End Flatness Tolerance Met? YES</b>			

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	6/13/2024
Tested By:	gp
Checked By:	smd
Boring ID:	BB-BSA-110
Sample ID:	R1
Depth, ft:	5.93-6.31



After cutting and grinding

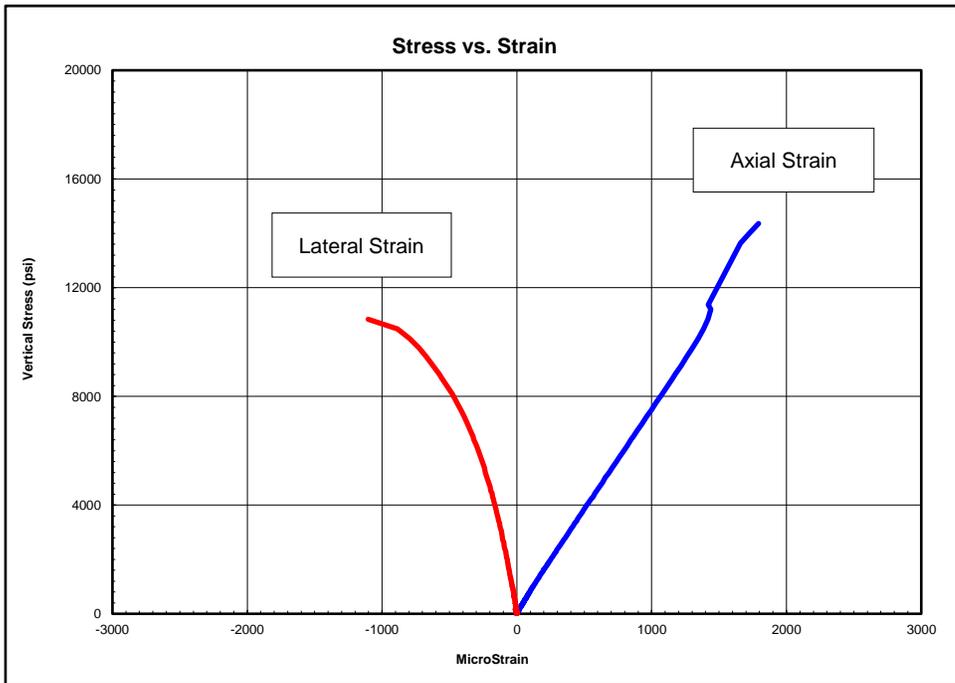


After break



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-101
Sample ID:	R-4
Depth, ft:	37-37.3
Sample Type:	rock core
Sample Description:	See photographs Intact material failure Best Effort end preparation performed

## Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 14,361 psi

The lateral strain gauges failed before the peak value was attained. Poisson's Ratio could not be determined within the second and third stress ranges.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
1400-5300	7,410,000	0.34
5300-9100	7,340,000	---
9100-12900	11,000,000	---

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature. The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes. Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed. Calculations assume samples are isotropic, which is not necessarily the case.



Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-101		
Sample ID:	R-4		
Depth (ft):	37-37.3		
Visual Description:	See photographs		

**UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543**

<b>BULK DENSITY</b>				<b>DEVIATION FROM STRAIGHTNESS (Procedure S1)</b>			
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap $\leq$ 0.02 in.? <b>YES</b>			
Specimen Length, in:	4.33	4.33	4.33	Maximum difference must be $<$ 0.020 in. <b>Straightness Tolerance Met? YES</b>			
Specimen Diameter, in:	1.97	1.97	1.97				
Specimen Mass, g:	589.14						
Bulk Density, lb/ft <sup>3</sup> :	170						
Length to Diameter Ratio:	2.2						
		<b>Minimum Diameter Tolerance Met?</b>	<b>YES</b>				
		<b>Length to Diameter Ratio Tolerance Met?</b>	<b>YES</b>				

<b>END FLATNESS AND PARALLELISM (Procedure FP1)</b>															
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	0.00120	0.00100	0.00080	0.00070	0.00050	0.00040	0.00000	0.00000	0.00000	-0.00010	-0.00030	-0.00060	-0.00080	-0.00090	-0.00120
Diameter 2, in (rotated 90°)	0.00100	0.00080	0.00070	0.00070	0.00050	0.00030	0.00010	0.00000	0.00000	-0.00010	-0.00040	-0.00050	-0.00070	-0.00070	-0.00130
	Difference between max and min readings, in: 0° = 0.00240      90° = 0.00230														
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	0.00110	0.00100	0.00070	0.00060	0.00040	0.00030	0.00020	0.00000	-0.00010	-0.00040	-0.00060	-0.00070	-0.00110	-0.00130	-0.00140
Diameter 2, in (rotated 90°)	-0.00130	-0.00110	-0.00090	-0.00070	-0.00030	-0.00020	-0.00010	0.00000	0.00000	0.00020	0.00040	0.00050	0.00070	0.00080	0.00120
	Difference between max and min readings, in: 0° = 0.0025      90° = 0.0025 Maximum difference must be $<$ 0.0020 in.      Difference = $\pm$ 0.00125 <b>Flatness Tolerance Met? NO</b>														

	<p><b>DIAMETER 1</b></p> <p>End 1: Slope of Best Fit Line: 0.00128 Angle of Best Fit Line: 0.07334</p> <p>End 2: Slope of Best Fit Line: 0.00143 Angle of Best Fit Line: 0.08218</p> <p>Maximum Angular Difference: 0.00884</p> <p><b>Parallelism Tolerance Met? NO</b> Spherically Seated</p> <hr/> <p><b>DIAMETER 2</b></p> <p>End 1: Slope of Best Fit Line: 0.00116 Angle of Best Fit Line: 0.06630</p> <p>End 2: Slope of Best Fit Line: 0.00128 Angle of Best Fit Line: 0.07317</p> <p>Maximum Angular Difference: 0.00688</p> <p><b>Parallelism Tolerance Met? NO</b> Spherically Seated</p>
--	---

<b>PERPENDICULARITY (Procedure P1)</b> (Calculated from End Flatness and Parallelism measurements above)					
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?
Diameter 1, in	0.00240	1.970	0.00122	0.070	YES
Diameter 2, in (rotated 90°)	0.00230	1.970	0.00117	0.067	YES
	Maximum angle of departure must be $\leq$ 0.25° <b>Perpendicularity Tolerance Met? YES</b>				
END 2					
Diameter 1, in	0.00250	1.970	0.00127	0.073	YES
Diameter 2, in (rotated 90°)	0.00250	1.970	0.00127	0.073	YES



Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-101	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R-4		
Depth (ft):	37-37.3		
Visual Description:	See photographs		

**BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO ASTM D4543**

<b>END FLATNESS</b>		
END 1		
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES
END 2		
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES
<b>End Flatness Tolerance Met? YES</b>		

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	smd
Boring ID:	BB-BSA-101
Sample ID:	R-4
Depth, ft:	37-37.3



After cutting and grinding

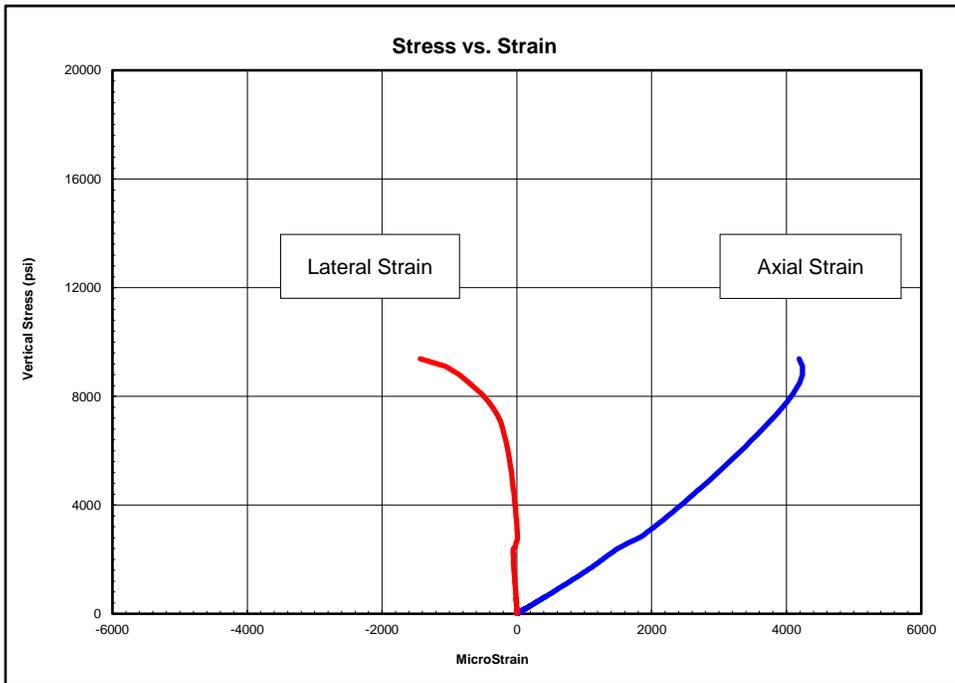


After break



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-105
Sample ID:	R-1
Depth, ft:	28.8-29.1
Sample Type:	rock core
Sample Description:	See photographs Intact material failure Best Effort end preparation performed

## Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 9,458 psi

Poisson's Ratio within the first and third stress ranges could not be determined.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
900-3500	1,610,000	---
3500-6000	2,190,000	0.10
6000-8500	2,730,000	---

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature. The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes. Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed. Calculations assume samples are isotropic, which is not necessarily the case.



Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-105		
Sample ID:	R-1		
Depth (ft):	28.8-29.1		
Visual Description:	See photographs		

**UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543**

<b>BULK DENSITY</b>				<b>DEVIATION FROM STRAIGHTNESS (Procedure S1)</b>			
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap $\leq$ 0.02 in.? <b>YES</b>			
Specimen Length, in:	4.30	4.30	4.30	Maximum difference must be < 0.020 in. <b>Straightness Tolerance Met? YES</b>			
Specimen Diameter, in:	1.96	1.96	1.96				
Specimen Mass, g:	582.84						
Bulk Density, lb/ft <sup>3</sup> :	171						
Length to Diameter Ratio:	2.2						
		<b>Minimum Diameter Tolerance Met?</b>	<b>YES</b>				
		<b>Length to Diameter Ratio Tolerance Met?</b>	<b>YES</b>				

<b>END FLATNESS AND PARALLELISM (Procedure FP1)</b>															
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00160	-0.00120	-0.00100	-0.00060	-0.00030	-0.00010	0.00000	0.00000	0.00030	0.00070	0.00080	0.00080	0.00110	0.00120	0.00150
Diameter 2, in (rotated 90°)	-0.00100	-0.00080	-0.00080	-0.00050	-0.00040	-0.00030	-0.00010	0.00000	0.00000	0.00010	0.00020	0.00030	0.00030	0.00050	0.00070
											Difference between max and min readings, in: 0° = 0.00310      90° = 0.00170				
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00190	-0.00150	-0.00130	-0.00080	-0.00060	-0.00050	-0.00020	0.00000	0.00010	0.00030	0.00050	0.00060	0.00090	0.00110	0.00120
Diameter 2, in (rotated 90°)	0.00070	0.00060	0.00060	0.00060	0.00030	0.00010	0.00000	0.00000	0.00000	-0.00010	-0.00030	-0.00060	-0.00070	-0.00080	-0.00110
											Difference between max and min readings, in: 0° = 0.0031      90° = 0.0018 Maximum difference must be < 0.0020 in.      Difference = $\pm$ 0.00155 <b>Flatness Tolerance Met? NO</b>				

		<p><b>DIAMETER 1</b></p> <p>End 1: Slope of Best Fit Line: 0.00164 Angle of Best Fit Line: 0.09396</p> <p>End 2: Slope of Best Fit Line: 0.00169 Angle of Best Fit Line: 0.09675</p> <p>Maximum Angular Difference: 0.00278</p> <p><b>Parallelism Tolerance Met? YES</b> Spherically Seated</p>

<b>PERPENDICULARITY (Procedure P1)</b> (Calculated from End Flatness and Parallelism measurements above)						Maximum angle of departure must be $\leq$ 0.25°	
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?		
Diameter 1, in	0.00310	1.960	0.00158	0.091	YES		
Diameter 2, in (rotated 90°)	0.00170	1.960	0.00087	0.050	YES	<b>Perpendicularity Tolerance Met? YES</b>	
END 2							
Diameter 1, in	0.00310	1.960	0.00158	0.091	YES		
Diameter 2, in (rotated 90°)	0.00180	1.960	0.00092	0.053	YES		

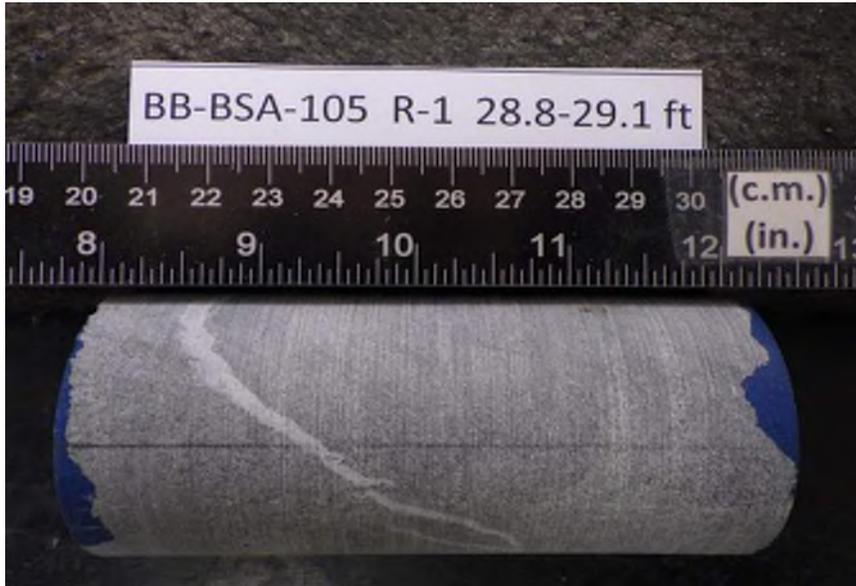


Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-105	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R-1		
Depth (ft):	28.8-29.1		
Visual Description:	See photographs		

**BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO ASTM D4543**

<b>END FLATNESS</b>			
END 1			
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
END 2			
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
<b>End Flatness Tolerance Met? YES</b>			

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	smd
Boring ID:	BB-BSA-105
Sample ID:	R-1
Depth, ft:	28.8-29.1



After cutting and grinding

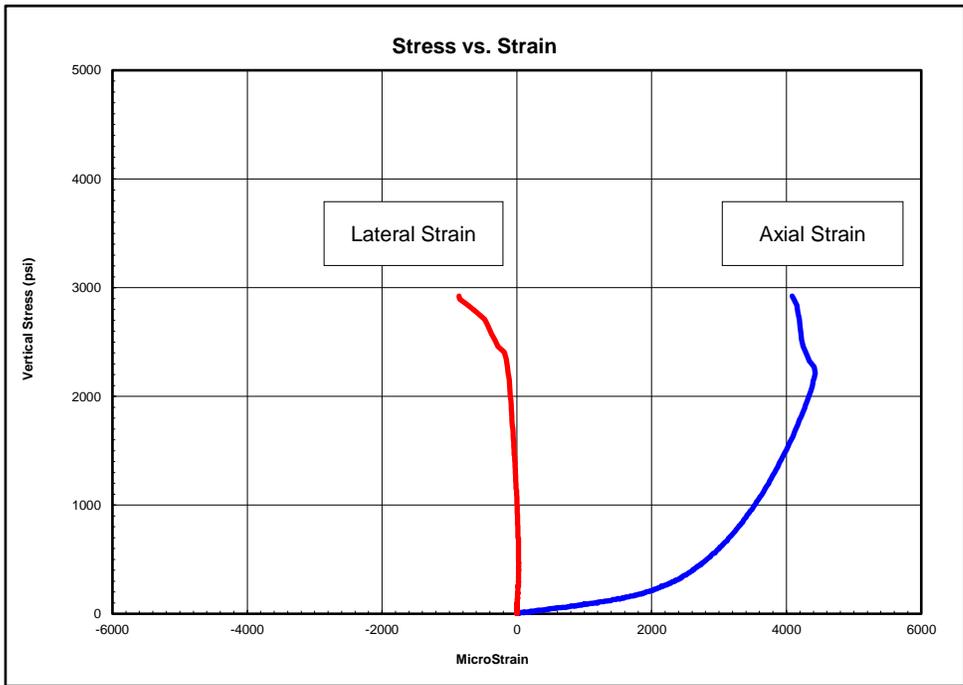


After break



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-106
Sample ID:	R-3
Depth, ft:	69.3-69.6
Sample Type:	rock core
Sample Description:	See photographs Intact material failure Best Effort end preparation performed

## Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 3,226 psi

The strain gauges failed before the peak value was attained. Young's Modulus and Poisson's Ratio could not be determined within the third stress range.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
300-1200	626,000	0.03
1200-2000	1,310,000	0.14
2000-2900	---	---

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature. The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes. Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed. Calculations assume samples are isotropic, which is not necessarily the case.



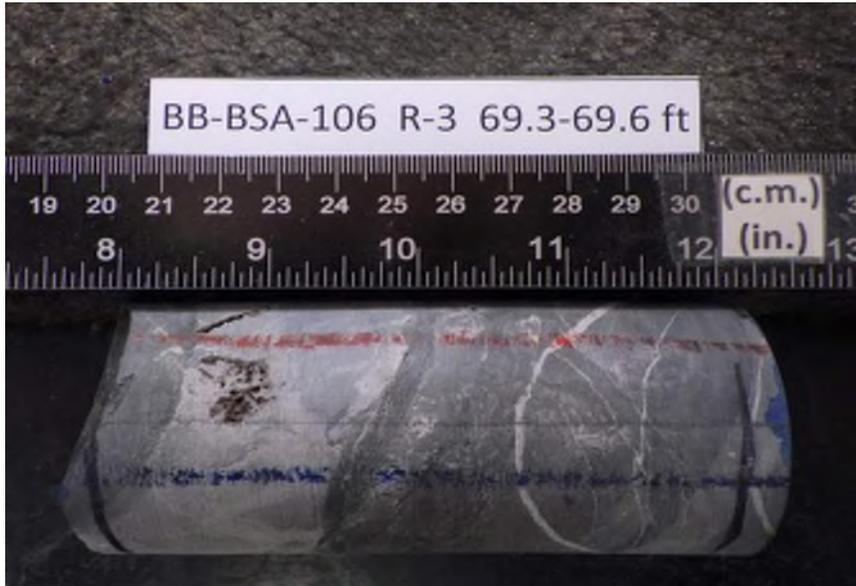


Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-106	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R-3		
Depth (ft):	69.3-69.6		
Visual Description:	See photographs		

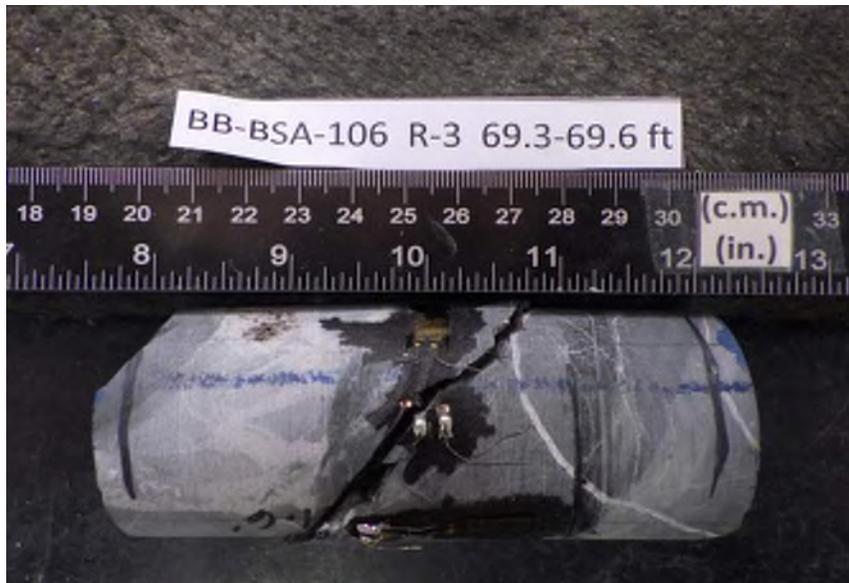
**BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO ASTM D4543**

<b>END FLATNESS</b>			
END 1			
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
END 2			
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
<b>End Flatness Tolerance Met? YES</b>			

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	smd
Boring ID:	BB-BSA-106
Sample ID:	R-3
Depth, ft:	69.3-69.6



After cutting and grinding

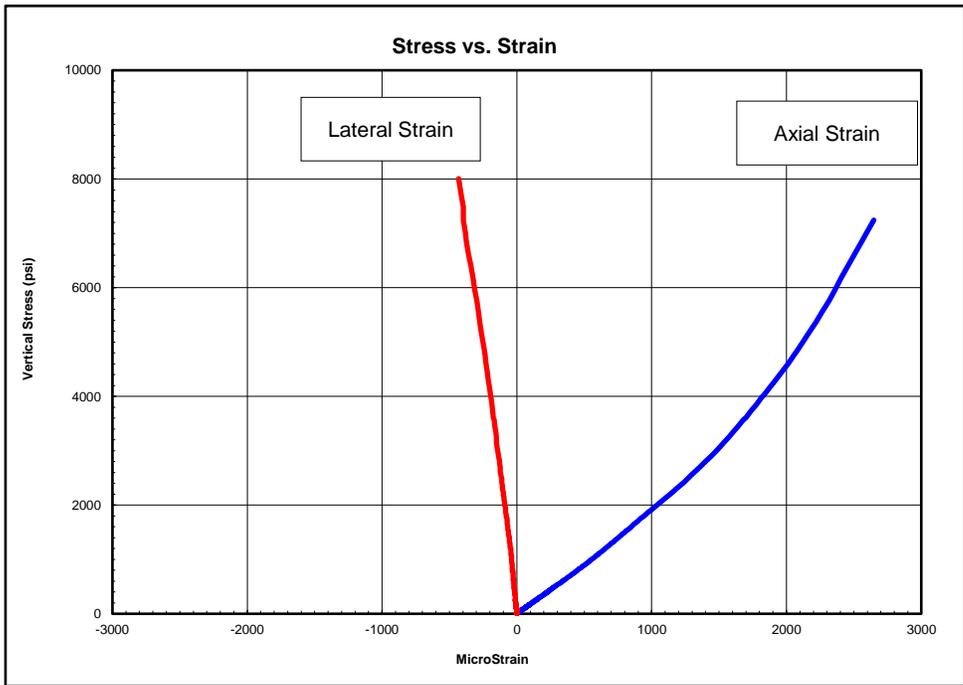


After break



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-111
Sample ID:	R-1
Depth, ft:	21.4-21.7
Sample Type:	rock core
Sample Description:	See photographs Intact material and discontinuity failure Best Effort end preparation performed

## Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 8,006 psi

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
800-2900	2,080,000	0.10
2900-5100	3,070,000	0.17
5100-7200	4,360,000	0.29

**Notes:** Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature. The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes. Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed. Calculations assume samples are isotropic, which is not necessarily the case.





Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-111	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R-1		
Depth (ft):	21.4-21.7		
Visual Description:	See photographs		

**BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO ASTM D4543**

<b>END FLATNESS</b>			
END 1			
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
END 2			
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES	
<b>End Flatness Tolerance Met? YES</b>			

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	smd
Boring ID:	BB-BSA-111
Sample ID:	R-1
Depth, ft:	21.4-21.7



After cutting and grinding



After break

**APPENDIX D**

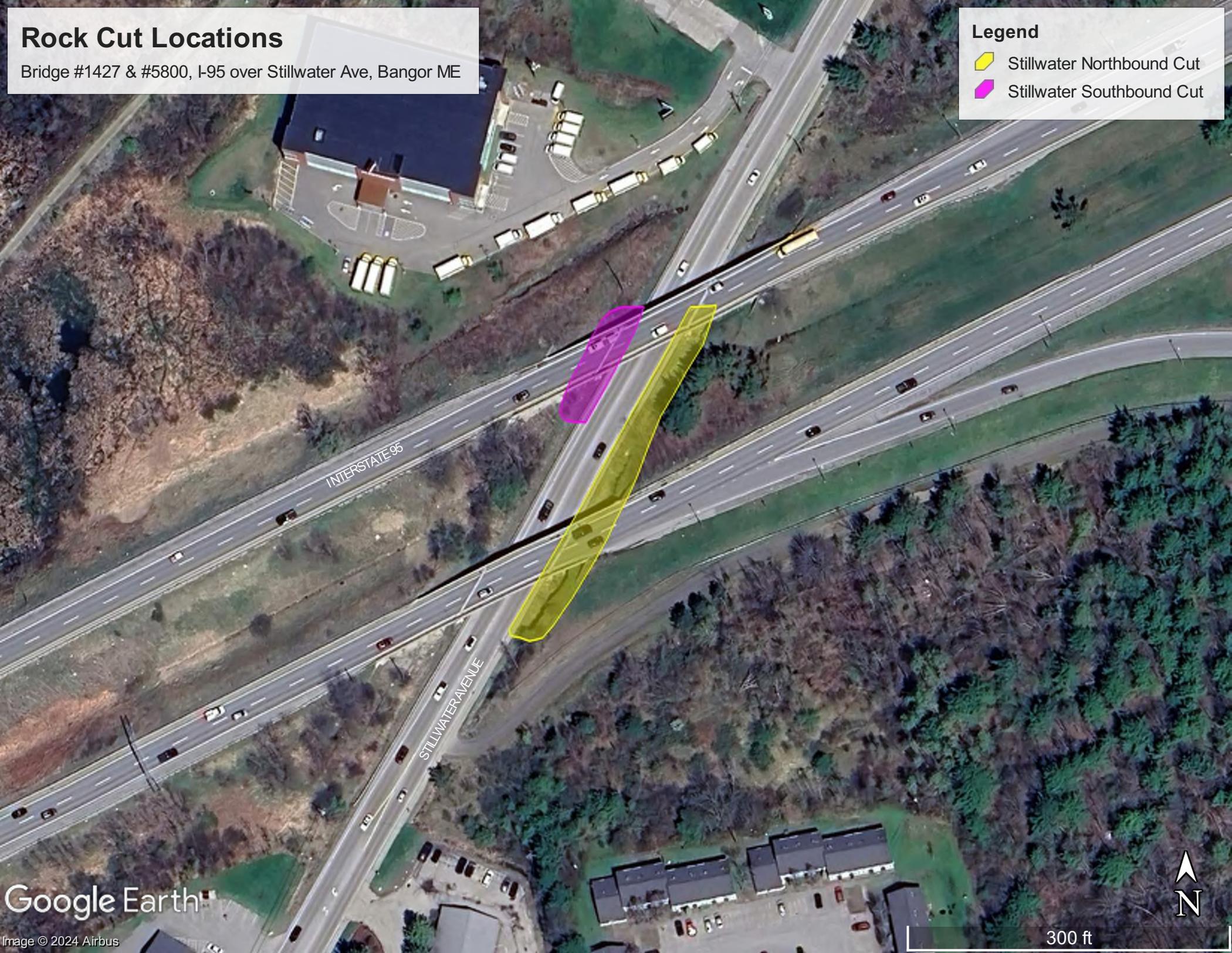
# Rock Discontinuity Calculations

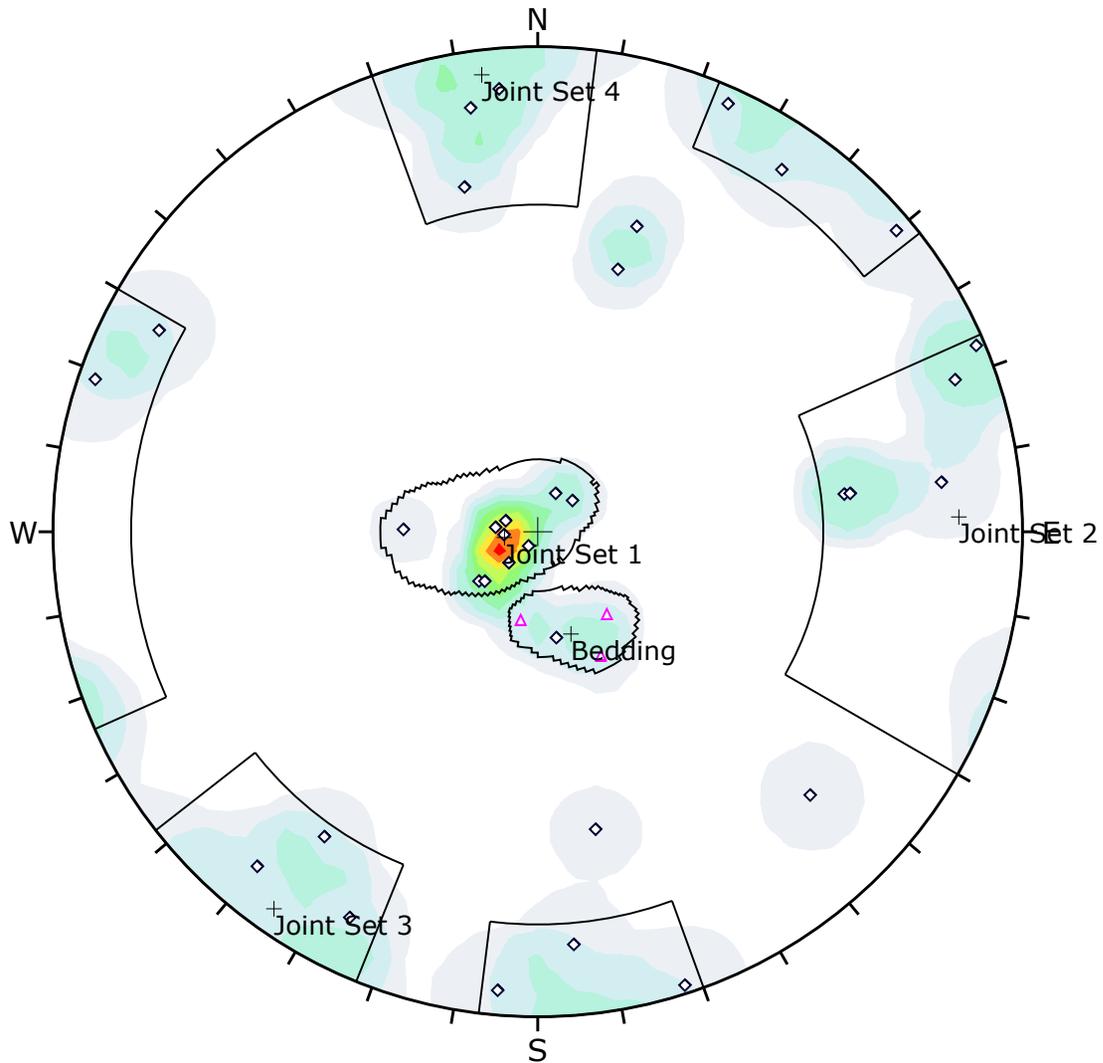
# Rock Cut Locations

Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor ME

## Legend

-  Stillwater Northbound Cut
-  Stillwater Southbound Cut





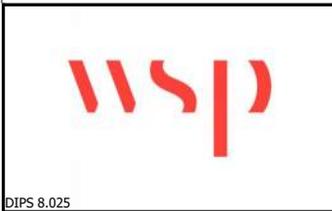
Symbol	TYPE	Quantity
▲	bedding	3
◇	joint	34

Color	Density Concentrations
	0.00 - 1.40
	1.40 - 2.80
	2.80 - 4.20
	4.20 - 5.60
	5.60 - 7.00
	7.00 - 8.40
	8.40 - 9.80
	9.80 - 11.20
	11.20 - 12.60
	12.60 - 14.00

Contour Data	Pole Vectors
Maximum Density	13.44%
Contour Distribution	Fisher
Counting Circle Size	1.0%

	Color	Dip	Dip Direction	Label
<b>Mean Set Planes</b>				
1m	■	8	80	Joint Set 1
2m	■	82	268	Joint Set 2
3m	■	87	35	Joint Set 3
4m	■	87	173	Joint Set 4
5m	■	25	342	Bedding

Plot Mode	Pole Vectors
Vector Count	37 (37 Entries)
Hemisphere	Lower
Projection	Equal Angle



<i>Project</i>		I-95 Bridge #1427 & #5800 over Stillwater Ave, Bangor ME, MaineDOT WIN 027176.00			
<i>Analysis Description</i>		Outcrops along Stillwater Ave Northbound and Southbound			
<i>Drawn By</i>	KAR	<i>Checked By</i>	BK	<i>Reviewed By</i>	JDL
<i>Date</i>	5/21/2024	<i>Scale</i>	N/A		
<i>File Name</i>	Stillwater-outcrop-data.dips8				<b>Appendix D.1</b>
DIPS 8.025					

**Appendix D.2: Calculation of Rock Mass Rating**  
**Preliminary Geotechnical Design Report**  
**Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine**  
**MaineDOT WIN 027176.00**

*References:*

1. Bieniawski, Z.T. 1989. Engineering Rock Mass Classifications: A Complete Manual for Engineers and Geologists in Mining, Civil, and Petroleum Engineering. John Wiley & Sons.
2. Wyllie, Duncan C. 1999. Foundations on Rock, 2nd Edition. E&FN Spon.
3. Hoek, Evert. 2006. Practical Rock Engineering. Rocscience Inc.

*Notes:*

1. The RMR ratings for parameter 1 (intact rock strength), parameter 2 (drill core quality RQD), and parameter 3 (discontinuity spacing) are selected using Charts A, B, and C, respectively, from Bieniawski 1989 (Ref. 1). For core runs on which UCS lab testing was not performed, the intact strength rating is selected based on field strength estimates using Table 3.5 from Wyllie 1999 (Ref. 2).
2. The RMR ratings for parameter 4 (discontinuity condition) are selected using Section E of Table 4 from Hoek 2006 (Ref. 3).
3. The RMR ratings for parameter 5 (groundwater) are selected using Table 3.5 from Wyllie 1999 (Ref. 2).
4. For the outcrop discontinuities, the RQD is correlated from discontinuity spacing based on Chart D from Bieniawski 1989 (Ref. 1).
5. For the boring core runs, the persistence rating is based on an average of the persistence measurements at the outcrops.
6. The rating adjustment for joint orientation (parameter B) is selected from Bieniawski 1989 (Ref. 1), using an orientation adjustment of -15 ("unfavorable" for foundations) for the bedding set based on the kinematic possibility of planar sliding and for joint set 2 based on the kinematic possibility of toppling. Since the boring rock core was collected unoriented, an average of all outcrop orientation adjustments is used for the boring core runs.

Prepared by: KAR  
 Checked by: BK  
 Reviewed by: JDL

**Overall average RMR = 54**

Boring or Outcrop	Run Number or Discontinuity ID	Intact Strength			RQD (%)	Fracture Spacing			A. Classification Parameters										B. Rating adjustment for joint orientation	RMR
		UCS (psi)	UCS (MPa)	Field Strength Estimate		Average fractures per foot	Average spacing (ft)	Average spacing (mm)	1	2	3	4						5		
									Strength of rock	RQD	Spacing of joints	Condition of Joints								
												Persistence	Aperture	Roughness	Infilling	Weathering	Total			
BB-BSA-101	R1	-	-	Very Strong (R5)	0	broken	-	-	12	3	5	2	0	1	0	5	8	7	-4	31
	R2	-	-	Strong (R4) to Very Strong (R5)	0	broken	-	-	7	3	5	2	0	5	0	5	12	7	-4	30
	R3	-	-	Strong (R4) to Very Strong (R5)	14	3.5	0.3	87	7	5	6	2	0	5	6	5	18	7	-4	39
	R4	-	-	Strong (R4)	60	1.6	0.6	191	9	12	8	2	5	5	6	6	24	7	-4	56
BB-BSA-102	R1	17,296	119	Strong (R4) to Extremely Strong (R6)	52	3.2	0.3	95	11	10	6	2	0	1	2	5	10	7	-4	40
	R2	-	-	Extremely Strong (R6)	88	0.2	5.0	1524	15	18	16	2	0	6	6	6	20	7	-4	72
BB-BSA-103	R1	-	-	Extremely Strong (R6)	31	4.0	0.3	76	15	7	6	2	1	1	4	5	13	7	-4	44
	R2	-	-	Extremely Strong (R6)	70	2.0	0.5	152	15	14	7	2	4	5	6	6	23	7	-4	62
BB-BSA-104A	R1	-	-	Strong (R4) to Very Strong (R5)	56	1.6	0.6	191	7	11	8	2	0	5	0	5	12	7	-4	41
	R2	-	-	Strong (R4) to Very Strong (R5)	61	0.5	2.0	610	7	12	12	2	5	5	6	6	24	7	-4	58
	R3	-	-	Strong (R4) to Very Strong (R5)	23	3.5	0.3	87	7	6	6	2	0	5	6	6	19	7	-4	41
BB-BSA-105	R1	-	-	Strong (R4)	30	3.2	0.3	95	7	7	6	2	0	5	6	5	18	7	-4	41
	R2	-	-	Very Strong (R5)	75	1.6	0.6	191	12	15	8	2	5	1	6	6	20	7	-4	58
BB-BSA-106	R1	-	-	Strong (R4) to Very Strong (R5)	0	broken	-	-	7	3	5	2	0	5	6	5	18	7	-4	36
	R2	-	-	Strong (R4) to Very Strong (R5)	47	3.3	0.3	92	7	10	6	2	0	1	0	6	9	7	-4	35
	R3	-	-	Weak (R2)	62	1.4	0.7	218	3	12	8	2	0	5	6	6	19	7	-4	45
BB-BSA-107	R1	-	-	Strong (R4)	0	broken	-	-	7	3	5	2	0	5	0	1	8	7	-4	26
	R2	-	-	Strong (R4)	0	broken	-	-	7	3	5	2	0	6	0	1	9	7	-4	27
	R3	-	-	Strong (R4) to Very Strong (R5)	35	3.5	0.3	87	7	8	6	2	0	5	0	5	12	7	-4	36
	R4	-	-	Strong (R4) to Very Strong (R5)	39	3.2	0.3	95	7	8	6	2	0	5	0	5	12	7	-4	36

Boring or Outcrop	Run Number or Discontinuity ID	Intact Strength			RQD (%)	Fracture Spacing			A. Classification Parameters										B. Rating adjustment for joint orientation	RMR
		UCS (psi)	UCS (MPa)	Field Strength Estimate		Average fractures per foot	Average spacing (ft)	Average spacing (mm)	1	2	3	4					5			
									Strength of rock	RQD	Spacing of joints	Condition of Joints					Ground water			
												Persistence	Aperture	Roughness	Infilling	Weathering		Total		
BB-BSA-108	R1	-	-	Very Strong (R5) to Extremely Strong (R6)	58	2.6	0.4	117	12	11	7	2	0	5	6	5	18	7	-4	51
	R2	-	-	Extremely Strong (R6)	42	1.0	1.0	305	15	9	9	2	1	1	6	5	15	7	-4	51
	R3	-	-	Extremely Strong (R6)	17	2.5	0.4	122	15	5	7	2	1	1	6	5	15	7	-4	45
	R4	-	-	Extremely Strong (R6)	35	2.0	0.5	152	15	8	7	2	1	1	6	5	15	7	-4	48
BB-BSA-109A	R1	-	-	Very Strong (R5) to Extremely Strong (R6)	30	1.8	0.6	169	12	7	7	2	0	1	6	5	14	7	-4	43
	R2	-	-	Very Strong (R5) to Extremely Strong (R6)	49	1.6	0.6	191	12	10	8	2	1	1	6	6	16	7	-4	49
BB-BSA-110	R1	5,948	41	Medium Strong (R3)	49	1.0	1.0	305	5	10	9	2	1	1	6	6	16	7	-4	43
	R2	-	-	Very Strong (R5) to Extremely Strong (R6)	71	0.8	1.3	381	12	14	10	2	0	1	6	6	15	7	-4	54
BB-BSA-111	R1	-	-	Strong (R4) to Very Strong (R5)	15	broken	-	-	6	5	5	2	0	5	6	5	18	7	-4	37
	R2	-	-	Strong (R4) to Very Strong (R5)	60	1.6	0.6	191	7	12	8	2	5	5	6	6	24	7	-4	54
Outcrop along Stillwater Ave Northbound	Disc. 1	-	-	-	20	-	0.2	61	15	5	6	2	1	5	6	5	19	10	-15	40
	Disc. 2	-	-	-	93	-	1.5	457	15	19	10	2	0	3	0	5	10	10	0	64
	Disc. 3	-	-	-	99	-	2.8	853	15	20	13	6	0	3	6	5	20	10	0	78
	Disc. 4	-	-	-	85	-	0.9	274	15	17	9	4	0	1	0	5	10	10	-15	46
	Disc. 5	-	-	-	100	-	5.9	1798	15	20	16	4	1	1	6	5	17	10	0	78
	Disc. 6	-	-	-	95	-	1.6	488	15	19	11	2	1	3	6	5	17	10	0	72
	Disc. 7	-	-	R6	41	-	0.3	91	15	9	6	2	6	5	6	5	24	10	-15	49
	Disc. 8	-	-	-	100	-	5.9	1798	15	20	16	6	0	1	0	5	12	10	0	73
	Disc. 9	-	-	-	88	-	1.1	335	4	18	9	2	1	3	6	5	17	10	0	58
	Disc. 10	-	-	-	86	-	1.0	305	4	17	9	2	0	3	2	5	12	10	0	52
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	Disc. 13	-	-	-	100	-	5.4	1646	4	20	16	4	1	3	6	5	19	10	-15	54
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	Disc. 18	-	-	-	99	-	2.5	762	15	20	13	2	6	1	6	5	20	10	0	78
	Disc. 19	-	-	-	96	-	1.8	549	12	19	11	2	1	5	6	5	19	10	0	71
	Disc. 20	-	-	-	96	-	1.7	518	12	19	11	2	0	3	0	5	10	10	-15	47
	Disc. 21	-	-	-	56	-	0.4	122	12	11	7	4	1	1	6	5	17	10	-15	42
	Disc. 22	-	-	-	96	-	1.8	549	12	19	11	2	1	3	6	5	17	10	-15	54
	Disc. 23	-	-	R5	98	-	2.0	610	12	20	12	2	0	1	2	5	10	10	0	64
	Disc. 24	-	-	-	92	-	1.4	427	12	18	10	2	6	3	6	5	22	10	0	72
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	Disc. 27	-	-	-	100	-	4.0	1219	15	20	15	2	0	1	0	5	8	10	0	68
	Disc. 28	-	-	-	96	-	1.8	549	15	19	11	2	0	5	2	5	14	10	0	69
	Disc. 29	-	-	R6	99	-	2.2	671	15	20	12	2	1	5	4	5	17	10	0	74
	Disc. 30	-	-	R6	95	-	1.6	488	15	19	11	2	0	3	2	5	12	10	0	67
	Disc. 31	-	-	R6	99	-	2.3	701	15	20	12	4	0	3	0	5	12	10	0	69

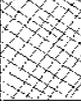
Boring or Outcrop	Run Number or Discontinuity ID	Intact Strength			RQD (%)	Fracture Spacing			A. Classification Parameters										B. Rating adjustment for joint orientation	RMR
		UCS (psi)	UCS (MPa)	Field Strength Estimate		Average fractures per foot	Average spacing (ft)	Average spacing (mm)	1	2	3	4						5		
									Strength of rock	RQD	Spacing of joints	Condition of Joints						Ground water		
												Persistence	Aperture	Roughness	Infilling	Weathering	Total			
Outcrop along Stillwater Ave Southbound	Disc. 32	-	-	-	85	-	0.9	274	15	17	9	4	0	6	0	5	15	10	0	66
	Disc. 33	-	-	-	20	-	0.2	61	15	5	6	4	1	5	2	5	17	10	0	53
	Disc. 34	-	-	-	41	-	0.3	91	12	9	6	4	1	6	2	5	18	10	-15	40
	Disc. 35	-	-	-	98	-	2.0	610	12	20	12	4	0	5	6	5	20	10	0	74
	Disc. 36	-	-	R5	76	-	0.6	183	12	15	8	6	1	1	2	5	15	10	0	60
	Disc. 37	-	-	-	56	-	0.4	122	12	11	7	4	0	1	6	5	16	10	-15	41

**Appendix D.3: Calculation of Geological Strength Index  
Preliminary Geotechnical Design Report  
Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine  
MaineDOT WIN 027176.00**

Prepared by: KAR  
Checked by: BK  
Reviewed by: JDL

**GSI = 55**

Table 5: Most common GSI ranges for typical sandstones.\*

GEOLOGICAL STRENGTH INDEX FOR JOINTED ROCKS (Hoek and Marinos, 2000) From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. <u>Note that the table does not apply to structurally controlled failures.</u> Where weak planar structural planes are present in an unfavourable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis.		SURFACE CONDITIONS								
STRUCTURE		DECREASING SURFACE QUALITY →								
	INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities	90	80	70	60	50	40	30	20	10
	BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets	90	80	70	60	50	40	30	20	10
	VERY BLOCKY- interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets	90	80	70	60	50	40	30	20	10
	BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity	90	80	70	60	50	40	30	20	10
	DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces	90	80	70	60	50	40	30	20	10
	LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

**\*WARNING:**  
The shaded areas are indicative and may not be appropriate for site specific design purposes. Mean values are not suggested for indicative characterisation; the use of ranges is recommended

- 1. Massive or bedded (no clayey cement present)
- 2. Brecciated (no clayey cement present)

GSI chart from: Marinos, Paul, and Hoek, Evert. November 2000. GSI: a geologically friendly tool for rock mass strength estimation. ISRM International Symposium, Melbourne, Australia, paper number ISRM-IS-2000-035.

**APPENDIX E**

**Rock Cut Discontinuity Photographs**

NORTH

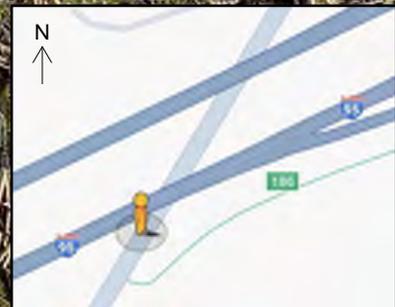
SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**02**

OF 54



NORTH

SOUTH

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Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



NORTH

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**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



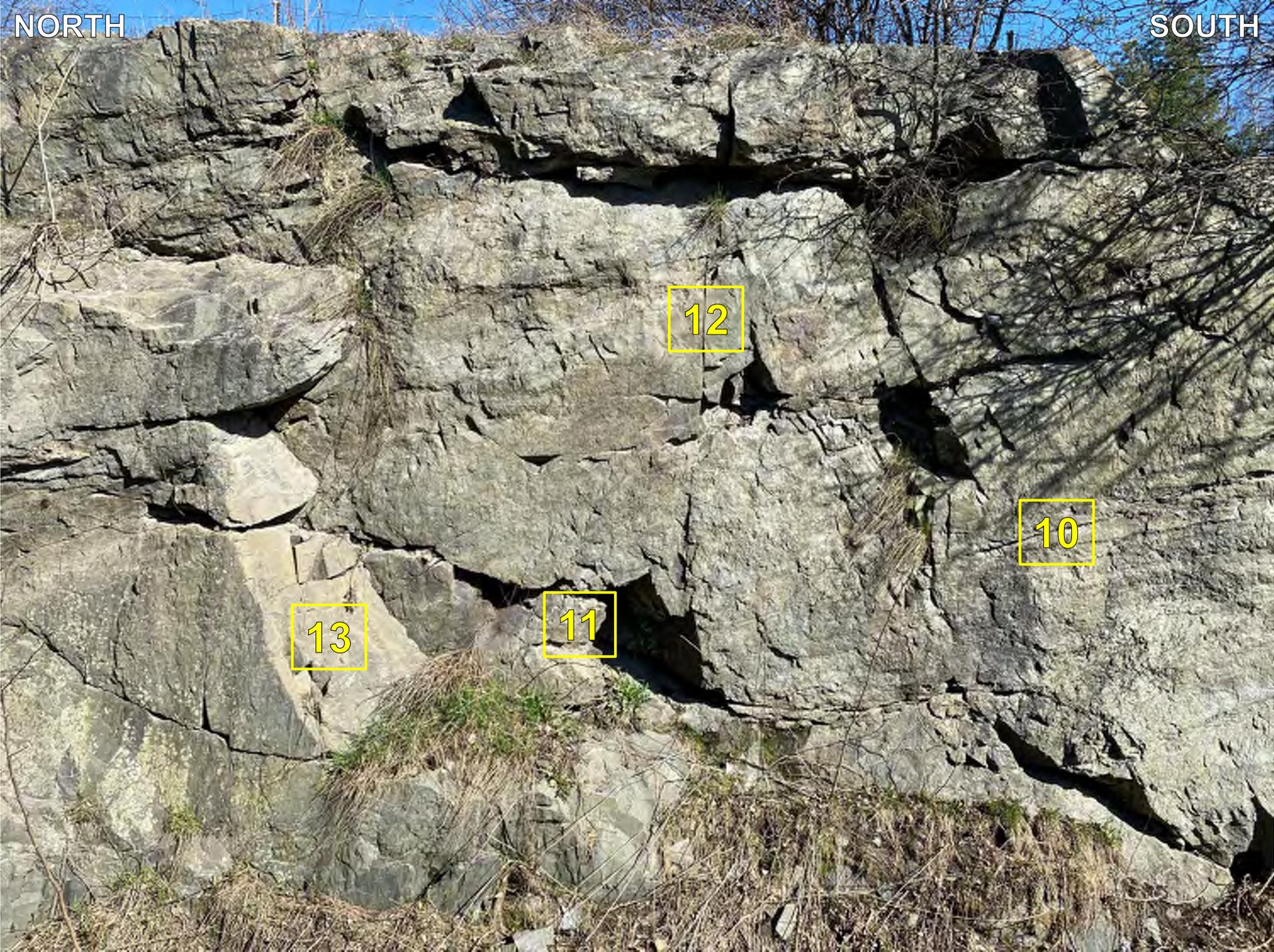
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I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



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**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

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OF 54



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**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**06**

OF 54



NORTH

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ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



NORTH

SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
**STILLWATER AVENUE NORTHBOUND**



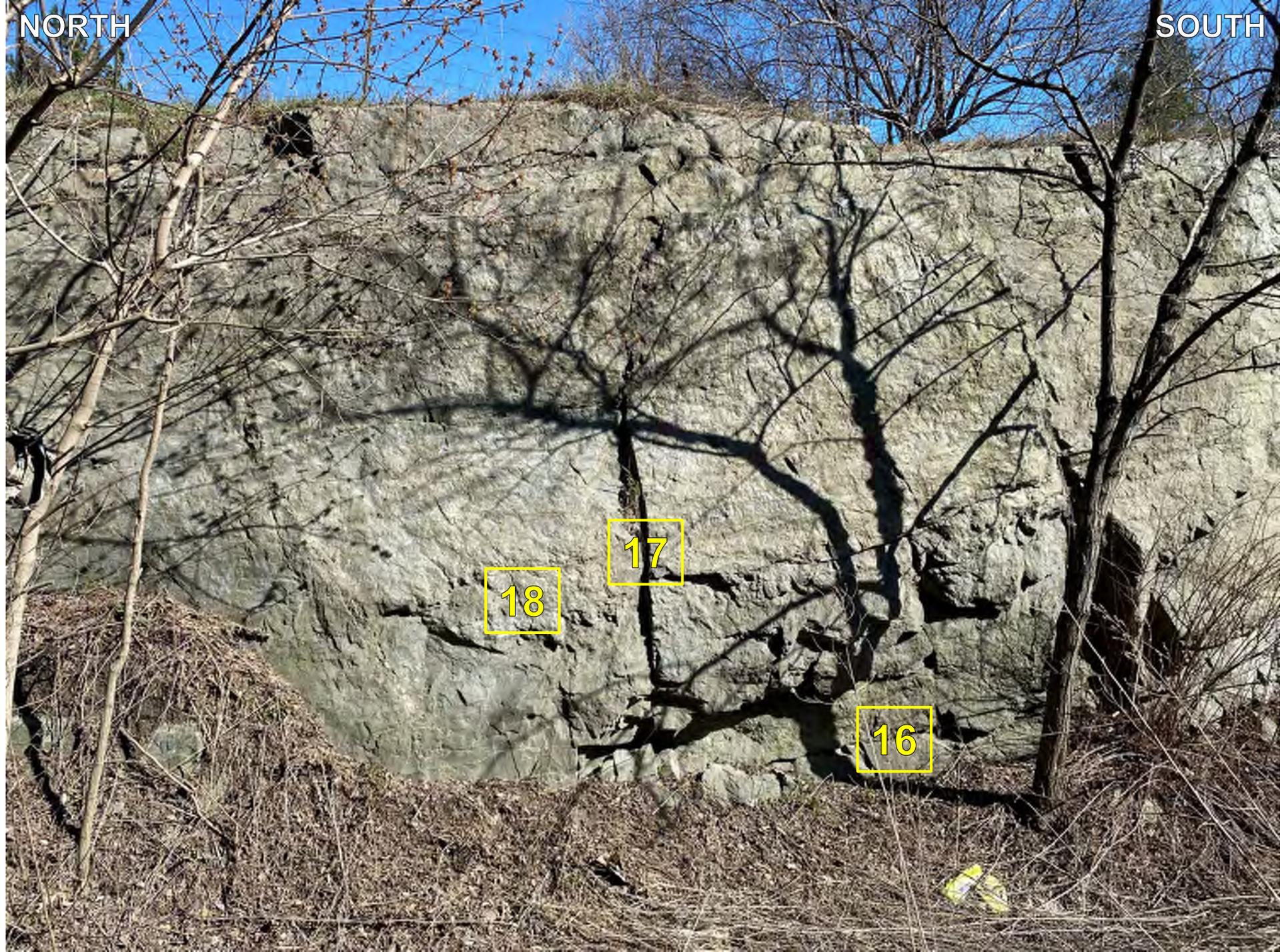
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I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



NORTH

SOUTH

ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**09**

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE NORTHBOUND

19

18

17

BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



NORTH

SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**11**

OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



NORTH

SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**13**

OF 54



NORTH

SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE NORTHBOUND

24



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

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14

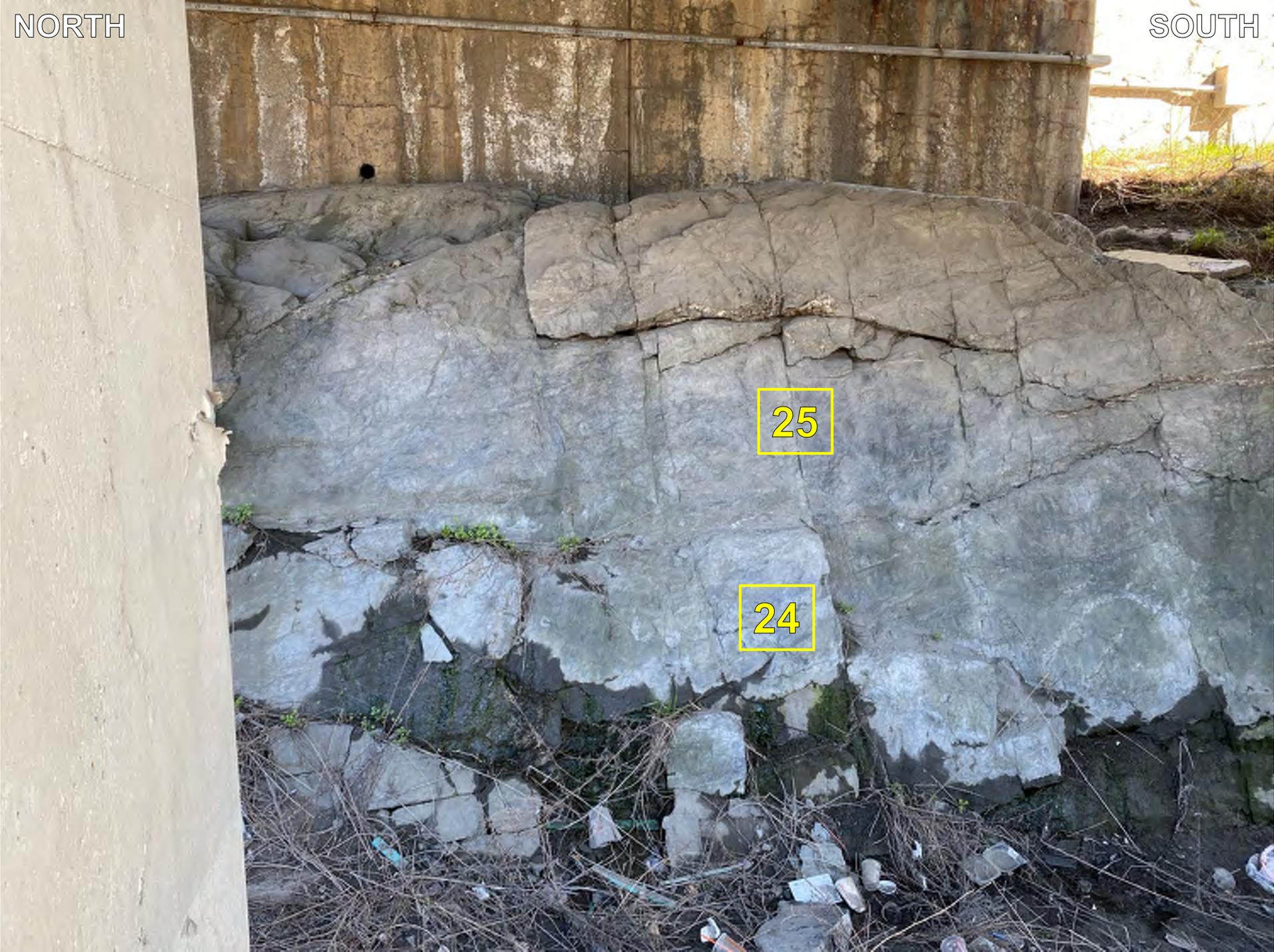
OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

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OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**16**

OF 54



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SOUTH

Date: 11/4/2024  
Prepared: KAR  
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Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**17**

OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND

26



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**18**

OF 54



NORTH

SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



NORTH

SOUTH

ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



28

27

BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

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OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**22**  
OF 54



NORTH

SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

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OF 54



NORTH

SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

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OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE NORTHBOUND**



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**25**

OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**26**

OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
**STILLWATER AVENUE NORTHBOUND**



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**27**

OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
**STILLWATER AVENUE NORTHBOUND**



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE NORTHBOUND**



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I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00**



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**30**

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

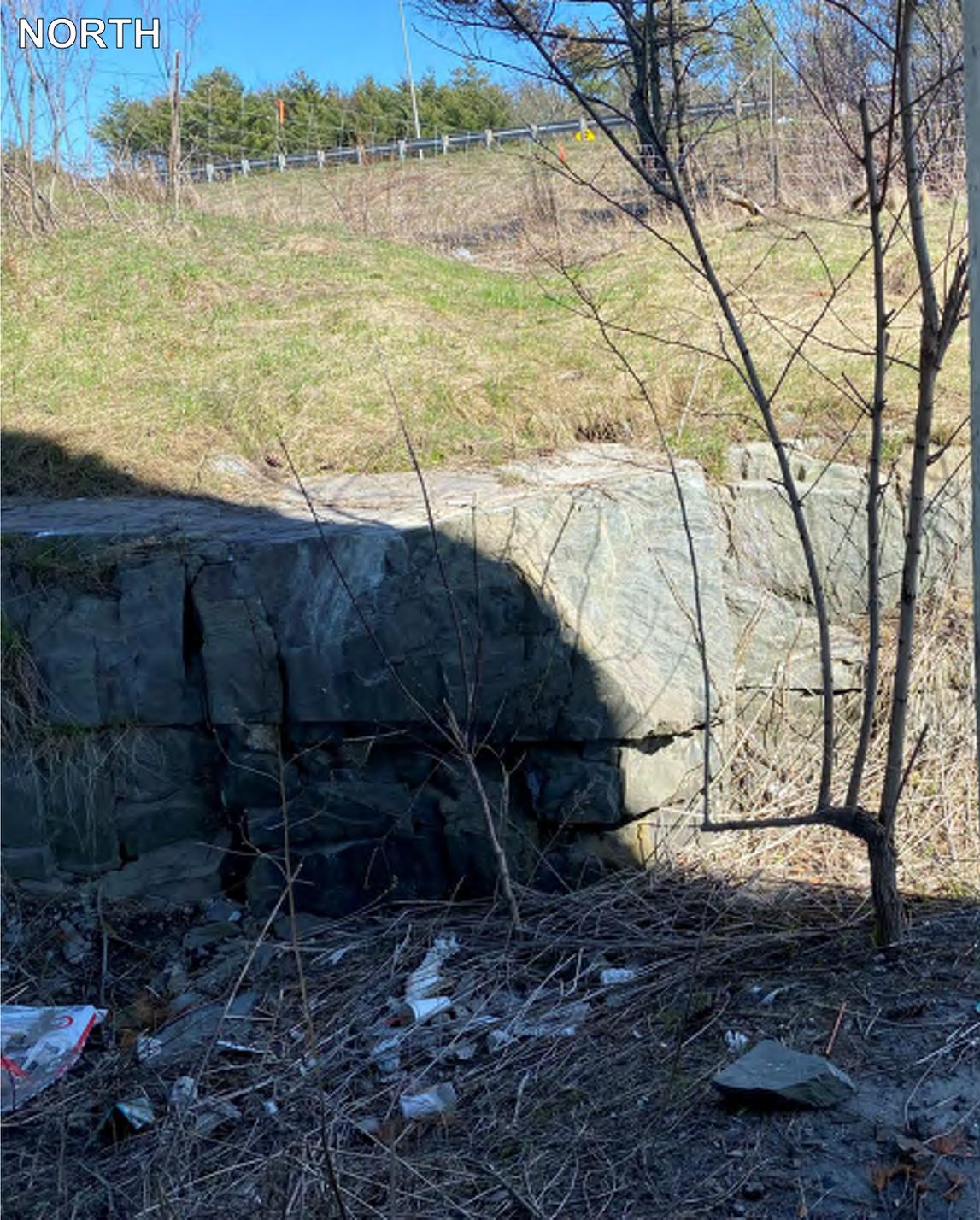


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SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**32**

OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**33**

OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**34**

OF 54



NORTH

SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**35**

OF 54



NORTH

SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**36**  
OF 54

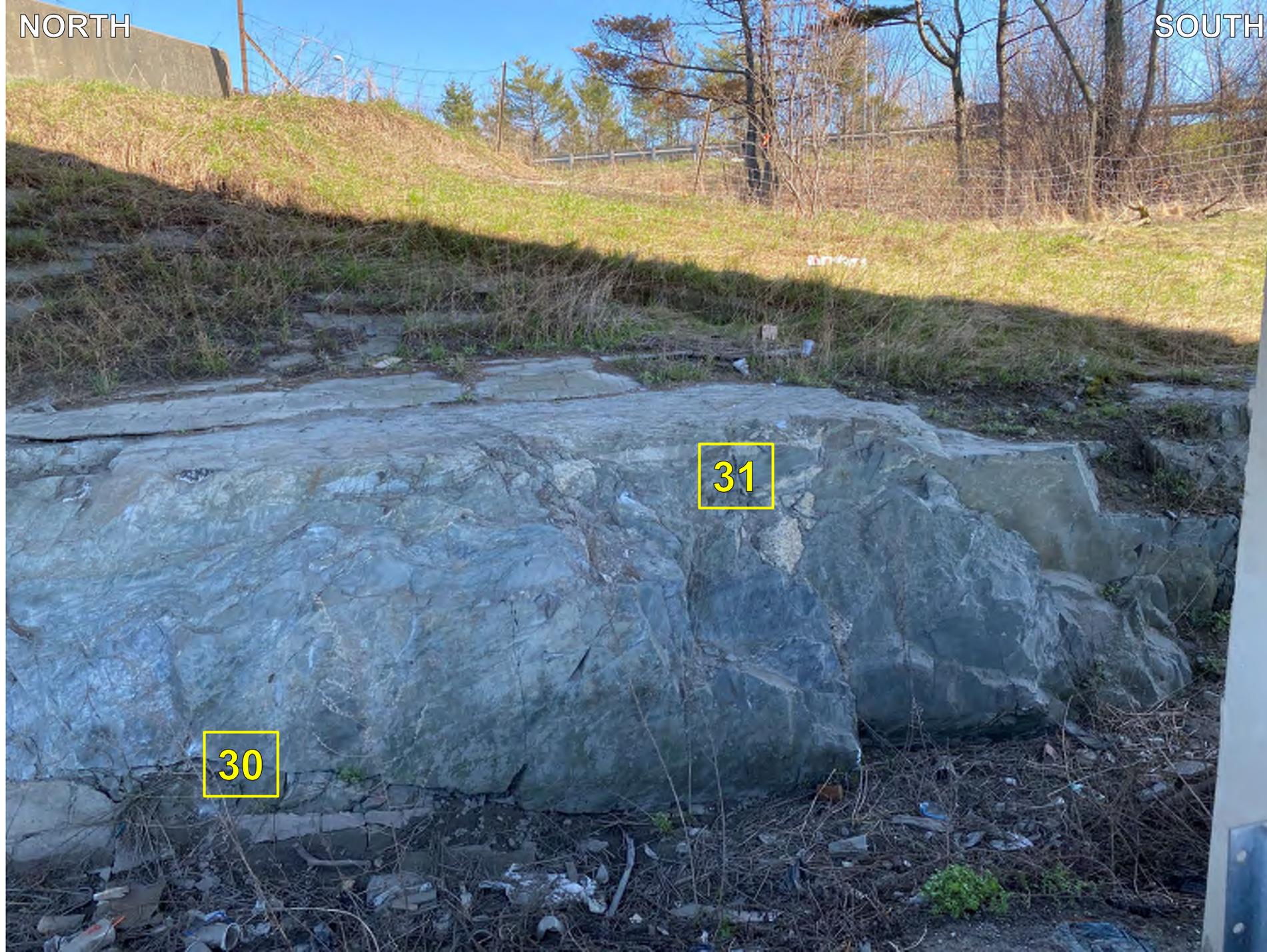


NORTH

SOUTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**37**  
OF 54



NORTH

SOUTH

ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**38**  
OF 54



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



NORTH

SOUTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**41**

OF 54



SOUTH

NORTH

ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

42

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



**ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE SOUTHBOUND**



**BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00**



SOUTH

NORTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**45**

OF 54



SOUTH

NORTH

Date: 11/4/2024  
Prepared: KAR  
Checked: LMP  
Reviewed: MEL

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE SOUTHBOUND



35

BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**46**

OF 54



**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00



ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE SOUTHBOUND



36

BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

ROCK CUT DISCONTINUITY ID LOCATIONS  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SOUTH

NORTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**50**

OF 54



SOUTH

NORTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**51**

OF 54



SOUTH

NORTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**52**

OF 54



SOUTH

NORTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**53**

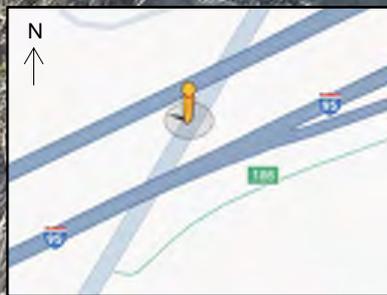
OF 54



SOUTH

NORTH

**ROCK CUT DISCONTINUITY ID LOCATIONS**  
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800  
I-95 OVER STILLWATER AVE, BANGOR, MAINE  
MAINEDOT WIN 027176.00

SHEET NUMBER

**54**  
OF 54



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